

COMMITTENTE



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Comune di Vinci
Piazza Leonardo da Vinci 29, Vinci 50059
RUP: Ing. Claudia Peruzzi

VINCI (FI)

NUOVA SCUOLA DELL'INFANZIA "STACCIA BURATTA"

PROGETTISTA



ST GRUPPO MARCHE
Contrada Potenza, 11 62100 Macerata
P.Iva 00141310433
Tel. +39 0733 492522
azienda certificata
ISO 9001:2015 e ISO 14001:2015

Progetto Esecutivo

Elaborati Generali

RELAZIONE DI CALCOLO DELLA FONDAZIONE

Repertorio/Posizione 2815/01

Data Aprile 2021

Verificato da AC

E-GF-3

Scala

N.	Descrizione	Data
0	Prima Emissione	Apr 2021
1	Revisione	Ago 2021
2		
3		
4		
5		
6		





Comune di Vinci (FI)

REALIZZAZIONE NUOVA SCUOLA DELL'INFANZIA "STACCIA BURATTA"
NEL COMUNE DI VINCI (FI)

Progetto Esecutivo

RELAZIONE DI CALCOLO DELLA FONDAZIONE

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Relazione di calcolo strutturale impostata e redatta secondo le modalità previste nel D.M. 17 Gennaio 2018 cap. 10 "Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo".

Origine e Caratteristiche dei Codici di Calcolo	
Codice di calcolo:	PRO_SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2020-12-191)
Produttore-Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l. Via Garibaldi, 90 44121 Ferrara FE (Italy) Tel. +39 0532 200091 www.2si.it
Codice Licenza:	Licenza dsi2289

Descrizione	
Ubicazione	Comune di VINCI (FI) (Regione TOSCANA)
	Località VINCI (FI)
	Longitudine 10.924, Latitudine 43.782

In merito al punto 10.2 delle Norme Tecniche per le Costruzioni (*Affidabilità dei codici utilizzati*), si fa riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Agosto 2020, disponibile per il download sul sito: <https://www.2si.it/it/prodotti/affidabilita/>

1. INTESTAZIONE E CONTENUTI DELLA RELAZIONE

Progetto

REALIZZAZIONE NUOVA SCUOLA DELL'INFANZIA "STACCIA BURATTA"
NEL COMUNE DI VINCI (FI) - Progetto Esecutivo - Fondazioni

Contenuti della relazione:

RELAZIONE DI CALCOLO STRUTTURALE

- *Origine e Caratteristiche dei Codici di Calcolo*
- *Affidabilità dei codici utilizzati*
- *Validazione dei codici*
- *Tipo di analisi svolta*
- *Modalità di presentazione dei risultati*
- *Informazioni generali sull'elaborazione*
- *Giudizio motivato di accettabilità dei risultati*

STAMPA DEI DATI DI INGRESSO

- *Normative prese a riferimento*
- *Criteri adottati per le misure di sicurezza*
- *Criteri seguiti nella schematizzazione della struttura, dei vincoli e delle sconessioni*
- *Interazione tra terreno e struttura*
- *Legami costitutivi adottati per la modellazione dei materiali e dei terreni*
- *Schematizzazione delle azioni, condizioni e combinazioni di carico*
- *Metodologie numeriche utilizzate per l'analisi strutturale*
- *Metodologie numeriche utilizzate per la progettazione e la verifica degli elementi strutturali*

STAMPA DEI RISULTATI

2. CARATTERISTICHE MATERIALI UTILIZZATI

LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale E
Poisson	coefficiente di contrazione trasversale ni
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica
Fattore di confidenza FC m	Fattore di confidenza specifico per materiale; (è riportato solo se diverso da quello globale della

	struttura)
Fattore di confidenza FC a	Fattore di confidenza specifico per l'armatura (è riportato solo se diverso da quello globale della struttura)
Elasto-plastico	Materiale elastico perfettamente plastico per aste non lineari
Massima compressione	Massima tensione di compressione per aste non lineari
Massima trazione	Massima tensione di trazione per aste non lineari
Fattore attrito	Coefficiente di attrito per aste non lineari
Rapporto HRDb	Rapporto di hardening a flessione
Rapporto HRDv	Rapporto di hardening a taglio

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	c.a.	Resistenza Rc	resistenza a compressione cubica
		Resistenza fctm	resistenza media a trazione semplice
		Coefficiente ksb	Coefficiente di riduzione della resistenza a compressione da utilizzare nello stress block
2	acciaio	Tensione ft	Valore della tensione di rottura
		Tensione fy	Valore della tensione di snervamento
		Resistenza fd	Resistenza di calcolo per SL CNR-UNI 10011
		Resistenza fd (>40)	Resistenza di calcolo per SL CNR-UNI 10011 per spessori > 40mm
		Tensione ammissibile	Tensione ammissibile CNR-UNI 10011
		Tensione ammissibile(>40)	Tensione ammissibile CNR-UNI 10011 per spessori > 40mm
3	muratura	Muratura consolidata	Muratura per la quale si prevedono interventi di rinforzo"
		Incremento resistenza	Incremento conseguito in termini di resistenza
		Incremento rigidezza	Incremento conseguito in termini di rigidezza
		Resistenza f	Valore della resistenza a compressione
		Resistenza fv0	Valore della resistenza a taglio in assenza di tensioni normali
		Resistenza fh	Valore della resistenza a compressione orizzontale
		Resistenza fb	Valore della resistenza a compressione dei blocchi
		Resistenza fbh	Valore della resistenza a compressione dei blocchi in direzione orizzontale
		Resistenza fv0h	Valore della resistenza a taglio in assenza di tensioni normali per le travi
		Resistenza ft	Valore della resistenza a trazione per fessurazione diagonale
		Resistenza fvlim	Valore della massima resistenza a taglio
		Resistenza fbt	Valore della resistenza a trazione dei blocchi
		Coefficiente mu	Coefficiente d'attrito utilizzato per la resistenza a taglio (tipicamente 0.4)
		Coefficiente fi	Coefficiente d'ingranamento utilizzato per la resistenza a taglio
		Coefficiente ksb	Coefficiente di riduzione della resistenza a compressione da utilizzare nello stress block
4	legno		

E0,05	Modulo di elasticità corrispondente ad un frattile del 5%
Resistenza fc0	Valore della resistenza a compressione parallela
Resistenza ft0	Valore della resistenza a trazione parallela
Resistenza fm	Valore della resistenza a flessione
Resistenza fv	Valore della resistenza a taglio
Resist. ft0k	Resistenza caratteristica (tensione amm. per REGLES) per trazione
Resist. fmk	Resistenza caratteristica (tensione amm. per REGLES) per flessione
Resist. fvk	Resistenza caratteristica (tensione amm. per REGLES) per taglio
Modulo E0,05	Modulo elastico parallelo caratteristico
Lamellare	lamellare o massiccio

Nel tabulato si riportano sia i valori caratteristici che medi utilizzando gli uni e/o gli altri in relazione alle richieste di normativa ed alla tipologia di verifica. (Cap.7 NTC18 per materiali nuovi, Cap.8 NTC18 e relativa circolare 21/01/2019 per materiali esistenti, Linee Guida Reluis per incamiciatura CAM, CNR-DT 200 per interventi con FRP)

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm3		
3	Calcestruzzo Classe C28/35			3.260e+05	0.20	1.358e+05	2.50e-03	1.00e-05	
	Resistenza Rc	350.0							
	Resistenza fctm		28.4						
	Rapporto Rfessurata								1.00
	Coefficiente ksb								0.85
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
129	Legno lamellare omogeneo GL24h-legno E = 1.150e+05			1.150e+05	0.0	6500.0	4.20e-04	1.00e-05	
	Modulo E0,05		9.599e+04						
	Lamellare : SI								
	Resistenza fc0	240.0							
	Resistenza ft0	192.0							
	Resistenza fm	240.0							
	Resistenza fv	35.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
145	Legno E = 1.260e+05 XLAM Pannelli orizzontali isotropi (XLAM -2- oriz)			5.685e+04	0.0	6900.0	5.00e-04	1.00e-05	
	Modulo E0,05		5.685e+04						
	Lamellare : SI								
	Resistenza fc0	1.0							
	Resistenza ft0	1.0							
	Resistenza fm	1.0							
	Resistenza fv	1.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
157	Materiale inf. rigido no peso E = 1.000e+09			1.000e+09	0.0	5.000e+08	0.0	1.20e-05	
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
200	XLAM vert 10 (2+2+2+2)-legno E = 8.874e+04 (XLAM -3- vert)			6.748e+04	0.0	6900.0	5.00e-04	1.00e-05	
	Modulo E0,05		6.748e+04						
	Lamellare : SI								
	Resistenza fc0	1.0							
	Resistenza ft0	1.0							
	Resistenza fm	1.0							
	Resistenza fv	1.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
201	XLAM oriz 18 (4+3+4+3+4)-legno E = 8.874e+04 (XLAM -4- oriz)			5.685e+04	0.0	6900.0	5.00e-04	1.00e-05	
	Modulo E0,05		5.685e+04						
	Lamellare : SI								
	Resistenza fc0	1.0							
	Resistenza ft0	1.0							

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
	Resistenza fm	1.0							
	Resistenza fv	1.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05

Travi c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetta a filo	SI	NO	NO	NO	NO	NO
Af inf: da q*L*L /	0.0	0.0	0.0	0.0	0.0	0.0
Armatura						
Minima tesa	0.20	0.31	0.31	0.31	0.31	0.31
Minima compressa	0.20	0.31	0.31	0.31	0.31	0.31
Massima tesa	0.78	0.78	0.78	0.78	0.78	0.78
Da sezione	SI	SI	SI	SI	SI	SI
Usa armatura teorica	NO	NO	NO	NO	NO	NO
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4500.00	4500.00	4500.00	4500.00
Tensione fy staffe [daN/cm2]	4500.00	4500.00	4500.00	4500.00	4500.00	4500.00
Tipo acciaio	tipo C	tipo C	tipo C	tipo C	tipo C	tipo C
Coefficiente gamma s	1.15	1.15	1.15	1.15	1.15	1.15
Coefficiente gamma c	1.50	1.50	1.50	1.50	1.50	1.50
Verifiche con N costante	SI	SI	SI	SI	SI	SI
Fattore di redistribuzione	0.0	0.0	0.0	0.0	0.0	0.0
Modello per il confinamento						
Relazione tensio-deformativa	Mander	Mander	Mander	Mander	Mander	Mander
Incrudimento acciaio	5.000e-03	5.000e-03	5.000e-03	5.000e-03	5.000e-03	5.000e-03
Fattore lambda	1.00	1.00	1.00	1.00	1.00	1.00
epsilon max,s	4.000e-02	4.000e-02	4.000e-02	4.000e-02	4.000e-02	4.000e-02
epsilon cu2	4.500e-03	4.500e-03	4.500e-03	4.500e-03	4.500e-03	4.500e-03
epsilon c2	0.0	0.0	0.0	0.0	0.0	0.0
epsilon cy	0.0	0.0	0.0	0.0	0.0	0.0
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50	97.50	97.50	97.50
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00	2600.00	2600.00	2600.00
Rapporto omogeneizzazione N	15.00	15.00	15.00	15.00	15.00	15.00
Massimo rapporto area compressa/tesa	1.00	1.00	1.00	1.00	1.00	1.00
Staffe						
Diametro staffe	8.00	0.0	0.0	0.0	0.0	0.0
Passo minimo [cm]	4.00	4.00	4.00	4.00	4.00	4.00
Passo massimo [cm]	30.00	30.00	30.00	30.00	30.00	30.00
Passo raffittito [cm]	15.00	15.00	15.00	15.00	15.00	15.00
Lunghezza zona raffittita [cm]	50.00	50.00	50.00	50.00	50.00	50.00
Ctg(Teta) Max	2.50	2.50	2.50	2.50	2.50	2.50
Percentuale sagomati	0.0	0.0	0.0	0.0	0.0	0.0
Luce di taglio per GR [cm]	1.00	1.00	1.00	1.00	1.00	1.00
Adotta scorrimento medio	NO	NO	NO	NO	NO	NO
Torsione non essenziale inclusa	SI	SI	SI	SI	SI	SI

Solai e pannelli	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Usa tensioni ammissibili	NO	NO	NO	NO	NO	NO
Af inf: da traliccio	SI	SI	SI	SI	SI	SI
Consenti armatura a taglio	NO	NO	NO	NO	NO	NO
Incrementa armatura longitudinale per taglio	SI	SI	SI	SI	SI	SI
Af inf: da q*L*L /	20.00	20.00	20.00	20.00	20.00	20.00
Incremento fascia piena [cm]	5.00	5.00	5.00	5.00	5.00	5.00
Armatura						
Minima tesa	0.15	0.15	0.15	0.15	0.15	0.15
Massima tesa	3.00	3.00	3.00	3.00	3.00	3.00
Minima compressa	0.0	0.0	0.0	0.0	0.0	0.0
Af/h [cm]	7.000e-02	7.000e-02	7.000e-02	7.000e-02	7.000e-02	7.000e-02
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4500.00	4500.00	4500.00	4500.00
Tipo acciaio	tipo C	tipo C	tipo C	tipo C	tipo C	tipo C
Coefficiente gamma s	1.15	1.15	1.15	1.15	1.15	1.15
Coefficiente gamma c	1.50	1.50	1.50	1.50	1.50	1.50

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Solai e pannelli	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Fattore di ridistribuzione	0.0	0.0	0.0	0.0	0.0	0.0
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	85.00	85.00	85.00	85.00	85.00	85.00
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00	2600.00	2600.00	2600.00
Rapporto omogeneizzazione N	15.00	15.00	15.00	15.00	15.00	15.00
Massimo rapporto area compressa/tesa	1.00	1.00	1.00	1.00	1.00	1.00
Verifica freccia						
Infinita	250.00	250.00	250.00	250.00	250.00	250.00
Istantanea	500.00	500.00	500.00	500.00	500.00	500.00
Fattore viscosità	3.00	3.00	3.00	3.00	3.00	3.00
Usa J non fessurato	NO	NO	NO	NO	NO	NO
Elementi non strutturali						
Tamponatura antiespulsione	NO	NO	NO	NO	NO	NO
Tamponatura con armatura	NO	NO	NO	NO	NO	NO
Fattore di struttura/comportamento	2.00	2.00	2.00	2.00	2.00	2.00
Coefficiente gamma m	0.0	0.0	0.0	0.0	0.0	0.0
Periodo Ta	0.0	0.0	0.0	0.0	0.0	0.0
Altezza pannello	0.0	0.0	0.0	0.0	0.0	0.0

Legno	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
aste						
Beta assegnato	0.80	0.80	0.80	0.80	0.80	0.80
travi						
3-3 Beta * L automatico	SI	NO	SI	SI	SI	SI
3-3 Beta assegnato	1.00	1.00	1.00	1.00	1.00	1.00
3-3 Beta * L assegnato [cm]	725.00	725.00	725.00	725.00	725.00	725.00
2-2 Beta * L automatico	SI	NO	SI	SI	SI	SI
2-2 Beta assegnato	725.00	725.00	725.00	725.00	725.00	725.00
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0	0.0	0.0	0.0
1-1 Beta * L automatico	SI	SI	SI	SI	SI	SI
1-1 Beta assegnato	1.00	1.00	1.00	1.00	1.00	1.00
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0	0.0	0.0	0.0
pilastr						
Metodo di calcolo 3-3	Assegnato	Assegnato	Assegnato	Assegnato	Assegnato	Assegnato
3-3 Beta assegnato	2.00	2.00	2.00	2.00	2.00	2.00
3-3 Beta * L assegnato [cm]	540.00	380.00	540.00	540.00	540.00	540.00
Metodo di calcolo 2-2	Assegnato	Assegnato	Assegnato	Assegnato	Assegnato	Assegnato
2-2 Beta assegnato	2.00	2.00	2.00	2.00	2.00	2.00
2-2 Beta * L assegnato [cm]	540.00	380.00	540.00	540.00	540.00	540.00
1-1 Beta assegnato	1.00	1.00	1.00	1.00	1.00	1.00
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0	0.0	0.0	0.0
Generalità						
Gamma non sismico	1.45	1.45	1.45	1.45	1.45	1.45
Gamma sismico	1.25	1.25	1.25	1.25	1.25	1.25
Classificazione						
Classe di servizio	1 (bassa umidità)	1 (bassa umidità)	1 (bassa umidità)	1 (bassa umidità)	1 (bassa umidità)	1 (bassa umidità)
Per classe di servizio 1						
Kmod permanente	0.60	0.60	0.60	0.60	0.60	0.60
Kmod lunga	0.70	0.70	0.70	0.70	0.70	0.70
Kmod media	0.80	0.80	0.80	0.80	0.80	0.80
Kmod breve	0.90	0.90	0.90	0.90	0.90	0.90
Kmod istantanea	1.10	1.10	1.10	1.10	1.10	1.10
Kdef	0.60	0.60	0.60	0.60	0.60	0.60
Per classe di servizio 2						
Kmod permanente	0.60	0.60	0.60	0.60	0.60	0.60
Kmod lunga	0.70	0.70	0.70	0.70	0.70	0.70
Kmod media	0.80	0.80	0.80	0.80	0.80	0.80
Kmod breve	0.90	0.90	0.90	0.90	0.90	0.90
Kmod istantanea	1.10	1.10	1.10	1.10	1.10	1.10
Kdef	0.80	0.80	0.80	0.80	0.80	0.80
Per classe di servizio 3						
Kmod permanente	0.50	0.50	0.50	0.50	0.50	0.50
Kmod lunga	0.55	0.55	0.55	0.55	0.55	0.55

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Legno	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Kmod media	0.65	0.65	0.65	0.65	0.65	0.65
Kmod breve	0.70	0.70	0.70	0.70	0.70	0.70
Kmod istantanea	0.90	0.90	0.90	0.90	0.90	0.90
Kdef	2.00	2.00	2.00	2.00	2.00	2.00

XLAM	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
L direzione 1 [*] [cm]	1.00	1.00	1.00	1.00	1.00	1.00
L direzione 2 [cm]	0.0	0.0	0.0	0.0	0.0	0.0
Verifica V da D.38	NO	NO	NO	NO	NO	NO
Verifica M da M.5-45	NO	NO	NO	NO	NO	NO
Media valori elementi	SI	SI	SI	SI	SI	SI
Connessioni pareti						
rvpk [daN/cm]	50.00	50.00	60.00	60.00	25.00	35.00
rvtk [daN/cm]	50.00	50.00	50.00	50.00	50.00	50.00
rvlk [daN/cm]	100.00	50.00	100.00	100.00	100.00	100.00
RHk [daN]	4200.00	4200.00	8400.00	4200.00	4200.00	4200.00
dH [cm]	25.00	25.00	25.00	25.00	25.00	25.00
fcH90k [daN/cm2]	20.00	20.00	20.00	20.00	20.00	20.00
Pannelli solaio						
f ist<L/	300.00	500.00	300.00	300.00	300.00	300.00
f inf<L/	250.00	350.00	250.00	250.00	250.00	250.00
Verifica vibrazioni (EC5 7.3)	NO	NO	NO	NO	NO	NO
E massetto collaborante [daN/cm2]	200000.00	200000.00	200000.00	200000.00	200000.00	200000.00
t massetto collaborante [cm]	1.000e-02	4.00	1.000e-02	1.000e-02	1.000e-02	1.000e-02
Smorzamento percentuale	0.0	0.0	0.0	0.0	0.0	0.0
Resistenza al fuoco						
Spessore carbonizzazione [cm]	0.0	0.0	0.0	0.0	0.0	0.0
3- intradosso	NO	NO	NO	NO	NO	NO
3+ estradosso	NO	NO	NO	NO	NO	NO

3. MODELLAZIONE DELLE SEZIONI

LEGENDA TABELLA DATI SEZIONI

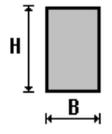
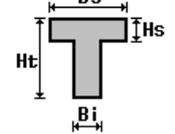
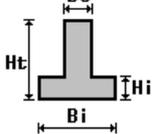
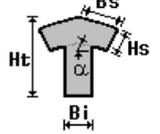
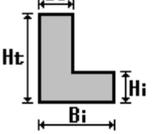
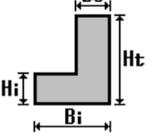
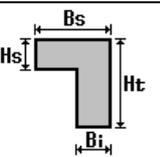
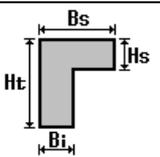
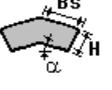
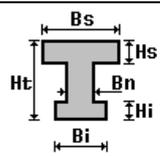
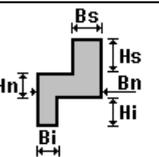
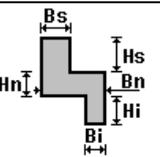
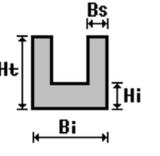
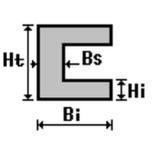
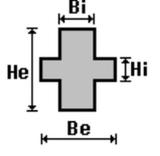
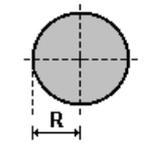
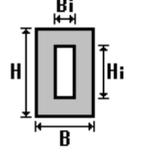
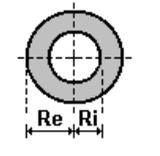
Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

1. sezione di tipo generico
2. profilati semplici
3. profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

Area	area della sezione
A V2	area della sezione/fattore di taglio (per il taglio in direzione 2)
A V3	area della sezione/fattore di taglio (per il taglio in direzione 3)
Jt	fattore torsionale di rigidità
J2-2	momento d'inerzia della sezione riferito all'asse 2
J3-3	momento d'inerzia della sezione riferito all'asse 3
W2-2	modulo di resistenza della sezione riferito all'asse 2
W3-3	modulo di resistenza della sezione riferito all'asse 3
Wp2-2	modulo di resistenza plastico della sezione riferito all'asse 2
Wp3-3	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidità degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

 rettangolare	 a T	 a T rovescia	 a T di colmo	 a L	 a L specchiata
 a L specchiata rovescia	 a L rovescia	 a L di colmo	 a doppio T	 a quattro specchiata	 a quattro
 a U	 a C	 a croce	 circolare	 rettangolare cava	 circolare cava



Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):
 i valori dimensionali con prefisso B sono riferiti all'asse 2
 i valori dimensionali con prefisso H sono riferiti all'asse 3

Id	Tipo	Area	A V2	A V3	Jt	J 2-2	J 3-3	W 2-2	W 3-3	Wp 2-2	Wp 3-3
		cm2	cm2	cm2	cm4	cm4	cm4	cm3	cm3	cm3	cm3
1	pil legno-Rettangolare: b=16 h=40	640.00	533.33	533.33	4.085e+04	1.365e+04	8.533e+04	1706.67	4266.67	2560.00	6400.00
2	trave legno-Rettangolare: b=16 h=50	800.00	666.67	666.67	5.450e+04	1.707e+04	1.667e+05	2133.33	6666.67	3200.00	1.000e+04
4	FITTIZIA-Rettangolare: b=10 h=10	100.00	83.33	83.33	1405.68	833.33	833.33	166.67	166.67	250.00	250.00
5	FONDAZIONE-T rovescia: bi=100 ht=109 bs=30 hi=40	6070.00	0.0	0.0	2.407e+06	3.489e+06	5.406e+06	6.977e+04	7.678e+04	1.155e+05	1.421e+05
6	FONDAZIONE-T rovescia: bi=100 ht=109 bs=60 hi=40	8140.00	0.0	0.0	6.722e+06	4.575e+06	8.219e+06	9.151e+04	1.341e+05	1.621e+05	2.227e+05

4. MODELLAZIONE STRUTTURA: NODI

LEGENDA TABELLA DATI NODI

Il programma utilizza per la modellazione nodi strutturali.

Ogni nodo è individuato dalle coordinate cartesiane nel sistema di riferimento globale (X Y Z).

Ad ogni nodo è eventualmente associato un codice di vincolamento rigido, un codice di fondazione speciale, ed un set di sei molle (tre per le traslazioni, tre per le rotazioni). Le tabelle sottoriportate riflettono le succitate possibilità. In particolare per ogni nodo viene indicato in tabella:

Nodo	numero del nodo.
X	valore della coordinata X
Y	valore della coordinata Y
Z	valore della coordinata Z

Per i nodi ai quali sia associato un codice di vincolamento rigido, un codice di fondazione speciale o un set di molle viene indicato in tabella:

Nodo	numero del nodo.
X	valore della coordinata X
Y	valore della coordinata Y
Z	valore della coordinata Z
Note	eventuale codice di vincolo (es. v=110010 sei valori relativi ai sei gradi di libertà previsti per il nodo TxTyTzRxRyRz, il valore 1 indica che lo spostamento o rotazione relativo è impedito, il valore 0 indica che lo spostamento o rotazione relativo è libero).
Note	(FS = 1, 2,...) eventuale codice del tipo di fondazione speciale (1, 2,... fanno riferimento alle tipologie: plinto, palo, plinto su pali,...) che è collegato al nodo. (ISO = "id SIGLA") indice e sigla identificativa dell' eventuale isolatore sismico assegnato al nodo
Rig. TX	valore della rigidezza dei vincoli elastici eventualmente applicati al nodo, nello specifico TX (idem per TY, TZ, RX, RY, RZ).

Per strutture sismicamente isolate viene inoltre inserita la tabella delle caratteristiche per gli isolatori utilizzati; le caratteristiche sono indicate in conformità al cap. 7.10 del D.M. 17/01/18

TABELLA DATI NODI

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
	cm	cm	cm		cm	cm	cm		cm	cm	cm
1	-22.1	588.5	0.0	2	-12.6	588.5	0.0	3	64.9	588.5	0.0
4	142.4	588.5	0.0	5	219.9	588.5	0.0	6	297.4	588.5	0.0
7	374.9	588.5	0.0	8	452.4	588.5	0.0	9	529.9	588.5	0.0
10	607.4	588.5	0.0	11	684.9	588.5	0.0	12	762.4	588.5	0.0
13	772.4	588.5	0.0	14	848.9	588.5	0.0	15	934.9	588.5	0.0
16	1020.9	588.5	0.0	17	1076.6	588.5	0.0	18	1132.2	588.5	0.0
19	1187.9	588.5	0.0	20	1213.4	588.5	0.0	21	1308.4	588.5	0.0
22	1371.6	588.5	0.0	23	1434.7	588.5	0.0	24	1497.9	588.5	0.0
25	1541.4	588.5	0.0	26	1626.9	588.5	0.0	27	1712.4	588.5	0.0
28	1786.5	588.5	0.0	29	1860.6	588.5	0.0	30	1934.7	588.5	0.0
31	2008.8	588.5	0.0	32	2082.9	588.5	0.0	33	2467.9	588.5	0.0
34	2524.6	588.5	0.0	35	2581.2	588.5	0.0	36	2637.9	588.5	0.0
37	2714.6	588.5	0.0	38	2791.2	588.5	0.0	39	2867.9	588.5	0.0
40	2922.9	588.5	0.0	41	2977.9	588.5	0.0	42	3062.2	588.5	0.0
43	3146.5	588.5	0.0	44	3230.8	588.5	0.0	45	3315.1	588.5	0.0
46	3399.3	588.5	0.0	47	3483.6	588.5	0.0	48	3567.9	588.5	0.0
49	3643.6	588.5	0.0	50	3719.2	588.5	0.0	51	3794.9	588.5	0.0
52	4005.4	588.5	0.0	53	4066.2	588.5	0.0	54	4127.1	588.5	0.0
55	4187.9	588.5	0.0	56	2977.9	637.1	0.0	57	1187.9	646.9	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



58	-22.1	649.1	0.0	59	3567.9	653.1	0.0	60	4187.9	659.0	0.0
61	772.4	659.4	0.0	62	2467.9	659.8	0.0	63	2082.9	660.8	0.0
64	1497.9	666.3	0.0	65	2977.9	685.6	0.0	66	1187.9	705.3	0.0
67	-22.1	709.6	0.0	68	4187.9	729.5	0.0	69	772.4	730.3	0.0
70	2467.9	731.1	0.0	71	2082.9	733.1	0.0	72	1497.9	744.1	0.0
73	3567.9	747.1	0.0	74	1187.9	763.7	0.0	75	3567.9	780.1	0.0
76	2977.9	790.6	0.0	77	4187.9	800.1	0.0	78	772.4	801.2	0.0
79	2467.9	802.5	0.0	80	2082.9	805.5	0.0	81	1497.9	821.8	0.0
82	1187.9	822.1	0.0	83	-22.1	849.6	0.0	84	2977.9	868.0	0.0
85	4187.9	870.6	0.0	86	772.4	872.1	0.0	87	2467.9	873.8	0.0
88	3567.9	875.1	0.0	89	2082.9	877.8	0.0	90	1497.9	899.6	0.0
91	1187.9	917.1	0.0	92	-22.1	922.8	0.0	93	4187.9	941.1	0.0
94	772.4	942.9	0.0	95	2977.9	945.4	0.0	96	3567.9	947.6	0.0
97	2082.9	950.1	0.0	98	2467.9	950.1	0.0	99	1497.9	977.4	0.0
100	1187.9	991.4	0.0	101	-22.1	995.9	0.0	102	772.4	1013.8	0.0
103	3567.9	1020.1	0.0	104	2977.9	1022.8	0.0	105	1497.9	1055.2	0.0
106	1187.9	1065.7	0.0	107	-22.1	1069.1	0.0	108	4187.9	1069.1	0.0
109	772.4	1084.7	0.0	110	3567.9	1092.6	0.0	111	2977.9	1100.2	0.0
112	1497.9	1133.0	0.0	113	1187.9	1139.9	0.0	114	-22.1	1142.2	0.0
115	4187.9	1142.2	0.0	116	772.4	1155.6	0.0	117	2977.9	1177.6	0.0
118	1497.9	1210.7	0.0	119	1187.9	1214.2	0.0	120	-22.1	1215.4	0.0
121	4187.9	1215.4	0.0	122	772.4	1250.6	0.0	123	2977.9	1262.6	0.0
124	3567.9	1264.1	0.0	125	-142.1	1288.5	0.0	126	-82.1	1288.5	0.0
127	-22.1	1288.5	0.0	128	597.9	1288.5	0.0	129	663.2	1288.5	0.0
130	728.5	1288.5	0.0	131	772.4	1288.5	0.0	132	793.8	1288.5	0.0
133	859.1	1288.5	0.0	134	892.9	1288.5	0.0	135	924.4	1288.5	0.0
136	1024.4	1288.5	0.0	137	1106.2	1288.5	0.0	138	1187.9	1288.5	0.0
139	1265.4	1288.5	0.0	140	1342.9	1288.5	0.0	141	1420.4	1288.5	0.0
142	1497.9	1288.5	0.0	143	1575.4	1288.5	0.0	144	1652.9	1288.5	0.0
145	1730.4	1288.5	0.0	146	1807.9	1288.5	0.0	147	1884.4	1288.5	0.0
148	1979.4	1288.5	0.0	149	2031.2	1288.5	0.0	150	2082.9	1288.5	0.0
151	2103.9	1288.5	0.0	152	2357.9	1288.5	0.0	153	2443.9	1288.5	0.0
154	2467.9	1288.5	0.0	155	2546.0	1288.5	0.0	156	2641.0	1288.5	0.0
157	2667.9	1288.5	0.0	158	2745.4	1288.5	0.0	159	2822.9	1288.5	0.0
160	2900.4	1288.5	0.0	161	2977.9	1288.5	0.0	162	3051.7	1288.5	0.0
163	3125.4	1288.5	0.0	164	3199.2	1288.5	0.0	165	3272.9	1288.5	0.0
166	3353.4	1288.5	0.0	167	3433.9	1288.5	0.0	168	3567.9	1288.5	0.0
169	3637.9	1288.5	0.0	170	3707.9	1288.5	0.0	171	3777.9	1288.5	0.0
172	3847.9	1288.5	0.0	173	3917.9	1288.5	0.0	174	3987.9	1288.5	0.0
175	4057.9	1288.5	0.0	176	4122.9	1288.5	0.0	177	4187.9	1288.5	0.0
178	4057.9	1355.3	0.0	179	-142.1	1358.9	0.0	180	3567.9	1372.8	0.0
181	597.9	1376.5	0.0	182	4057.9	1422.1	0.0	183	-142.1	1429.3	0.0
184	3567.9	1457.0	0.0	185	597.9	1466.0	0.0	186	4057.9	1488.9	0.0
187	-142.1	1499.7	0.0	188	3567.9	1541.3	0.0	189	597.9	1552.5	0.0
190	4057.9	1555.7	0.0	191	-142.1	1570.1	0.0	192	4057.9	1622.5	0.0
193	3567.9	1625.5	0.0	194	-142.1	1640.5	0.0	195	597.9	1640.5	0.0
196	3567.9	1708.0	0.0	197	4057.9	1709.0	0.0	198	-142.1	1780.5	0.0
199	597.9	1780.5	0.0	200	3567.9	1790.5	0.0	201	4057.9	1795.5	0.0
202	-142.1	1808.5	0.0	203	-59.9	1808.5	0.0	204	22.4	1808.5	0.0
205	104.6	1808.5	0.0	206	186.8	1808.5	0.0	207	269.0	1808.5	0.0
208	351.2	1808.5	0.0	209	433.5	1808.5	0.0	210	515.7	1808.5	0.0
211	597.9	1808.5	0.0	212	3567.9	1808.5	0.0	213	3614.9	1808.5	0.0
214	3719.9	1808.5	0.0	215	3787.5	1808.5	0.0	216	3855.1	1808.5	0.0
217	3922.7	1808.5	0.0	218	3990.3	1808.5	0.0	219	4057.9	1808.5	0.0
220	-142.1	1833.6	0.0	221	4057.9	1833.6	0.0	222	-142.1	1973.6	0.0
223	4057.9	1973.6	0.0	224	-142.1	1998.5	0.0	225	-82.1	1998.5	0.0
226	-22.1	1998.5	0.0	227	42.7	1998.5	0.0	228	107.5	1998.5	0.0
229	172.3	1998.5	0.0	230	237.0	1998.5	0.0	231	301.8	1998.5	0.0
232	366.6	1998.5	0.0	233	431.4	1998.5	0.0	234	561.4	1998.5	0.0
235	597.9	1998.5	0.0	236	671.7	1998.5	0.0	237	745.4	1998.5	0.0
238	819.2	1998.5	0.0	239	892.9	1998.5	0.0	240	966.7	1998.5	0.0
241	1040.4	1998.5	0.0	242	1114.2	1998.5	0.0	243	1187.9	1998.5	0.0
244	1244.4	1998.5	0.0	245	1374.4	1998.5	0.0	246	1436.2	1998.5	0.0
247	1497.9	1998.5	0.0	248	1558.9	1998.5	0.0	249	1622.2	1998.5	0.0
250	1685.6	1998.5	0.0	251	1748.9	1998.5	0.0	252	1784.4	1998.5	0.0
253	1807.9	1998.5	0.0	254	1819.9	1998.5	0.0	255	2082.9	1998.5	0.0
256	2345.9	1998.5	0.0	257	2357.9	1998.5	0.0	258	2390.9	1998.5	0.0
259	2423.9	1998.5	0.0	260	2485.6	1998.5	0.0	261	2547.2	1998.5	0.0
262	2608.9	1998.5	0.0	263	2667.9	1998.5	0.0	264	2744.2	1998.5	0.0
265	2820.4	1998.5	0.0	266	2950.4	1998.5	0.0	267	2977.9	1998.5	0.0
268	3051.7	1998.5	0.0	269	3125.4	1998.5	0.0	270	3199.2	1998.5	0.0
271	3272.9	1998.5	0.0	272	3352.9	1998.5	0.0	273	3432.9	1998.5	0.0
274	3500.4	1998.5	0.0	275	3567.9	1998.5	0.0	276	3597.4	1998.5	0.0
277	3737.4	1998.5	0.0	278	3817.5	1998.5	0.0	279	3897.7	1998.5	0.0
280	3977.8	1998.5	0.0	281	4057.9	1998.5	0.0	282	4122.9	1998.5	0.0
283	4187.9	1998.5	0.0	284	597.9	2070.6	0.0	285	1187.9	2070.6	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



286	3567.9	2070.6	0.0	287	2977.9	2075.6	0.0	288	-22.1	2077.2	0.0
289	1807.9	2077.2	0.0	290	2357.9	2077.2	0.0	291	4187.9	2077.2	0.0
292	-22.1	2155.8	0.0	293	1807.9	2155.8	0.0	294	2357.9	2155.8	0.0
295	4187.9	2155.8	0.0	296	-22.1	2234.4	0.0	297	1807.9	2234.4	0.0
298	2357.9	2234.4	0.0	299	4187.9	2234.4	0.0	300	-22.1	2313.1	0.0
301	1807.9	2313.1	0.0	302	2357.9	2313.1	0.0	303	4187.9	2313.1	0.0
304	1187.9	2328.1	0.0	305	2977.9	2328.1	0.0	306	597.9	2333.1	0.0
307	3567.9	2333.1	0.0	308	-22.1	2391.7	0.0	309	1807.9	2391.7	0.0
310	2357.9	2391.7	0.0	311	4187.9	2391.7	0.0	312	597.9	2411.1	0.0
313	1187.9	2411.1	0.0	314	2977.9	2411.1	0.0	315	3567.9	2411.1	0.0
316	-22.1	2470.3	0.0	317	1807.9	2470.3	0.0	318	2357.9	2470.3	0.0
319	4187.9	2470.3	0.0	320	597.9	2489.1	0.0	321	1187.9	2489.1	0.0
322	2977.9	2489.1	0.0	323	3567.9	2489.1	0.0	324	-22.1	2549.0	0.0
325	1807.9	2549.0	0.0	326	2357.9	2549.0	0.0	327	4187.9	2549.0	0.0
328	1187.9	2562.1	0.0	329	3567.9	2562.1	0.0	330	597.9	2567.1	0.0
331	2977.9	2567.1	0.0	332	-22.1	2627.6	0.0	333	1807.9	2627.6	0.0
334	2357.9	2627.6	0.0	335	4187.9	2627.6	0.0	336	597.9	2662.1	0.0
337	2977.9	2662.1	0.0	338	1187.9	2667.1	0.0	339	3567.9	2667.1	0.0
340	-22.1	2706.2	0.0	341	1807.9	2706.2	0.0	342	2357.9	2706.2	0.0
343	4187.9	2706.2	0.0	344	597.9	2729.2	0.0	345	1187.9	2729.2	0.0
346	2977.9	2729.2	0.0	347	3567.9	2729.2	0.0	348	-22.1	2784.9	0.0
349	1807.9	2784.9	0.0	350	2357.9	2784.9	0.0	351	4187.9	2784.9	0.0
352	597.9	2796.4	0.0	353	1187.9	2796.4	0.0	354	2977.9	2796.4	0.0
355	3567.9	2796.4	0.0	356	-22.1	2863.5	0.0	357	59.9	2863.5	0.0
358	574.9	2863.5	0.0	359	597.9	2863.5	0.0	360	1187.9	2863.5	0.0
361	1213.9	2863.5	0.0	362	1733.9	2863.5	0.0	363	1758.9	2863.5	0.0
364	1807.9	2863.5	0.0	365	1821.9	2863.5	0.0	366	2341.9	2863.5	0.0
367	2357.9	2863.5	0.0	368	2406.9	2863.5	0.0	369	2431.9	2863.5	0.0
370	2951.9	2863.5	0.0	371	2977.9	2863.5	0.0	372	3567.9	2863.5	0.0
373	3590.9	2863.5	0.0	374	4115.9	2863.5	0.0	375	4187.9	2863.5	0.0
376	597.9	2903.4	0.0	377	2977.9	2903.4	0.0	378	3567.9	2903.4	0.0
379	1187.9	2908.4	0.0	380	-22.1	2930.2	0.0	381	4187.9	2930.2	0.0
382	-22.1	2996.9	0.0	383	4187.9	2996.9	0.0	384	1758.9	3020.6	0.0
385	1940.9	3020.6	0.0	386	2224.9	3020.6	0.0	387	2406.9	3020.6	0.0
388	597.9	3038.4	0.0	389	1187.9	3038.4	0.0	390	2977.9	3038.4	0.0
391	3567.9	3038.4	0.0	392	-22.1	3063.6	0.0	393	50.9	3063.6	0.0
394	597.9	3063.6	0.0	395	671.7	3063.6	0.0	396	745.4	3063.6	0.0
397	819.2	3063.6	0.0	398	892.9	3063.6	0.0	399	966.7	3063.6	0.0
400	1040.4	3063.6	0.0	401	1114.2	3063.6	0.0	402	1187.9	3063.6	0.0
403	1758.9	3063.6	0.0	404	1819.6	3063.6	0.0	405	1880.2	3063.6	0.0
406	1940.9	3063.6	0.0	407	2224.9	3063.6	0.0	408	2285.6	3063.6	0.0
409	2346.2	3063.6	0.0	410	2406.9	3063.6	0.0	411	2977.9	3063.6	0.0
412	3051.7	3063.6	0.0	413	3125.4	3063.6	0.0	414	3199.2	3063.6	0.0
415	3272.9	3063.6	0.0	416	3346.7	3063.6	0.0	417	3420.4	3063.6	0.0
418	3494.2	3063.6	0.0	419	3567.9	3063.6	0.0	420	4114.9	3063.6	0.0
421	4187.9	3063.6	0.0	3229	1817.1	3020.6	0.0	3230	2348.7	3020.6	0.0

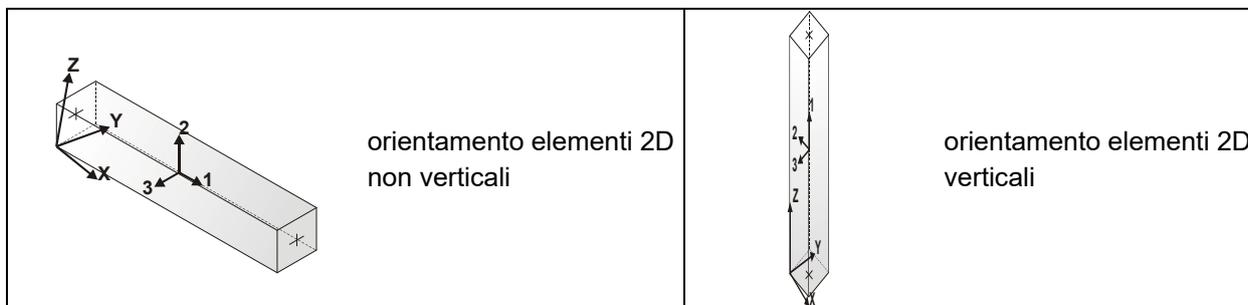
5. MODELLAZIONE STRUTTURA: ELEMENTI TRAVE

TABELLA DATI TRAVI

Il programma utilizza per la modellazione elementi a due nodi denominati in generale travi.

Ogni elemento trave è individuato dal nodo iniziale e dal nodo finale.

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: trave, trave di fondazione, pilastro, asta, asta tesa, asta compressa,
Nodo I (J)	numero del nodo iniziale (finale)
Mat.	codice del materiale assegnato all'elemento
Sez.	codice della sezione assegnata all'elemento
Rotaz.	valore della rotazione dell'elemento, attorno al proprio asse, nel caso in cui l'orientamento di default non sia adottabile; l'orientamento di default prevede per gli elementi non verticali l'asse 2 contenuto nel piano verticale e l'asse 3 orizzontale, per gli elementi verticali l'asse 2 diretto secondo X negativo e l'asse 3 diretto secondo Y negativo
Svincolo I (J)	codici di svincolo per le azioni interne; i primi sei codici si riferiscono al nodo iniziale, i restanti sei al nodo finale (il valore 1 indica che la relativa azione interna non è attiva)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione della trave su suolo elastico
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Crit.	Rotaz. gradi	Svincolo I	Svincolo J	Wink V daN/cm3	Wink O daN/cm3
105	Trave f.	19	57	3	5	1				0.30	1.00
106	Trave f.	24	64	3	5	1				0.30	1.00
107	Trave f.	257	290	3	5	1				0.30	1.00
108	Trave f.	360	361	3	5	1				0.30	1.00
109	Trave f.	138	243	3	5	1				0.30	1.00
110	Trave f.	32	63	3	5	1				0.30	1.00
111	Trave f.	212	213	3	5	1				0.30	1.00
112	Trave f.	152	257	3	5	1				0.30	1.00
113	Trave f.	202	203	3	5	1				0.30	1.00
114	Trave f.	146	253	3	5	1				0.30	1.00
115	Trave f.	13	61	3	5	1				0.30	1.00
116	Trave f.	356	357	3	5	1				0.30	1.00
117	Trave f.	372	373	3	5	1				0.30	1.00
124	Trave f.	226	288	3	5	1				0.30	1.00
125	Trave f.	224	225	3	5	1				0.30	1.00
126	Trave f.	125	179	3	5	1				0.30	1.00
127	Trave f.	125	126	3	5	1				0.30	1.00
128	Trave f.	1	58	3	5	1				0.30	1.00
129	Trave f.	1	2	3	5	1				0.30	1.00
130	Trave f.	55	60	3	5	1				0.30	1.00
131	Trave f.	127	128	3	5	1				0.30	1.00
132	Trave f.	392	393	3	5	1				0.30	1.00
133	Trave f.	283	291	3	5	1				0.30	1.00
134	Trave f.	226	227	3	5	1				0.30	1.00
135	Trave f.	128	181	3	5	1				0.30	1.00
136	Trave f.	243	285	3	5	1				0.30	1.00
137	Trave f.	253	289	3	5	1				0.30	1.00
138	Trave f.	48	59	3	5	1				0.30	1.00
139	Trave f.	175	178	3	5	1				0.30	1.00
140	Trave f.	267	287	3	5	1				0.30	1.00
141	Trave f.	161	267	3	5	1				0.30	1.00
142	Trave f.	41	56	3	5	1				0.30	1.00
143	Trave f.	33	62	3	5	1				0.30	1.00
144	Trave f.	97	150	3	5	1				0.30	1.00
145	Trave f.	98	154	3	5	1				0.30	1.00
146	Trave f.	57	66	3	5	1				0.30	1.00
147	Trave f.	64	72	3	5	1				0.30	1.00
148	Trave f.	290	294	3	5	1				0.30	1.00
149	Trave f.	361	362	3	5	1				0.30	1.00
150	Trave f.	63	71	3	5	1				0.30	1.00
151	Trave f.	213	214	3	5	1				0.30	1.00
152	Trave f.	203	204	3	5	1				0.30	1.00
153	Trave f.	61	69	3	5	1				0.30	1.00
154	Trave f.	357	358	3	5	1				0.30	1.00
155	Trave f.	373	374	3	5	1				0.30	1.00
156	Trave f.	288	292	3	5	1				0.30	1.00
157	Trave f.	225	226	3	5	1				0.30	1.00
158	Trave f.	179	183	3	5	1				0.30	1.00
159	Trave f.	126	127	3	5	1				0.30	1.00
160	Trave f.	58	67	3	5	1				0.30	1.00
161	Trave f.	2	3	3	5	1				0.30	1.00
162	Trave f.	60	68	3	5	1				0.30	1.00
163	Trave f.	128	129	3	6	1				0.30	1.00
164	Trave f.	393	394	3	5	1				0.30	1.00
165	Trave f.	291	295	3	5	1				0.30	1.00
166	Trave f.	227	228	3	5	1				0.30	1.00
167	Trave f.	181	185	3	5	1				0.30	1.00
168	Trave f.	285	304	3	5	1				0.30	1.00
169	Trave f.	289	293	3	5	1				0.30	1.00
170	Trave f.	59	73	3	5	1				0.30	1.00
171	Trave f.	178	182	3	5	1				0.30	1.00
172	Trave f.	287	305	3	5	1				0.30	1.00
173	Trave f.	56	65	3	5	1				0.30	1.00
174	Trave f.	62	70	3	5	1				0.30	1.00
175	Trave f.	66	74	3	5	1				0.30	1.00
176	Trave f.	72	81	3	5	1				0.30	1.00
177	Trave f.	294	298	3	5	1				0.30	1.00
178	Trave f.	362	363	3	5	1				0.30	1.00
179	Trave f.	71	80	3	5	1				0.30	1.00
180	Trave f.	214	215	3	5	1				0.30	1.00
181	Trave f.	204	205	3	5	1				0.30	1.00
182	Trave f.	69	78	3	5	1				0.30	1.00

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



183	Trave f.	358	359	3	5	1	0.30	1.00
184	Trave f.	374	375	3	5	1	0.30	1.00
185	Trave f.	292	296	3	5	1	0.30	1.00
186	Trave f.	183	187	3	5	1	0.30	1.00
187	Trave f.	67	83	3	5	1	0.30	1.00
188	Trave f.	3	4	3	5	1	0.30	1.00
189	Trave f.	68	77	3	5	1	0.30	1.00
190	Trave f.	129	130	3	6	1	0.30	1.00
191	Trave f.	394	395	3	5	1	0.30	1.00
192	Trave f.	295	299	3	5	1	0.30	1.00
193	Trave f.	228	229	3	5	1	0.30	1.00
194	Trave f.	185	189	3	5	1	0.30	1.00
195	Trave f.	304	313	3	5	1	0.30	1.00
196	Trave f.	293	297	3	5	1	0.30	1.00
197	Trave f.	73	75	3	5	1	0.30	1.00
198	Trave f.	182	186	3	5	1	0.30	1.00
199	Trave f.	305	314	3	5	1	0.30	1.00
200	Trave f.	65	76	3	5	1	0.30	1.00
201	Trave f.	70	79	3	5	1	0.30	1.00
202	Trave f.	74	82	3	5	1	0.30	1.00
203	Trave f.	81	90	3	5	1	0.30	1.00
204	Trave f.	298	302	3	5	1	0.30	1.00
205	Trave f.	363	364	3	5	1	0.30	1.00
206	Trave f.	80	89	3	5	1	0.30	1.00
207	Trave f.	215	216	3	5	1	0.30	1.00
208	Trave f.	205	206	3	5	1	0.30	1.00
209	Trave f.	78	86	3	5	1	0.30	1.00
210	Trave f.	296	300	3	5	1	0.30	1.00
211	Trave f.	187	191	3	5	1	0.30	1.00
212	Trave f.	83	92	3	5	1	0.30	1.00
213	Trave f.	4	5	3	5	1	0.30	1.00
214	Trave f.	77	85	3	5	1	0.30	1.00
215	Trave f.	130	131	3	6	1	0.30	1.00
216	Trave f.	395	396	3	5	1	0.30	1.00
217	Trave f.	299	303	3	5	1	0.30	1.00
218	Trave f.	229	230	3	5	1	0.30	1.00
219	Trave f.	189	195	3	5	1	0.30	1.00
220	Trave f.	313	321	3	5	1	0.30	1.00
221	Trave f.	297	301	3	5	1	0.30	1.00
222	Trave f.	75	88	3	5	1	0.30	1.00
223	Trave f.	186	190	3	5	1	0.30	1.00
224	Trave f.	314	322	3	5	1	0.30	1.00
225	Trave f.	76	84	3	5	1	0.30	1.00
226	Trave f.	79	87	3	5	1	0.30	1.00
227	Trave f.	82	91	3	5	1	0.30	1.00
228	Trave f.	90	99	3	5	1	0.30	1.00
229	Trave f.	302	310	3	5	1	0.30	1.00
230	Trave f.	364	365	3	5	1	0.30	1.00
231	Trave f.	89	97	3	5	1	0.30	1.00
232	Trave f.	216	217	3	5	1	0.30	1.00
233	Trave f.	206	207	3	5	1	0.30	1.00
234	Trave f.	86	94	3	5	1	0.30	1.00
235	Trave f.	300	308	3	5	1	0.30	1.00
236	Trave f.	191	194	3	5	1	0.30	1.00
237	Trave f.	92	101	3	5	1	0.30	1.00
238	Trave f.	5	6	3	5	1	0.30	1.00
239	Trave f.	85	93	3	5	1	0.30	1.00
240	Trave f.	131	132	3	6	1	0.30	1.00
241	Trave f.	396	397	3	5	1	0.30	1.00
242	Trave f.	303	311	3	5	1	0.30	1.00
243	Trave f.	230	231	3	5	1	0.30	1.00
244	Trave f.	195	199	3	5	1	0.30	1.00
245	Trave f.	321	328	3	5	1	0.30	1.00
246	Trave f.	301	309	3	5	1	0.30	1.00
247	Trave f.	88	96	3	5	1	0.30	1.00
248	Trave f.	190	192	3	5	1	0.30	1.00
249	Trave f.	322	331	3	5	1	0.30	1.00
250	Trave f.	84	95	3	5	1	0.30	1.00
251	Trave f.	87	98	3	5	1	0.30	1.00
252	Trave f.	91	100	3	5	1	0.30	1.00
253	Trave f.	99	105	3	5	1	0.30	1.00
254	Trave f.	310	318	3	5	1	0.30	1.00
255	Trave f.	365	366	3	5	1	0.30	1.00
256	Trave f.	217	218	3	5	1	0.30	1.00
257	Trave f.	207	208	3	5	1	0.30	1.00
258	Trave f.	94	102	3	5	1	0.30	1.00

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



259	Trave f.	308	316	3	5	1	0.30	1.00
260	Trave f.	194	198	3	5	1	0.30	1.00
261	Trave f.	101	107	3	5	1	0.30	1.00
262	Trave f.	6	7	3	5	1	0.30	1.00
263	Trave f.	93	108	3	5	1	0.30	1.00
264	Trave f.	132	133	3	6	1	0.30	1.00
265	Trave f.	397	398	3	5	1	0.30	1.00
266	Trave f.	311	319	3	5	1	0.30	1.00
267	Trave f.	231	232	3	5	1	0.30	1.00
268	Trave f.	199	211	3	5	1	0.30	1.00
269	Trave f.	328	338	3	5	1	0.30	1.00
270	Trave f.	309	317	3	5	1	0.30	1.00
271	Trave f.	96	103	3	5	1	0.30	1.00
272	Trave f.	192	197	3	5	1	0.30	1.00
273	Trave f.	331	337	3	5	1	0.30	1.00
274	Trave f.	95	104	3	5	1	0.30	1.00
275	Trave f.	100	106	3	5	1	0.30	1.00
276	Trave f.	105	112	3	5	1	0.30	1.00
277	Trave f.	318	326	3	5	1	0.30	1.00
278	Trave f.	366	367	3	5	1	0.30	1.00
279	Trave f.	218	219	3	5	1	0.30	1.00
280	Trave f.	208	209	3	5	1	0.30	1.00
281	Trave f.	102	109	3	5	1	0.30	1.00
282	Trave f.	316	324	3	5	1	0.30	1.00
283	Trave f.	198	202	3	5	1	0.30	1.00
284	Trave f.	107	114	3	5	1	0.30	1.00
285	Trave f.	7	8	3	5	1	0.30	1.00
286	Trave f.	108	115	3	5	1	0.30	1.00
287	Trave f.	133	134	3	6	1	0.30	1.00
288	Trave f.	398	399	3	5	1	0.30	1.00
289	Trave f.	319	327	3	5	1	0.30	1.00
290	Trave f.	232	233	3	5	1	0.30	1.00
291	Trave f.	211	235	3	5	1	0.30	1.00
292	Trave f.	338	345	3	5	1	0.30	1.00
293	Trave f.	317	325	3	5	1	0.30	1.00
294	Trave f.	103	110	3	5	1	0.30	1.00
295	Trave f.	197	201	3	5	1	0.30	1.00
296	Trave f.	337	346	3	5	1	0.30	1.00
297	Trave f.	104	111	3	5	1	0.30	1.00
298	Trave f.	106	113	3	5	1	0.30	1.00
299	Trave f.	112	118	3	5	1	0.30	1.00
300	Trave f.	326	334	3	5	1	0.30	1.00
301	Trave f.	367	368	3	5	1	0.30	1.00
302	Trave f.	209	210	3	5	1	0.30	1.00
303	Trave f.	109	116	3	5	1	0.30	1.00
304	Trave f.	324	332	3	5	1	0.30	1.00
305	Trave f.	202	220	3	5	1	0.30	1.00
306	Trave f.	114	120	3	5	1	0.30	1.00
307	Trave f.	8	9	3	5	1	0.30	1.00
308	Trave f.	115	121	3	5	1	0.30	1.00
309	Trave f.	134	135	3	6	1	0.30	1.00
310	Trave f.	399	400	3	5	1	0.30	1.00
311	Trave f.	327	335	3	5	1	0.30	1.00
312	Trave f.	233	234	3	5	1	0.30	1.00
313	Trave f.	235	284	3	5	1	0.30	1.00
314	Trave f.	345	353	3	5	1	0.30	1.00
315	Trave f.	325	333	3	5	1	0.30	1.00
316	Trave f.	110	124	3	5	1	0.30	1.00
317	Trave f.	201	219	3	5	1	0.30	1.00
318	Trave f.	346	354	3	5	1	0.30	1.00
319	Trave f.	111	117	3	5	1	0.30	1.00
320	Trave f.	113	119	3	5	1	0.30	1.00
321	Trave f.	118	142	3	5	1	0.30	1.00
322	Trave f.	334	342	3	5	1	0.30	1.00
323	Trave f.	368	369	3	5	1	0.30	1.00
324	Trave f.	210	211	3	5	1	0.30	1.00
325	Trave f.	116	122	3	5	1	0.30	1.00
326	Trave f.	332	340	3	5	1	0.30	1.00
327	Trave f.	220	222	3	5	1	0.30	1.00
328	Trave f.	120	127	3	5	1	0.30	1.00
329	Trave f.	9	10	3	5	1	0.30	1.00
330	Trave f.	121	177	3	5	1	0.30	1.00
331	Trave f.	135	136	3	6	1	0.30	1.00
332	Trave f.	400	401	3	5	1	0.30	1.00
333	Trave f.	335	343	3	5	1	0.30	1.00
334	Trave f.	234	235	3	6	1	0.30	1.00

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



335	Trave f.	284	306	3	5	1	0.30	1.00
336	Trave f.	353	360	3	5	1	0.30	1.00
337	Trave f.	333	341	3	5	1	0.30	1.00
338	Trave f.	124	168	3	5	1	0.30	1.00
339	Trave f.	219	221	3	5	1	0.30	1.00
340	Trave f.	354	371	3	5	1	0.30	1.00
341	Trave f.	117	123	3	5	1	0.30	1.00
342	Trave f.	119	138	3	5	1	0.30	1.00
343	Trave f.	342	350	3	5	1	0.30	1.00
344	Trave f.	369	370	3	5	1	0.30	1.00
345	Trave f.	122	131	3	5	1	0.30	1.00
346	Trave f.	340	348	3	5	1	0.30	1.00
347	Trave f.	222	224	3	5	1	0.30	1.00
348	Trave f.	10	11	3	5	1	0.30	1.00
349	Trave f.	136	137	3	6	1	0.30	1.00
350	Trave f.	401	402	3	5	1	0.30	1.00
351	Trave f.	343	351	3	5	1	0.30	1.00
352	Trave f.	235	236	3	6	1	0.30	1.00
353	Trave f.	306	312	3	5	1	0.30	1.00
354	Trave f.	360	379	3	5	1	0.30	1.00
355	Trave f.	341	349	3	5	1	0.30	1.00
356	Trave f.	168	180	3	5	1	0.30	1.00
357	Trave f.	221	223	3	5	1	0.30	1.00
358	Trave f.	371	377	3	5	1	0.30	1.00
359	Trave f.	123	161	3	5	1	0.30	1.00
360	Trave f.	350	367	3	5	1	0.30	1.00
361	Trave f.	370	371	3	5	1	0.30	1.00
362	Trave f.	348	356	3	5	1	0.30	1.00
363	Trave f.	11	12	3	5	1	0.30	1.00
364	Trave f.	137	138	3	6	1	0.30	1.00
365	Trave f.	402	403	3	5	1	0.30	1.00
366	Trave f.	351	375	3	5	1	0.30	1.00
367	Trave f.	236	237	3	6	1	0.30	1.00
368	Trave f.	312	320	3	5	1	0.30	1.00
369	Trave f.	379	389	3	5	1	0.30	1.00
370	Trave f.	349	364	3	5	1	0.30	1.00
371	Trave f.	180	184	3	5	1	0.30	1.00
372	Trave f.	223	281	3	5	1	0.30	1.00
373	Trave f.	377	390	3	5	1	0.30	1.00
374	Trave f.	356	380	3	5	1	0.30	1.00
375	Trave f.	12	13	3	5	1	0.30	1.00
376	Trave f.	138	139	3	6	1	0.30	1.00
377	Trave f.	403	404	3	5	1	0.30	1.00
378	Trave f.	375	381	3	5	1	0.30	1.00
379	Trave f.	237	238	3	6	1	0.30	1.00
380	Trave f.	320	330	3	5	1	0.30	1.00
381	Trave f.	389	402	3	5	1	0.30	1.00
382	Trave f.	184	188	3	5	1	0.30	1.00
383	Trave f.	390	411	3	5	1	0.30	1.00
384	Trave f.	380	382	3	5	1	0.30	1.00
385	Trave f.	13	14	3	5	1	0.30	1.00
386	Trave f.	139	140	3	6	1	0.30	1.00
387	Trave f.	404	405	3	5	1	0.30	1.00
388	Trave f.	381	383	3	5	1	0.30	1.00
389	Trave f.	238	239	3	6	1	0.30	1.00
390	Trave f.	330	336	3	5	1	0.30	1.00
391	Trave f.	188	193	3	5	1	0.30	1.00
392	Trave f.	382	392	3	5	1	0.30	1.00
393	Trave f.	14	15	3	5	1	0.30	1.00
394	Trave f.	140	141	3	6	1	0.30	1.00
395	Trave f.	405	406	3	5	1	0.30	1.00
396	Trave f.	383	421	3	5	1	0.30	1.00
397	Trave f.	239	240	3	6	1	0.30	1.00
398	Trave f.	336	344	3	5	1	0.30	1.00
399	Trave f.	193	196	3	5	1	0.30	1.00
400	Trave f.	15	16	3	5	1	0.30	1.00
401	Trave f.	141	142	3	6	1	0.30	1.00
402	Trave f.	406	407	3	5	1	0.30	1.00
403	Trave f.	240	241	3	6	1	0.30	1.00
404	Trave f.	344	352	3	5	1	0.30	1.00
405	Trave f.	196	200	3	5	1	0.30	1.00
406	Trave f.	16	17	3	5	1	0.30	1.00
407	Trave f.	142	143	3	6	1	0.30	1.00
408	Trave f.	407	408	3	5	1	0.30	1.00
409	Trave f.	241	242	3	6	1	0.30	1.00
410	Trave f.	352	359	3	5	1	0.30	1.00

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



411	Trave f.	200	212	3	5	1	0.30	1.00
412	Trave f.	17	18	3	5	1	0.30	1.00
413	Trave f.	143	144	3	6	1	0.30	1.00
414	Trave f.	408	409	3	5	1	0.30	1.00
415	Trave f.	242	243	3	6	1	0.30	1.00
416	Trave f.	359	376	3	5	1	0.30	1.00
417	Trave f.	212	275	3	5	1	0.30	1.00
418	Trave f.	18	19	3	5	1	0.30	1.00
419	Trave f.	144	145	3	6	1	0.30	1.00
420	Trave f.	409	410	3	5	1	0.30	1.00
421	Trave f.	243	244	3	6	1	0.30	1.00
422	Trave f.	376	388	3	5	1	0.30	1.00
423	Trave f.	275	286	3	5	1	0.30	1.00
424	Trave f.	19	20	3	5	1	0.30	1.00
425	Trave f.	145	146	3	6	1	0.30	1.00
426	Trave f.	410	411	3	5	1	0.30	1.00
427	Trave f.	244	245	3	6	1	0.30	1.00
428	Trave f.	388	394	3	5	1	0.30	1.00
429	Trave f.	286	307	3	5	1	0.30	1.00
430	Trave f.	20	21	3	5	1	0.30	1.00
431	Trave f.	146	147	3	6	1	0.30	1.00
432	Trave f.	411	412	3	5	1	0.30	1.00
433	Trave f.	245	246	3	6	1	0.30	1.00
434	Trave f.	307	315	3	5	1	0.30	1.00
435	Trave f.	21	22	3	5	1	0.30	1.00
436	Trave f.	147	148	3	6	1	0.30	1.00
437	Trave f.	412	413	3	5	1	0.30	1.00
438	Trave f.	246	247	3	6	1	0.30	1.00
439	Trave f.	315	323	3	5	1	0.30	1.00
440	Trave f.	22	23	3	5	1	0.30	1.00
441	Trave f.	148	149	3	6	1	0.30	1.00
442	Trave f.	413	414	3	5	1	0.30	1.00
443	Trave f.	247	248	3	6	1	0.30	1.00
444	Trave f.	323	329	3	5	1	0.30	1.00
445	Trave f.	23	24	3	5	1	0.30	1.00
446	Trave f.	149	150	3	6	1	0.30	1.00
447	Trave f.	414	415	3	5	1	0.30	1.00
448	Trave f.	248	249	3	6	1	0.30	1.00
449	Trave f.	329	339	3	5	1	0.30	1.00
450	Trave f.	24	25	3	5	1	0.30	1.00
451	Trave f.	150	151	3	6	1	0.30	1.00
452	Trave f.	415	416	3	5	1	0.30	1.00
453	Trave f.	249	250	3	6	1	0.30	1.00
454	Trave f.	339	347	3	5	1	0.30	1.00
455	Trave f.	25	26	3	5	1	0.30	1.00
456	Trave f.	151	152	3	6	1	0.30	1.00
457	Trave f.	416	417	3	5	1	0.30	1.00
458	Trave f.	250	251	3	6	1	0.30	1.00
459	Trave f.	347	355	3	5	1	0.30	1.00
460	Trave f.	26	27	3	5	1	0.30	1.00
461	Trave f.	152	153	3	6	1	0.30	1.00
462	Trave f.	417	418	3	5	1	0.30	1.00
463	Trave f.	251	252	3	6	1	0.30	1.00
464	Trave f.	355	372	3	5	1	0.30	1.00
465	Trave f.	27	28	3	5	1	0.30	1.00
466	Trave f.	153	154	3	6	1	0.30	1.00
467	Trave f.	418	419	3	5	1	0.30	1.00
468	Trave f.	252	253	3	6	1	0.30	1.00
469	Trave f.	372	378	3	5	1	0.30	1.00
470	Trave f.	28	29	3	5	1	0.30	1.00
471	Trave f.	154	155	3	6	1	0.30	1.00
472	Trave f.	419	420	3	5	1	0.30	1.00
473	Trave f.	253	254	3	6	1	0.30	1.00
474	Trave f.	378	391	3	5	1	0.30	1.00
475	Trave f.	29	30	3	5	1	0.30	1.00
476	Trave f.	155	156	3	6	1	0.30	1.00
477	Trave f.	420	421	3	5	1	0.30	1.00
478	Trave f.	254	255	3	6	1	0.30	1.00
479	Trave f.	391	419	3	5	1	0.30	1.00
480	Trave f.	30	31	3	5	1	0.30	1.00
481	Trave f.	156	157	3	6	1	0.30	1.00
482	Trave f.	255	256	3	6	1	0.30	1.00
483	Trave f.	31	32	3	5	1	0.30	1.00
484	Trave f.	157	158	3	6	1	0.30	1.00
485	Trave f.	256	257	3	6	1	0.30	1.00
486	Trave f.	32	33	3	5	1	0.30	1.00

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



487	Trave f.	158	159	3	6	1	0.30	1.00
488	Trave f.	257	258	3	6	1	0.30	1.00
489	Trave f.	33	34	3	5	1	0.30	1.00
490	Trave f.	159	160	3	6	1	0.30	1.00
491	Trave f.	258	259	3	6	1	0.30	1.00
492	Trave f.	34	35	3	5	1	0.30	1.00
493	Trave f.	160	161	3	6	1	0.30	1.00
494	Trave f.	259	260	3	6	1	0.30	1.00
495	Trave f.	35	36	3	5	1	0.30	1.00
496	Trave f.	161	162	3	6	1	0.30	1.00
497	Trave f.	260	261	3	6	1	0.30	1.00
498	Trave f.	36	37	3	5	1	0.30	1.00
499	Trave f.	162	163	3	6	1	0.30	1.00
500	Trave f.	261	262	3	6	1	0.30	1.00
501	Trave f.	37	38	3	5	1	0.30	1.00
502	Trave f.	163	164	3	6	1	0.30	1.00
503	Trave f.	262	263	3	6	1	0.30	1.00
504	Trave f.	38	39	3	5	1	0.30	1.00
505	Trave f.	164	165	3	6	1	0.30	1.00
506	Trave f.	263	264	3	6	1	0.30	1.00
507	Trave f.	39	40	3	5	1	0.30	1.00
508	Trave f.	165	166	3	6	1	0.30	1.00
509	Trave f.	264	265	3	6	1	0.30	1.00
510	Trave f.	40	41	3	5	1	0.30	1.00
511	Trave f.	166	167	3	6	1	0.30	1.00
512	Trave f.	265	266	3	6	1	0.30	1.00
513	Trave f.	41	42	3	5	1	0.30	1.00
514	Trave f.	167	168	3	6	1	0.30	1.00
515	Trave f.	266	267	3	6	1	0.30	1.00
516	Trave f.	42	43	3	5	1	0.30	1.00
517	Trave f.	168	169	3	5	1	0.30	1.00
518	Trave f.	267	268	3	6	1	0.30	1.00
519	Trave f.	43	44	3	5	1	0.30	1.00
520	Trave f.	169	170	3	5	1	0.30	1.00
521	Trave f.	268	269	3	6	1	0.30	1.00
522	Trave f.	44	45	3	5	1	0.30	1.00
523	Trave f.	170	171	3	5	1	0.30	1.00
524	Trave f.	269	270	3	6	1	0.30	1.00
525	Trave f.	45	46	3	5	1	0.30	1.00
526	Trave f.	171	172	3	5	1	0.30	1.00
527	Trave f.	270	271	3	6	1	0.30	1.00
528	Trave f.	46	47	3	5	1	0.30	1.00
529	Trave f.	172	173	3	5	1	0.30	1.00
530	Trave f.	271	272	3	6	1	0.30	1.00
531	Trave f.	47	48	3	5	1	0.30	1.00
532	Trave f.	173	174	3	5	1	0.30	1.00
533	Trave f.	272	273	3	6	1	0.30	1.00
534	Trave f.	48	49	3	5	1	0.30	1.00
535	Trave f.	174	175	3	5	1	0.30	1.00
536	Trave f.	273	274	3	6	1	0.30	1.00
537	Trave f.	49	50	3	5	1	0.30	1.00
538	Trave f.	175	176	3	5	1	0.30	1.00
539	Trave f.	274	275	3	6	1	0.30	1.00
540	Trave f.	50	51	3	5	1	0.30	1.00
541	Trave f.	176	177	3	5	1	0.30	1.00
542	Trave f.	275	276	3	6	1	0.30	1.00
543	Trave f.	51	52	3	5	1	0.30	1.00
544	Trave f.	276	277	3	5	1	0.30	1.00
545	Trave f.	52	53	3	5	1	0.30	1.00
546	Trave f.	277	278	3	5	1	0.30	1.00
547	Trave f.	53	54	3	5	1	0.30	1.00
548	Trave f.	278	279	3	5	1	0.30	1.00
549	Trave f.	54	55	3	5	1	0.30	1.00
550	Trave f.	279	280	3	5	1	0.30	1.00
551	Trave f.	280	281	3	5	1	0.30	1.00
552	Trave f.	281	282	3	5	1	0.30	1.00
553	Trave f.	282	283	3	5	1	0.30	1.00
554	Trave f.	364	3229	3	5	1	0.30	1.00
555	Trave f.	409	3230	3	5	1	0.30	1.00
561	Trave f.	3229	404	3	5	1	0.30	1.00
562	Trave f.	3230	367	3	5	1	0.30	1.00
565	Trave f.	320	321	3	5	1	0.30	1.00
566	Trave f.	322	323	3	5	1	0.30	1.00

6. MODELLAZIONE DELLE AZIONI

LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza F_x , F_y , F_z , momento M_x , M_y , M_z)
2	spostamento nodale impresso 6 dati (spostamento T_x , T_y , T_z , rotazione R_x , R_y , R_z)
3	carico distribuito globale su elemento tipo trave 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di inizio carico) 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di inizio carico) 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (F_x , F_y , F_z , M_x , M_y , M_z , ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F_1 , F_2 , F_3 , M_1 , M_2 , M_3 , ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell'impronta, interasse tra i carichi)

	Carico concentrato nodale		Spostamento impresso
	Carico distribuito globale		Carico distribuito locale
	Carico concentrato globale		Carico concentrato locale
	Carico termico 2D		Carico termico 3D
	Carico pressione uniforme		Carico pressione variabile

Tipo carico distribuito globale su trave

Id	Tipo	Pos.	fx	fy	fz	mx	my	mz
		m	daN/ m	daN/ m	daN/ m	daN	daN	daN
18	marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15	0.0	0.0	0.0	-715.00	0.0	0.0	0.0
		0.0	0.0	0.0	-715.00	0.0	0.0	0.0
19	marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50	0.0	0.0	0.0	-1250.00	0.0	0.0	0.0
		0.0	0.0	0.0	-1250.00	0.0	0.0	0.0
20	marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73	0.0	0.0	0.0	-1573.00	0.0	0.0	0.0
		0.0	0.0	0.0	-1573.00	0.0	0.0	0.0
21	marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00	0.0	0.0	0.0	-400.00	0.0	0.0	0.0
		0.0	0.0	0.0	-400.00	0.0	0.0	0.0
22	marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00	0.0	0.0	0.0	-700.00	0.0	0.0	0.0
		0.0	0.0	0.0	-700.00	0.0	0.0	0.0
23	marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80	0.0	0.0	0.0	-880.00	0.0	0.0	0.0
		0.0	0.0	0.0	-880.00	0.0	0.0	0.0

Tipo carico di pressione uniforme su piastra

Id	Tipo	pressione
		daN/ m2
4	Vy+ copertura-P3:p= 3.000e-03	30.00
7	Vy- copertura-P3:p= 3.000e-03	30.00
10	Vx+ copertura-P3:p= 3.000e-03	30.00
13	Vx- copertura-P3:p= 3.000e-03	30.00

Tipo carico di pressione variabile su piastra

Id	Tipo	pressione	quota	pressione	quota
		daN/ m2	m	daN/ m2	m
2	Vy+ PARETE SOPRAVENTO-PL3:pi= 6.000e-03 qi=600.00 pf= 6.000e-03 qf=0.0	60.00	6.00	60.00	0.0
3	Vy+ PARETE SOTTOVENTO-PL3:pi= 3.000e-03 qi=600.00 pf= 3.000e-03 qf=0.0	30.00	6.00	30.00	0.0
5	Vy- PARETE SOPRAVENTO-PL3:pi=-6.000e-03 qi=600.00 pf=-6.000e-03 qf=0.0	-60.00	6.00	-60.00	0.0
6	Vy- PARETE SOTTOVENTO-PL3:pi=-3.000e-03 qi=600.00 pf=-3.000e-03 qf=0.0	-30.00	6.00	-30.00	0.0
8	Vx+ PARETE SOPRAVENTO-PL3:pi=-6.000e-03 qi=600.00 pf=-6.000e-03 qf=0.0	-60.00	6.00	-60.00	0.0
9	Vx+ PARETE SOTTOVENTO-PL3:pi= 3.000e-03 qi=600.00 pf= 3.000e-03 qf=0.0	30.00	6.00	30.00	0.0
11	Vx- PARETE SOPRAVENTO-PL3:pi=-6.000e-03 qi=600.00 pf=-6.000e-03 qf=0.0	-60.00	6.00	-60.00	0.0
12	Vx- PARETE SOTTOVENTO-PL3:pi= 3.000e-03 qi=600.00 pf= 3.000e-03 qf=0.0	30.00	6.00	30.00	0.0

Tipo carico variabile generale

Id	Tipo	ascissa	valore	ascissa	valore
		m	daN/ m2	m	daN/ m2
1	neve pensilina ingresso-QV:var y - Qz - Pres.				
	Y - Y Qz Pres. L2=0.0	4.00	-80.00	4.50	-80.00
		4.50	-80.00	4.50	-80.00
		4.50	-80.00	9.51	-200.00
14	acc neve h150-QV:var y - Qz - Pres.				
	Y - Y Qz Pres. L2=0.0	19.98	-120.00	24.98	0.0
15	acc neve h70-QV:var y - Qz - Pres.				
	Y - Y Qz Pres. L2=0.0	25.63	0.0	30.70	-60.00
16	acc neve h50-QV:var y - Qz - Pres.				
	Y - Y Qz Pres. L2=0.0	5.88	-20.00	10.88	0.0
17	neve pensilina lato-QV:var x - Qz - Pres.				
	X - X Qz Pres. L2=0.0	40.57	-200.00	45.57	-80.00

7. SCHEMATIZZAZIONE DEI CASI DI CARICO

LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Etk	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso:

Numero Tipo e Sigla identificativa, Valore di riferimento del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gsk	CDC=G1sk (permanente solai-coperture)	
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)	
4	Qnk	CDC=Qnk (carico da neve)	
5	Qvk	CDC=Qvk (carico da vento) dir X +	Azioni applicate:
6	Qvk	CDC=Qvk (carico da vento) dir X -	Azioni applicate:

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CDC	Tipo	Sigla Id	Note
7	Qvk	CDC=Qvk (carico da vento) dir Y +	Azioni applicate:
8	Qvk	CDC=Qvk (carico da vento) dir Y -	Azioni applicate:
9	Qk	CDC=Qk (variabile generico) accumulo neve	Azioni applicate:
10	Esk	CDC=Es (statico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura) partecipazione:1.00 per 2 CDC=G1sk (permanente solai-coperture) partecipazione:1.00 per 3 CDC=G2sk (permanente solai-coperture n.c.d.) partecipazione:1.00 per 4 CDC=Qnk (carico da neve)
11	Esk	CDC=Es (statico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
12	Esk	CDC=Es (statico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
13	Esk	CDC=Es (statico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
14	Esk	CDC=Es (statico SLD) alfa=0.0 (ecc. +)	come precedente CDC sismico
15	Esk	CDC=Es (statico SLD) alfa=0.0 (ecc. -)	come precedente CDC sismico
16	Esk	CDC=Es (statico SLD) alfa=90.00 (ecc. +)	come precedente CDC sismico
17	Esk	CDC=Es (statico SLD) alfa=90.00 (ecc. -)	come precedente CDC sismico
18	Gk	CDC=G1k (permanente generico) MARCIAPIEDE	Azioni applicate: D2 : 124 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 126 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15 D2 : 128 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 :da 129 a 130 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 :da 132 a 133 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 : 139 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 156 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 158 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15 D2 : 160 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 :da 161 a 162 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 :da 164 a 165 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 : 171 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 185 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 186 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15 D2 : 187 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 :da 188 a 189 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 :da 191 a 192 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 : 198 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 210 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 211 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15 D2 : 212 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 :da 213 a 214 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 :da 216 a 217 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 : 223 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 235 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 236 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15 D2 : 237 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 :da 238 a 239 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 :da 241 a 242 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 : 248 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 259 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 260 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15 D2 : 261 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 :da 262 a 263 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 :da 265 a 266 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 : 272 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 282 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 283 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15 D2 : 284 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 :da 285 a 286 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 :da 288 a 289 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50 D2 : 295 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 304 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73 D2 : 305 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15 D2 : 306 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73

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CDC	Tipo	Sigla Id	Note
			D2 :da 307 a 308 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 :da 310 a 311 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 317 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 326 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 327 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15
			D2 : 328 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 :da 329 a 330 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 :da 332 a 333 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 339 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 346 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 347 Azione : marciapiede L100 PERM-DG:Fzi=-7.15 Fzf=-7.15
			D2 : 348 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 :da 350 a 351 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 357 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 362 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 363 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 :da 365 a 366 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 372 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 374 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 375 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 :da 377 a 378 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 384 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 385 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 :da 387 a 388 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 392 Azione : marciapiede L220 PERM-DG:Fzi=-15.73 Fzf=-15.73
			D2 : 393 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 :da 395 a 396 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 400 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 402 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 406 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 408 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 412 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 414 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 418 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 420 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 424 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 426 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 430 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 432 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 435 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 437 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 440 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 442 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 445 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 447 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 450 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 452 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 455 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 457 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 460 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 462 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 465 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 467 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 470 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 472 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 475 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 477 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 480 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 483 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 486 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 489 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 492 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 495 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 498 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50

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CDC	Tipo	Sigla Id	Note
			D2 : 501 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 504 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 507 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 510 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 513 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 516 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 519 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 522 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 525 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 528 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 531 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 534 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 537 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 540 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 543 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 545 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 547 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
			D2 : 549 Azione : marciapiede L175 PERM-DG:Fzi=-12.50 Fzf=-12.50
19	Qk	CDC=Qk (variabile generico) MARCIAPIEDE	Azioni applicate:
			D2 : 124 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 126 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 128 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 129 a 130 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 132 a 133 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 139 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 156 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 158 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 160 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 161 a 162 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 164 a 165 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 171 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 185 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 186 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 187 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 188 a 189 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 191 a 192 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 198 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 210 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 211 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 212 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 213 a 214 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 216 a 217 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 223 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 235 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 236 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 237 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 238 a 239 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 241 a 242 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 248 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 259 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 260 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 261 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 262 a 263 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 265 a 266 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 272 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 282 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 283 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 284 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 285 a 286 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 288 a 289 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 295 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 304 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 305 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 306 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 307 a 308 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 310 a 311 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 317 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 326 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 : 327 Azione : marciapiede L100 ACC-DG:Fzi=-4.00 Fzf=-4.00
			D2 : 328 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80
			D2 :da 329 a 330 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 :da 332 a 333 Azione : marciapiede L175 ACC-DG:Fzi=-7.00 Fzf=-7.00
			D2 : 339 Azione : marciapiede L220 ACC-DG:Fzi=-8.80 Fzf=-8.80

8. DEFINIZIONE DELLE COMBINAZIONI

LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente. Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$$\gamma G_1 \cdot G_1 + \gamma G_2 \cdot G_2 + \gamma P \cdot P + \gamma Q_1 \cdot Q_{k1} + \gamma Q_2 \cdot \psi_{02} \cdot Q_{k2} + \gamma Q_3 \cdot \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione caratteristica (rara) SLE

$$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$$

Combinazione frequente SLE

$$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione quasi permanente SLE

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G_1 + G_2 + A_d + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Dove:

NTC 2018 Tabella 2.5.1

Destinazione d'uso/azione	ψ_0	ψ_1	ψ_2
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli $\leq 30kN$)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli $> 30kN$)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota $\leq 1000 m$	0,50	0,20	0,00
Neve a quota $> 1000 m$	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2018 Tabella 2.6.1

Coefficiente	EQU	A1	A2
γ_f			

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



<i>Carichi permanenti</i>	<i>Favorevoli</i>	$\gamma G1$	0,9	1,0	1,0
	<i>Sfavorevoli</i>		1,1	1,3	1,0
<i>Carichi permanenti non strutturali</i>	<i>Favorevoli</i>	$\gamma G2$	0,8	0,8	0,8
<i>(Non compiutamente definiti)</i>	<i>Sfavorevoli</i>		1,5	1,5	1,3
<i>Carichi variabili</i>	<i>Favorevoli</i>	γQi	0,0	0,0	0,0
	<i>Sfavorevoli</i>		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	
9	SLU	Comb. SLU A1 9	
10	SLU	Comb. SLU A1 10	
11	SLU	Comb. SLU A1 11	
12	SLU	Comb. SLU A1 12	
13	SLU	Comb. SLU A1 13	
14	SLU	Comb. SLU A1 14	
15	SLU	Comb. SLU A1 15	
16	SLU	Comb. SLU A1 16	
17	SLU	Comb. SLU A1 17	
18	SLU	Comb. SLU A1 18	
19	SLU	Comb. SLU A1 19	
20	SLU	Comb. SLU A1 20	
21	SLU	Comb. SLU A1 21	
22	SLU	Comb. SLU A1 22	
23	SLU	Comb. SLU A1 23	
24	SLU	Comb. SLU A1 24	
25	SLU	Comb. SLU A1 25	
26	SLU	Comb. SLU A1 26	
27	SLU	Comb. SLU A1 27	
28	SLU	Comb. SLU A1 28	
29	SLU	Comb. SLU A1 29	
30	SLU	Comb. SLU A1 30	
31	SLU	Comb. SLU A1 31	
32	SLU	Comb. SLU A1 32	
33	SLU	Comb. SLU A1 33	
34	SLU	Comb. SLU A1 34	
35	SLU	Comb. SLU A1 35	
36	SLU	Comb. SLU A1 36	
37	SLU	Comb. SLU A1 37	
38	SLU	Comb. SLU A1 38	
39	SLU	Comb. SLU A1 39	
40	SLU	Comb. SLU A1 40	
41	SLU	Comb. SLU A1 41	
42	SLU	Comb. SLU A1 42	
43	SLU	Comb. SLU A1 43	
44	SLU	Comb. SLU A1 44	
45	SLU	Comb. SLU A1 45	
46	SLU	Comb. SLU A1 46	
47	SLU	Comb. SLU A1 47	
48	SLU	Comb. SLU A1 48	
49	SLU	Comb. SLU A1 49	
50	SLU	Comb. SLU A1 50	
51	SLU	Comb. SLU A1 51	
52	SLU	Comb. SLU A1 52	
53	SLU	Comb. SLU A1 53	
54	SLU	Comb. SLU A1 54	
55	SLU	Comb. SLU A1 55	
56	SLU	Comb. SLU A1 56	
57	SLU	Comb. SLU A1 57	

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Cmb	Tipo	Sigla Id	effetto P-delta
58	SLU	Comb. SLU A1 58	
59	SLU	Comb. SLU A1 59	
60	SLU	Comb. SLU A1 60	
61	SLU	Comb. SLU A1 61	
62	SLU	Comb. SLU A1 62	
63	SLU	Comb. SLU A1 63	
64	SLU	Comb. SLU A1 64	
65	SLU	Comb. SLU A1 65	
66	SLU	Comb. SLU A1 66	
67	SLU	Comb. SLU A1 (SLV sism.) 67	
68	SLU	Comb. SLU A1 (SLV sism.) 68	
69	SLU	Comb. SLU A1 (SLV sism.) 69	
70	SLU	Comb. SLU A1 (SLV sism.) 70	
71	SLU	Comb. SLU A1 (SLV sism.) 71	
72	SLU	Comb. SLU A1 (SLV sism.) 72	
73	SLU	Comb. SLU A1 (SLV sism.) 73	
74	SLU	Comb. SLU A1 (SLV sism.) 74	
75	SLU	Comb. SLU A1 (SLV sism.) 75	
76	SLU	Comb. SLU A1 (SLV sism.) 76	
77	SLU	Comb. SLU A1 (SLV sism.) 77	
78	SLU	Comb. SLU A1 (SLV sism.) 78	
79	SLU	Comb. SLU A1 (SLV sism.) 79	
80	SLU	Comb. SLU A1 (SLV sism.) 80	
81	SLU	Comb. SLU A1 (SLV sism.) 81	
82	SLU	Comb. SLU A1 (SLV sism.) 82	
83	SLU	Comb. SLU A1 (SLV sism.) 83	
84	SLU	Comb. SLU A1 (SLV sism.) 84	
85	SLU	Comb. SLU A1 (SLV sism.) 85	
86	SLU	Comb. SLU A1 (SLV sism.) 86	
87	SLU	Comb. SLU A1 (SLV sism.) 87	
88	SLU	Comb. SLU A1 (SLV sism.) 88	
89	SLU	Comb. SLU A1 (SLV sism.) 89	
90	SLU	Comb. SLU A1 (SLV sism.) 90	
91	SLU	Comb. SLU A1 (SLV sism.) 91	
92	SLU	Comb. SLU A1 (SLV sism.) 92	
93	SLU	Comb. SLU A1 (SLV sism.) 93	
94	SLU	Comb. SLU A1 (SLV sism.) 94	
95	SLU	Comb. SLU A1 (SLV sism.) 95	
96	SLU	Comb. SLU A1 (SLV sism.) 96	
97	SLU	Comb. SLU A1 (SLV sism.) 97	
98	SLU	Comb. SLU A1 (SLV sism.) 98	
99	SLD(sis)	Comb. SLE (SLD Danno sism.) 99	
100	SLD(sis)	Comb. SLE (SLD Danno sism.) 100	
101	SLD(sis)	Comb. SLE (SLD Danno sism.) 101	
102	SLD(sis)	Comb. SLE (SLD Danno sism.) 102	
103	SLD(sis)	Comb. SLE (SLD Danno sism.) 103	
104	SLD(sis)	Comb. SLE (SLD Danno sism.) 104	
105	SLD(sis)	Comb. SLE (SLD Danno sism.) 105	
106	SLD(sis)	Comb. SLE (SLD Danno sism.) 106	
107	SLD(sis)	Comb. SLE (SLD Danno sism.) 107	
108	SLD(sis)	Comb. SLE (SLD Danno sism.) 108	
109	SLD(sis)	Comb. SLE (SLD Danno sism.) 109	
110	SLD(sis)	Comb. SLE (SLD Danno sism.) 110	
111	SLD(sis)	Comb. SLE (SLD Danno sism.) 111	
112	SLD(sis)	Comb. SLE (SLD Danno sism.) 112	
113	SLD(sis)	Comb. SLE (SLD Danno sism.) 113	
114	SLD(sis)	Comb. SLE (SLD Danno sism.) 114	
115	SLD(sis)	Comb. SLE (SLD Danno sism.) 115	
116	SLD(sis)	Comb. SLE (SLD Danno sism.) 116	
117	SLD(sis)	Comb. SLE (SLD Danno sism.) 117	
118	SLD(sis)	Comb. SLE (SLD Danno sism.) 118	
119	SLD(sis)	Comb. SLE (SLD Danno sism.) 119	
120	SLD(sis)	Comb. SLE (SLD Danno sism.) 120	
121	SLD(sis)	Comb. SLE (SLD Danno sism.) 121	
122	SLD(sis)	Comb. SLE (SLD Danno sism.) 122	
123	SLD(sis)	Comb. SLE (SLD Danno sism.) 123	
124	SLD(sis)	Comb. SLE (SLD Danno sism.) 124	
125	SLD(sis)	Comb. SLE (SLD Danno sism.) 125	
126	SLD(sis)	Comb. SLE (SLD Danno sism.) 126	
127	SLD(sis)	Comb. SLE (SLD Danno sism.) 127	
128	SLD(sis)	Comb. SLE (SLD Danno sism.) 128	
129	SLD(sis)	Comb. SLE (SLD Danno sism.) 129	
130	SLD(sis)	Comb. SLE (SLD Danno sism.) 130	

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Cmb	Tipo	Sigla Id	effetto P-delta
131	SLE(r)	Comb. SLE(rara) 131	
132	SLE(r)	Comb. SLE(rara) 132	
133	SLE(r)	Comb. SLE(rara) 133	
134	SLE(r)	Comb. SLE(rara) 134	
135	SLE(r)	Comb. SLE(rara) 135	
136	SLE(r)	Comb. SLE(rara) 136	
137	SLE(r)	Comb. SLE(rara) 137	
138	SLE(r)	Comb. SLE(rara) 138	
139	SLE(r)	Comb. SLE(rara) 139	
140	SLE(r)	Comb. SLE(rara) 140	
141	SLE(r)	Comb. SLE(rara) 141	
142	SLE(r)	Comb. SLE(rara) 142	
143	SLE(r)	Comb. SLE(rara) 143	
144	SLE(r)	Comb. SLE(rara) 144	
145	SLE(r)	Comb. SLE(rara) 145	
146	SLE(r)	Comb. SLE(rara) 146	
147	SLE(r)	Comb. SLE(rara) 147	
148	SLE(r)	Comb. SLE(rara) 148	
149	SLE(r)	Comb. SLE(rara) 149	
150	SLE(r)	Comb. SLE(rara) 150	
151	SLE(r)	Comb. SLE(rara) 151	
152	SLE(r)	Comb. SLE(rara) 152	
153	SLE(r)	Comb. SLE(rara) 153	
154	SLE(r)	Comb. SLE(rara) 154	
155	SLE(r)	Comb. SLE(rara) 155	
156	SLE(r)	Comb. SLE(rara) 156	
157	SLE(r)	Comb. SLE(rara) 157	
158	SLE(r)	Comb. SLE(rara) 158	
159	SLE(r)	Comb. SLE(rara) 159	
160	SLE(r)	Comb. SLE(rara) 160	
161	SLE(r)	Comb. SLE(rara) 161	
162	SLE(r)	Comb. SLE(rara) 162	
163	SLE(r)	Comb. SLE(rara) 163	
164	SLE(f)	Comb. SLE(freq.) 164	
165	SLE(f)	Comb. SLE(freq.) 165	
166	SLE(f)	Comb. SLE(freq.) 166	
167	SLE(f)	Comb. SLE(freq.) 167	
168	SLE(f)	Comb. SLE(freq.) 168	
169	SLE(f)	Comb. SLE(freq.) 169	
170	SLE(f)	Comb. SLE(freq.) 170	
171	SLE(p)	Comb. SLE(perm.) 171	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	1.30	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
2	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
3	1.00	1.00	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
4	1.00	1.00	0.80	1.50	0.0	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
5	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
6	1.00	1.00	0.80	0.75	0.0	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
7	1.30	1.30	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
8	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
9	1.00	1.00	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
10	1.00	1.00	0.80	0.75	0.0	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
11	1.30	1.30	1.50	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
12	1.30	1.30	1.50	1.50	0.90	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
13	1.00	1.00	0.80	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	1.00	1.05									
14	1.00	1.00	0.80	1.50	0.90	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
15	1.30	1.30	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
16	1.30	1.30	1.50	0.75	1.50	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
17	1.00	1.00	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
18	1.00	1.00	0.80	0.75	1.50	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
19	1.30	1.30	1.50	0.75	0.90	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
20	1.00	1.00	0.80	0.75	0.90	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
21	1.30	1.30	1.50	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
22	1.30	1.30	1.50	0.75	0.90	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
23	1.00	1.00	0.80	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
24	1.00	1.00	0.80	0.75	0.90	0.0	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
25	1.30	1.30	1.50	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
26	1.30	1.30	1.50	1.50	0.0	0.90	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
27	1.00	1.00	0.80	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
28	1.00	1.00	0.80	1.50	0.0	0.90	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
29	1.30	1.30	1.50	0.75	0.0	0.90	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
30	1.00	1.00	0.80	0.75	0.0	0.90	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
31	1.30	1.30	1.50	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
32	1.30	1.30	1.50	0.75	0.0	1.50	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
33	1.00	1.00	0.80	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
34	1.00	1.00	0.80	0.75	0.0	1.50	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
35	1.30	1.30	1.50	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
36	1.30	1.30	1.50	0.75	0.0	0.90	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
37	1.00	1.00	0.80	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
38	1.00	1.00	0.80	0.75	0.0	0.90	0.0	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
39	1.30	1.30	1.50	0.0	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
40	1.30	1.30	1.50	1.50	0.0	0.0	0.90	0.0	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
41	1.00	1.00	0.80	0.0	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
42	1.00	1.00	0.80	1.50	0.0	0.0	0.90	0.0	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
43	1.30	1.30	1.50	0.75	0.0	0.0	0.90	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
44	1.00	1.00	0.80	0.75	0.0	0.0	0.90	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
45	1.30	1.30	1.50	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
46	1.30	1.30	1.50	0.75	0.0	0.0	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
47	1.00	1.00	0.80	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
48	1.00	1.00	0.80	0.75	0.0	0.0	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
49	1.30	1.30	1.50	0.0	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	1.30	1.50									
50	1.30	1.30	1.50	0.75	0.0	0.0	0.90	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
51	1.00	1.00	0.80	0.0	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
52	1.00	1.00	0.80	0.75	0.0	0.0	0.90	0.0	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
53	1.30	1.30	1.50	0.0	0.0	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
54	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.90	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
55	1.00	1.00	0.80	0.0	0.0	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
56	1.00	1.00	0.80	1.50	0.0	0.0	0.0	0.90	1.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
57	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.90	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
58	1.00	1.00	0.80	0.75	0.0	0.0	0.0	0.90	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
59	1.30	1.30	1.50	0.0	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
60	1.30	1.30	1.50	0.75	0.0	0.0	0.0	1.50	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.05									
61	1.00	1.00	0.80	0.0	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
62	1.00	1.00	0.80	0.75	0.0	0.0	0.0	1.50	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.05									
63	1.30	1.30	1.50	0.0	0.0	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
64	1.30	1.30	1.50	0.75	0.0	0.0	0.0	0.90	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.30	1.50									
65	1.00	1.00	0.80	0.0	0.0	0.0	0.0	0.90	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
66	1.00	1.00	0.80	0.75	0.0	0.0	0.0	0.90	0.75	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.50									
67	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
68	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
69	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
70	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
71	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30	0.0
	0.0	0.0	0.0	1.00	0.60									
72	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30	0.0
	0.0	0.0	0.0	1.00	0.60									
73	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30	0.0
	0.0	0.0	0.0	1.00	0.60									
74	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30	0.0
	0.0	0.0	0.0	1.00	0.60									
75	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
76	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
77	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
78	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
79	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0
	0.0	0.0	0.0	1.00	0.60									
80	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0
	0.0	0.0	0.0	1.00	0.60									
81	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0
	0.0	0.0	0.0	1.00	0.60									
82	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0
	0.0	0.0	0.0	1.00	0.60									
83	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
84	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
85	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	1.00	0.60									
86	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
87	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	-1.00	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
88	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	1.00	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
89	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	-1.00	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
90	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	1.00	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
91	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	-1.00	0.0
	0.0	0.0	0.0	1.00	0.60									
92	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00	0.0
	0.0	0.0	0.0	1.00	0.60									
93	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00	0.0
	0.0	0.0	0.0	1.00	0.60									
94	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00	0.0
	0.0	0.0	0.0	1.00	0.60									
95	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0
	0.0	0.0	0.0	1.00	0.60									
96	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0
	0.0	0.0	0.0	1.00	0.60									
97	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0
	0.0	0.0	0.0	1.00	0.60									
98	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0
	0.0	0.0	0.0	1.00	0.60									
99	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00
	0.0	-0.30	0.0	1.00	0.60									
100	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00
	0.0	0.30	0.0	1.00	0.60									
101	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00
	0.0	-0.30	0.0	1.00	0.60									
102	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00
	0.0	0.30	0.0	1.00	0.60									
103	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00
	0.0	0.0	-0.30	1.00	0.60									
104	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.00
	0.0	0.0	0.30	1.00	0.60									
105	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00
	0.0	0.0	-0.30	1.00	0.60									
106	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00
	0.0	0.0	0.30	1.00	0.60									
107	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-1.00	-0.30	0.0	1.00	0.60									
108	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-1.00	0.30	0.0	1.00	0.60									
109	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	-0.30	0.0	1.00	0.60									
110	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.30	0.0	1.00	0.60									
111	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-1.00	0.0	-0.30	1.00	0.60									
112	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-1.00	0.0	0.30	1.00	0.60									
113	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	-0.30	1.00	0.60									
114	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1.00	0.0	0.30	1.00	0.60									
115	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30
	0.0	-1.00	0.0	1.00	0.60									
116	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30
	0.0	1.00	0.0	1.00	0.60									
117	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30
	0.0	-1.00	0.0	1.00	0.60									
118	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30
	0.0	1.00	0.0	1.00	0.60									
119	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-0.30	-1.00	0.0	1.00	0.60									
120	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-0.30	1.00	0.0	1.00	0.60									
121	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.30	-1.00	0.0	1.00	0.60									
122	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.30	1.00	0.0	1.00	0.60									
123	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30
	0.0	0.0	-1.00	1.00	0.60									
124	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.30
	0.0	0.0	1.00	1.00	0.60									
125	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30
	0.0	0.0	-1.00	1.00	0.60									
126	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30
	0.0	0.0	1.00	1.00	0.60									
127	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-0.30	0.0	-1.00	1.00	0.60									
128	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-0.30	0.0	1.00	1.00	0.60									
129	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.30	0.0	-1.00	1.00	0.60									
130	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.30	0.0	1.00	1.00	0.60									
131	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
132	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
133	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
134	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
135	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
136	1.00	1.00	1.00	0.0	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
137	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
138	1.00	1.00	1.00	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
139	1.00	1.00	1.00	0.50	1.00	0.0	0.0	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
140	1.00	1.00	1.00	0.50	0.60	0.0	0.0	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
141	1.00	1.00	1.00	0.0	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
142	1.00	1.00	1.00	0.50	0.60	0.0	0.0	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
143	1.00	1.00	1.00	0.0	0.0	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
144	1.00	1.00	1.00	1.00	0.0	0.60	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
145	1.00	1.00	1.00	0.50	0.0	0.60	0.0	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
146	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
147	1.00	1.00	1.00	0.50	0.0	1.00	0.0	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
148	1.00	1.00	1.00	0.0	0.0	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
149	1.00	1.00	1.00	0.50	0.0	0.60	0.0	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
150	1.00	1.00	1.00	0.0	0.0	0.0	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
151	1.00	1.00	1.00	1.00	0.0	0.0	0.60	0.0	1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
152	1.00	1.00	1.00	0.50	0.0	0.0	0.60	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
153	1.00	1.00	1.00	0.0	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
154	1.00	1.00	1.00	0.50	0.0	0.0	1.00	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
155	1.00	1.00	1.00	0.0	0.0	0.0	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
156	1.00	1.00	1.00	0.50	0.0	0.0	0.60	0.0	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
157	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.60	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
	0.0	0.0	0.0	1.00	0.70									
158	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.60	1.00	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
159	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.60	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
160	1.00	1.00	1.00	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
161	1.00	1.00	1.00	0.50	0.0	0.0	0.0	1.00	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
162	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.60	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
163	1.00	1.00	1.00	0.50	0.0	0.0	0.0	0.60	0.50	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	1.00									
164	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
165	1.00	1.00	1.00	0.20	0.0	0.0	0.0	0.0	0.20	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
166	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.70									
167	1.00	1.00	1.00	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
168	1.00	1.00	1.00	0.0	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
169	1.00	1.00	1.00	0.0	0.0	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
170	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.20	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									
171	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	1.00	0.60									

9. AZIONE SISMICA

VALUTAZIONE DELL' AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell' allegato alle NTC (rispettivamente media pesata e interpolazione).

L' azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

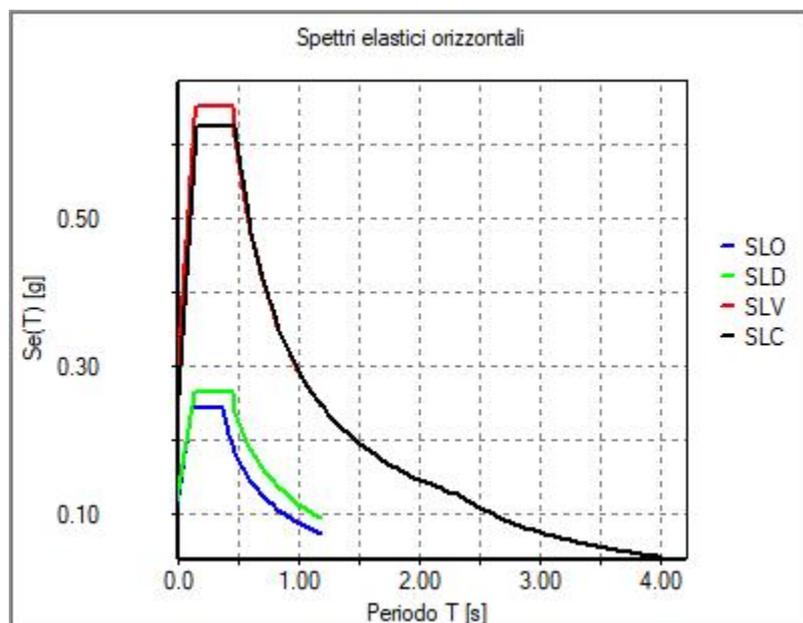
a_g : accelerazione orizzontale massima del terreno;

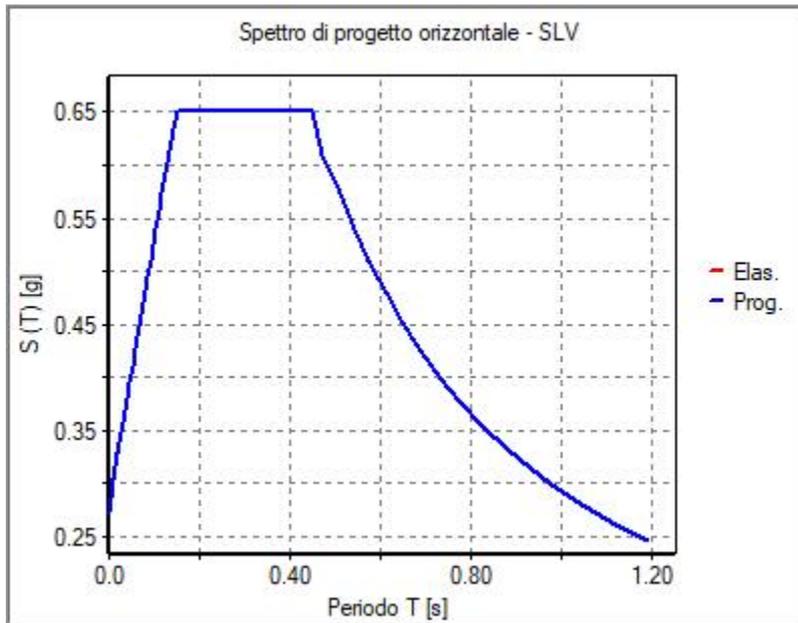
F_0 : valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T^*c : periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura					
Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
III	50.0	1.5	75.0	C	T1

A seguito di approfonditi studi geologici e geotecnici, ovvero di studi di microzonazione, si è giunti alla definizione degli spettri utilizzati per i diversi stati limite da utilizzarsi in alternativa a quelli previsti dalla normativa, ottenuti dall'indagine sismica e meglio indicati nella Relazione Geologica; si riporta la rappresentazione grafica degli spettri.





10. RISULTATI ANALISI SISMICHE

LEGENDA TABELLA ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

- 9. Esk** caso di carico sismico con analisi statica equivalente
10. Edk caso di carico sismico con analisi dinamica

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore q	Fattore di struttura/di comportamento. Dipendente dalla tipologia strutturale
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell' ordinata dello spettro in uso nel tratto costante
numero di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

- a) **analisi sismica statica equivalente:**
 - quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/Ls (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
 - azione sismica complessiva
- b) **analisi sismica dinamica con spettro di risposta:**
 - quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/Ls (per strutture a nucleo) , indici di regolarità e/r secondo EC8 4.2.3.2



- frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi
- massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione ϵ_T (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \epsilon_T/h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione ϵ_T , ϵ_P e ϵ_D degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \epsilon_T/h$ da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo la circolare n.7/2019 del C.S.LL.PP nelle combinazioni in SLC come previsto dal DM 17-01-2018. Per ogni combinazione è riportato il codice di verifica ed i valori utilizzati per la verifica: spostamento d_E , area ridotta e dimensione A_2 , azione verticale, deformazioni di taglio dell'elastomero e tensioni nell'acciaio.

Qualora si applichi l'Ordinanza 3274 e s.m.i. le verifiche sono eseguite in accordo con l'allegato 10.A. In particolare la tabella, per ogni combinazione di calcolo, riporta:

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva , NV – verifica negativa, ND – verifica non completata
dE	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta A_r (per dispositivi circolari)
V	Azione verticale agente
Ar	Area ridotta efficace
Dim A2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio
Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 1) $V > 0$
- 2) $\text{Sig } s < f_{yk}$
- 3) $\text{Gam } t < 5$
- 4) $\text{Gam } s < \text{Gam } * \text{ (caratteristica dell' elastomero)}$
- 5) $\text{Gam } s < 2$
- 6) $V < 0.5 V_{cr}$

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Calcolo dei fattori di comportamento secondo il D.M. 17/01/2018

La costruzione, nuova, è caratterizzata da regolarità sia in pianta sia in altezza ed è progettata considerando un comportamento non dissipativo (ND).

Parametri fattore in direzione x e y

Sistema costruttivo: legno
 Tipologia strutturale: pannelli di tavole incollate a strati incrociati, collegati mediante chiodi, viti, bulloni o strutture reticolari con collegamenti a mezzo di chiodi, viti, bulloni o spinotti o strutture cosiddette miste, ovvero con intelaiatura (sismo-resistente) in legno e tamponature non portanti

Valore base fattore $q_0 = 2.500$
 Fattore di regolarità $K_R = 1.0$
 Fattore dissipativo $q_D = q_0 \cdot K_R = 2.500$
 Fattore non dissipativo $q_{ND} = 2/3 \cdot q_D = 1.500 (\leq 1.5)$

Fattori di comportamento utilizzati

	Dissipativi	Non dissipativi
q SLU x	2.500	1.500
q SLU y	2.500	1.500
q SLU z	1.500	1.500

CDC	Tipo	Sigla Id	Note
10	Esk	CDC=Es (statico SLU) alfa=0.0 (ecc. +)	
			categoria suolo: da R.S.L.
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 1.229 sec.
			classe di duttilità CD: ND
			ordinata spettro Sd(T1): 0.246

Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	daN	daN	m	m	m	m	m	m			
5.40	4818.38	4818.38	1.264e+04	20.66	19.99	0.0	0.0	20.63	19.99	0.008	0.003	1.8398e-04
5.34	158.84	4977.23	421.07	15.49	19.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.26	279.73	5256.96	753.74	18.67	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.19	225.62	5482.58	616.26	15.45	19.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.11	270.51	5753.09	749.22	18.66	18.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.03	147.46	5900.55	415.41	15.42	18.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.00	682.58	6583.12	1933.82	20.83	18.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	291.82	6874.94	831.45	16.26	18.09	0.0	0.0	15.79	18.09	4.9874e-04	0.027	0.0
4.94	60.16	6935.10	172.42	40.58	17.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.93	87.38	7022.48	251.00	35.68	17.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.91	202.30	7224.78	583.78	2.75	17.81	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	278.07	7502.84	829.09	2.76	17.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	87.34	7590.19	260.60	40.58	17.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	122.10	7712.28	364.48	35.68	17.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.60	1133.53	8845.81	3490.68	21.78	17.28	0.0	-0.18	24.62	18.67	0.356	0.161	0.191
4.59	296.81	9142.62	915.37	2.96	16.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.56	83.95	9226.58	260.83	35.68	16.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	50.40	9276.97	156.82	40.58	16.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.43	1102.09	1.038e+04	3520.46	18.60	17.65	0.0	-1.24	25.46	18.10	1.381	0.236	0.026
4.40	73.82	1.045e+04	237.56	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.39	184.08	1.064e+04	593.31	5.98	15.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	131.60	1.077e+04	426.62	35.68	15.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.28	112.14	1.088e+04	371.52	-1.42	15.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.25	71.10	1.095e+04	236.88	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.20	749.50	1.170e+04	2527.89	17.34	14.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.18	124.70	1.183e+04	422.62	35.68	14.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.12	108.02	1.193e+04	371.63	-1.42	14.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	68.64	1.200e+04	237.08	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	1003.90	1.301e+04	3555.23	20.63	19.99	0.0	0.0	20.70	19.99	0.001	0.007	9.5900e-05
4.00	167.81	1.317e+04	594.53	5.98	13.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.99	117.86	1.329e+04	418.45	35.68	13.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	501.70	1.379e+04	1794.94	17.85	20.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	103.82	1.390e+04	371.52	-1.42	13.59	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	167.11	1.406e+04	598.29	29.78	20.76	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	497.17	1.456e+04	1780.38	20.85	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	65.62	1.463e+04	235.31	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.93	6.81	1.463e+04	24.54	35.68	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	491.52	1.513e+04	1780.10	20.83	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	718.10	1.584e+04	2601.56	20.76	21.58	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.87	492.17	1.634e+04	1802.89	21.03	22.29	0.0	-0.18	0.0	0.0	0.0	0.0	0.0
3.86	702.80	1.704e+04	2578.63	20.83	22.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	479.45	1.752e+04	1776.62	20.83	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	332.56	1.785e+04	1235.06	20.83	23.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	332.30	1.818e+04	1235.00	20.83	23.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	4376.70	2.256e+04	1.632e+04	20.37	13.23	0.0	-0.34	18.24	14.65	2.553	0.112	0.090
3.79	120.61	2.268e+04	451.26	35.68	12.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	111.60	2.279e+04	417.65	29.78	12.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.78	601.37	2.339e+04	2254.54	18.04	21.49	0.0	-0.57	0.0	0.0	0.0	0.0	0.0
3.77	628.20	2.402e+04	2361.97	20.83	24.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	177.88	2.420e+04	670.47	18.36	12.15	0.0	-7.00e-06	0.0	0.0	0.0	0.0	0.0
3.76	133.25	2.433e+04	502.33	11.88	12.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	110.95	2.444e+04	418.48	14.98	12.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	134.55	2.458e+04	508.03	20.83	12.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	126.26	2.470e+04	476.83	24.68	12.03	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.74	346.19	2.505e+04	1312.35	32.93	11.78	0.0	-3.74e-04	0.0	0.0	0.0	0.0	0.0
3.73	467.42	2.552e+04	1773.13	20.83	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	757.56	2.628e+04	2881.86	18.07	22.12	0.0	-0.67	0.0	0.0	0.0	0.0	0.0
3.72	176.42	2.645e+04	672.44	18.43	11.42	0.0	-1.45e-05	0.0	0.0	0.0	0.0	0.0
3.72	131.54	2.658e+04	501.54	11.88	11.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	109.41	2.669e+04	417.62	14.98	11.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	132.55	2.683e+04	507.01	20.83	11.19	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	124.33	2.695e+04	475.78	24.68	11.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	151.52	2.710e+04	581.28	29.78	11.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	461.42	2.756e+04	1771.39	20.83	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	168.31	2.773e+04	646.49	35.68	10.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	132.64	2.786e+04	510.10	7.72	10.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	343.74	2.821e+04	1322.28	23.78	25.62	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	333.82	2.854e+04	1285.10	17.88	25.67	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	158.34	2.870e+04	610.40	16.04	10.69	0.0	-2.15e-05	0.0	0.0	0.0	0.0	0.0
3.67	129.83	2.883e+04	500.76	11.88	10.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	107.87	2.894e+04	416.75	14.98	10.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	130.55	2.907e+04	505.99	20.83	10.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	118.85	2.919e+04	460.91	24.68	10.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	44.77	2.923e+04	173.75	41.88	10.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	149.48	2.938e+04	580.42	29.78	10.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	152.29	2.953e+04	591.58	35.68	10.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	455.43	2.999e+04	1769.64	20.83	26.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.64	131.00	3.012e+04	509.39	7.72	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	96.07	3.022e+04	374.61	-0.22	9.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	128.13	3.034e+04	499.97	11.88	9.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	352.29	3.070e+04	1376.25	20.91	24.50	0.0	-0.84	0.0	0.0	0.0	0.0	0.0
3.62	317.06	3.101e+04	1239.56	23.78	26.67	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.62	106.35	3.112e+04	415.89	14.98	9.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	223.76	3.134e+04	878.87	22.67	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	150.37	3.149e+04	590.83	35.68	9.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	147.45	3.164e+04	579.57	29.78	9.45	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	129.36	3.177e+04	508.67	7.72	9.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	508.04	3.228e+04	1998.36	23.26	25.03	0.0	-0.88	0.0	0.0	0.0	0.0	0.0
3.59	94.96	3.237e+04	374.61	-0.22	9.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	494.44	3.287e+04	1951.87	20.77	27.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	144.04	3.301e+04	568.73	11.88	9.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.58	104.82	3.312e+04	415.03	14.98	9.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	70.29	3.319e+04	279.28	20.83	8.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	171.47	3.336e+04	681.57	35.68	8.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	63.33	3.342e+04	251.80	24.68	8.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	127.73	3.355e+04	507.95	7.72	8.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	72.19	3.362e+04	287.16	41.88	8.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	145.43	3.377e+04	578.71	29.78	8.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	443.49	3.421e+04	1766.16	20.83	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	497.88	3.471e+04	1986.39	20.83	27.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	91.84	3.480e+04	366.54	-0.22	8.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	231.63	3.503e+04	928.63	13.26	8.22	0.0	-1.27e-04	0.0	0.0	0.0	0.0	0.0
3.52	69.48	3.510e+04	279.28	20.83	8.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	60.49	3.516e+04	243.27	24.68	8.02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	126.10	3.529e+04	507.23	7.72	8.01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	71.37	3.536e+04	287.16	41.88	8.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	168.95	3.553e+04	680.79	29.78	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	864.71	3.639e+04	3487.06	20.78	28.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	217.67	3.661e+04	878.63	21.03	7.80	0.0	-2.50e-04	0.0	0.0	0.0	0.0	0.0
3.50	96.65	3.671e+04	391.15	11.88	7.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	415.99	3.712e+04	1688.29	27.38	22.45	0.0	-1.08	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.49	101.79	3.723e+04	413.30	14.98	7.44	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	93.64	3.732e+04	380.36	11.88	29.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	194.23	3.751e+04	789.86	20.83	29.16	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	68.66	3.758e+04	279.28	20.83	7.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	59.79	3.764e+04	243.27	24.68	7.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	195.03	3.784e+04	793.68	20.08	7.30	0.0	-3.69e-04	0.0	0.0	0.0	0.0	0.0
3.48	133.25	3.797e+04	543.17	20.83	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	81.86	3.805e+04	334.25	-0.22	7.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	95.61	3.815e+04	390.66	11.88	7.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.46	139.57	3.829e+04	572.17	29.78	6.86	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	192.20	3.848e+04	788.32	20.83	29.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	471.08	3.895e+04	1933.00	20.91	29.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	100.29	3.905e+04	412.43	14.98	6.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	67.10	3.912e+04	276.19	20.83	6.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	250.21	3.937e+04	1030.18	21.10	6.59	0.0	-4.00e-04	0.0	0.0	0.0	0.0	0.0
3.44	130.43	3.950e+04	537.48	20.83	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	155.99	3.965e+04	642.94	35.68	6.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	74.54	3.973e+04	307.45	-0.22	6.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	94.57	3.982e+04	390.17	11.88	6.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	87.44	3.991e+04	361.35	29.78	6.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	173.20	4.008e+04	716.49	20.83	30.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.41	322.58	4.041e+04	1338.37	20.83	30.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	1271.49	4.168e+04	5297.49	20.62	16.75	0.0	-1.24	20.15	24.06	0.602	5.3732e-04	0.669
3.05	3451.13	4.513e+04	1.603e+04	23.08	16.50	0.0	-1.31	20.94	11.29	0.400	0.139	0.547
2.55	3.14	4.513e+04	17.46	40.58	16.51	0.0	-0.09	0.0	0.0	0.0	0.0	0.0
2.49	5.14	4.514e+04	29.22	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	3.99	4.514e+04	23.12	40.58	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	5.01	4.515e+04	29.23	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.37	4.89	4.515e+04	29.22	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.31	4.77	4.516e+04	29.23	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.27	7.45	4.516e+04	46.53	41.63	30.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	4.66	4.517e+04	29.18	41.88	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	4.65	4.517e+04	29.18	41.88	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.25	365.25	4.554e+04	2299.58	13.54	25.06	0.0	-1.11	1.11	30.28	0.156	1.958	0.941
2.24	10.90	4.555e+04	68.81	20.83	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.45	4.555e+04	34.40	41.88	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.69	4.556e+04	35.97	-0.60	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	10.86	4.557e+04	68.81	20.83	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.43	4.558e+04	34.40	41.88	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	10.83	4.559e+04	68.81	20.83	26.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	11.07	4.560e+04	70.38	20.59	22.09	0.0	-0.41	0.0	0.0	0.0	0.0	0.0
2.23	5.40	4.560e+04	34.40	-0.22	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	10.80	4.561e+04	68.81	20.83	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	5.39	4.562e+04	34.40	41.88	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	14.82	4.564e+04	94.72	11.49	24.21	0.0	-0.49	0.0	0.0	0.0	0.0	0.0
2.22	15.36	4.565e+04	98.18	25.27	25.68	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
2.21	5.37	4.566e+04	34.40	41.88	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	10.73	4.567e+04	68.81	20.83	23.92	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	10.96	4.568e+04	70.38	21.43	20.94	0.0	-0.29	0.0	0.0	0.0	0.0	0.0
2.20	10.70	4.569e+04	68.81	20.83	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	5.34	4.569e+04	34.40	-0.22	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	5.34	4.570e+04	34.40	41.88	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	10.66	4.571e+04	68.81	20.83	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	5.57	4.572e+04	35.97	2.69	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	5.32	4.572e+04	34.40	41.88	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	10.63	4.573e+04	68.81	20.83	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	19.90	4.575e+04	129.12	20.27	23.20	0.0	-0.46	0.0	0.0	0.0	0.0	0.0
2.18	14.95	4.577e+04	97.09	25.15	22.67	0.0	-0.33	0.0	0.0	0.0	0.0	0.0
2.18	5.29	4.577e+04	34.40	41.88	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	68.38	4.584e+04	445.37	19.22	20.05	0.0	-0.04	20.83	19.97	0.076	0.713	0.043
2.17	5.52	4.585e+04	35.97	4.33	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.17	4.81	4.585e+04	31.42	41.88	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	5.49	4.586e+04	35.97	5.16	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	7.68	4.586e+04	50.37	14.98	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	1134.24	4.700e+04	7473.13	22.84	13.76	0.0	-1.04	22.55	11.04	0.170	0.025	0.494
2.05	44.03	4.704e+04	304.23	3.74	5.99	0.0	-0.06	-0.18	5.90	0.052	6.800	0.099
1.30	986.99	4.803e+04	1.075e+04	20.77	17.75	0.0	-1.24	31.02	16.81	0.675	0.866	0.039
0.45	232.67	4.826e+04	7324.35	20.64	16.64	0.0	-1.24	20.46	11.88	0.520	0.011	0.459
0.33	20.59	4.828e+04	897.58	20.91	23.25	0.0	-0.43	20.83	20.06	0.336	0.029	0.799
Risulta	4.828e+04		1.962e+05									

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



CDC	Tipo	Sigla Id	Note
11	Esk	CDC=Es (statico SLU) alfa=0.0 (ecc. -)	
			categoria suolo: da R.S.L.
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 1.229 sec.
			classe di duttilità CD: ND
			ordinata spettro Sd(T1): 0.246

Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	daN	daN	m	m	m	m	m	m			
5.40	4818.38	4818.38	1.264e+04	20.66	19.99	0.0	0.0	20.63	19.99	0.008	0.003	1.8398e-04
5.34	158.84	4977.23	421.07	15.49	19.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.26	279.73	5256.96	753.74	18.67	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.19	225.62	5482.58	616.26	15.45	19.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.11	270.51	5753.09	749.22	18.66	18.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.03	147.46	5900.55	415.41	15.42	18.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.00	682.58	6583.12	1933.82	20.83	18.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	291.82	6874.94	831.45	16.26	18.09	0.0	0.0	15.79	18.09	4.9874e-04	0.027	0.0
4.94	60.16	6935.10	172.42	40.58	17.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.93	87.38	7022.48	251.00	35.68	17.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.91	202.30	7224.78	583.78	2.75	17.81	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	278.07	7502.84	829.09	2.76	17.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	87.34	7590.19	260.60	40.58	17.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	122.10	7712.28	364.48	35.68	17.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.60	1133.53	8845.81	3490.68	21.78	17.28	0.0	0.18	24.62	18.67	0.356	0.161	0.191
4.59	296.81	9142.62	915.37	2.96	16.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.56	83.95	9226.58	260.83	35.68	16.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	50.40	9276.97	156.82	40.58	16.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.43	1102.09	1.038e+04	3520.46	18.60	17.65	0.0	1.24	25.46	18.10	1.381	0.236	0.026
4.40	73.82	1.045e+04	237.56	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.39	184.08	1.064e+04	593.31	5.98	15.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	131.60	1.077e+04	426.62	35.68	15.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.28	112.14	1.088e+04	371.52	-1.42	15.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.25	71.10	1.095e+04	236.88	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.20	749.50	1.170e+04	2527.89	17.34	14.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.18	124.70	1.183e+04	422.62	35.68	14.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.12	108.02	1.193e+04	371.63	-1.42	14.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	68.64	1.200e+04	237.08	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	1003.90	1.301e+04	3555.23	20.63	19.99	0.0	0.0	20.70	19.99	0.001	0.007	9.5900e-05
4.00	167.81	1.317e+04	594.53	5.98	13.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.99	117.86	1.329e+04	418.45	35.68	13.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	501.70	1.379e+04	1794.94	17.85	20.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	103.82	1.390e+04	371.52	-1.42	13.59	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	167.11	1.406e+04	598.29	29.78	20.76	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	497.17	1.456e+04	1780.38	20.85	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	65.62	1.463e+04	235.31	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.93	6.81	1.463e+04	24.54	35.68	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	491.52	1.513e+04	1780.10	20.83	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	718.10	1.584e+04	2601.56	20.76	21.58	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.87	492.17	1.634e+04	1802.89	21.03	22.29	0.0	0.18	0.0	0.0	0.0	0.0	0.0
3.86	702.80	1.704e+04	2578.63	20.83	22.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	479.45	1.752e+04	1776.62	20.83	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	332.56	1.785e+04	1235.06	20.83	23.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	332.30	1.818e+04	1235.00	20.83	23.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	4376.70	2.256e+04	1.632e+04	20.37	13.23	0.0	0.34	18.24	14.65	2.553	0.112	0.090
3.79	120.61	2.268e+04	451.26	35.68	12.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	111.60	2.279e+04	417.65	29.78	12.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.78	601.37	2.339e+04	2254.54	18.04	21.49	0.0	0.57	0.0	0.0	0.0	0.0	0.0
3.77	628.20	2.402e+04	2361.97	20.83	24.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	177.88	2.420e+04	670.47	18.36	12.15	0.0	7.00e-06	0.0	0.0	0.0	0.0	0.0
3.76	133.25	2.433e+04	502.33	11.88	12.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	110.95	2.444e+04	418.48	14.98	12.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	134.55	2.458e+04	508.03	20.83	12.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	126.26	2.470e+04	476.83	24.68	12.03	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.74	346.19	2.505e+04	1312.35	32.93	11.78	0.0	3.74e-04	0.0	0.0	0.0	0.0	0.0
3.73	467.42	2.552e+04	1773.13	20.83	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.72	757.56	2.628e+04	2881.86	18.07	22.12	0.0	0.67	0.0	0.0	0.0	0.0	0.0
3.72	176.42	2.645e+04	672.44	18.43	11.42	0.0	1.45e-05	0.0	0.0	0.0	0.0	0.0
3.72	131.54	2.658e+04	501.54	11.88	11.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	109.41	2.669e+04	417.62	14.98	11.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	132.55	2.683e+04	507.01	20.83	11.19	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	124.33	2.695e+04	475.78	24.68	11.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	151.52	2.710e+04	581.28	29.78	11.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	461.42	2.756e+04	1771.39	20.83	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	168.31	2.773e+04	646.49	35.68	10.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	132.64	2.786e+04	510.10	7.72	10.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	343.74	2.821e+04	1322.28	23.78	25.62	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	333.82	2.854e+04	1285.10	17.88	25.67	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	158.34	2.870e+04	610.40	16.04	10.69	0.0	2.15e-05	0.0	0.0	0.0	0.0	0.0
3.67	129.83	2.883e+04	500.76	11.88	10.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	107.87	2.894e+04	416.75	14.98	10.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	130.55	2.907e+04	505.99	20.83	10.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	118.85	2.919e+04	460.91	24.68	10.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	44.77	2.923e+04	173.75	41.88	10.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	149.48	2.938e+04	580.42	29.78	10.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	152.29	2.953e+04	591.58	35.68	10.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	455.43	2.999e+04	1769.64	20.83	26.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.64	131.00	3.012e+04	509.39	7.72	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	96.07	3.022e+04	374.61	-0.22	9.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	128.13	3.034e+04	499.97	11.88	9.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	352.29	3.070e+04	1376.25	20.91	24.50	0.0	0.84	0.0	0.0	0.0	0.0	0.0
3.62	317.06	3.101e+04	1239.56	23.78	26.67	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.62	106.35	3.112e+04	415.89	14.98	9.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	223.76	3.134e+04	878.87	22.67	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	150.37	3.149e+04	590.83	35.68	9.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	147.45	3.164e+04	579.57	29.78	9.45	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	129.36	3.177e+04	508.67	7.72	9.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	508.04	3.228e+04	1998.36	23.26	25.03	0.0	0.88	0.0	0.0	0.0	0.0	0.0
3.59	94.96	3.237e+04	374.61	-0.22	9.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	494.44	3.287e+04	1951.87	20.77	27.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	144.04	3.301e+04	568.73	11.88	9.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.58	104.82	3.312e+04	415.03	14.98	9.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	70.29	3.319e+04	279.28	20.83	8.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	171.47	3.336e+04	681.57	35.68	8.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	63.33	3.342e+04	251.80	24.68	8.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	127.73	3.355e+04	507.95	7.72	8.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	72.19	3.362e+04	287.16	41.88	8.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	145.43	3.377e+04	578.71	29.78	8.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	443.49	3.421e+04	1766.16	20.83	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	497.88	3.471e+04	1986.39	20.83	27.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	91.84	3.480e+04	366.54	-0.22	8.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	231.63	3.503e+04	928.63	13.26	8.22	0.0	1.27e-04	0.0	0.0	0.0	0.0	0.0
3.52	69.48	3.510e+04	279.28	20.83	8.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	60.49	3.516e+04	243.27	24.68	8.02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	126.10	3.529e+04	507.23	7.72	8.01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	71.37	3.536e+04	287.16	41.88	8.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	168.95	3.553e+04	680.79	29.78	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	864.71	3.639e+04	3487.06	20.78	28.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	217.67	3.661e+04	878.63	21.03	7.80	0.0	2.50e-04	0.0	0.0	0.0	0.0	0.0
3.50	96.65	3.671e+04	391.15	11.88	7.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	415.99	3.712e+04	1688.29	27.38	22.45	0.0	1.08	0.0	0.0	0.0	0.0	0.0
3.49	101.79	3.723e+04	413.30	14.98	7.44	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	93.64	3.732e+04	380.36	11.88	29.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	194.23	3.751e+04	789.86	20.83	29.16	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	68.66	3.758e+04	279.28	20.83	7.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	59.79	3.764e+04	243.27	24.68	7.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	195.03	3.784e+04	793.68	20.08	7.30	0.0	3.69e-04	0.0	0.0	0.0	0.0	0.0
3.48	133.25	3.797e+04	543.17	20.83	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	81.86	3.805e+04	334.25	-0.22	7.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	95.61	3.815e+04	390.66	11.88	7.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.46	139.57	3.829e+04	572.17	29.78	6.86	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	192.20	3.848e+04	788.32	20.83	29.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	471.08	3.895e+04	1933.00	20.91	29.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	100.29	3.905e+04	412.43	14.98	6.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	67.10	3.912e+04	276.19	20.83	6.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	250.21	3.937e+04	1030.18	21.10	6.59	0.0	4.00e-04	0.0	0.0	0.0	0.0	0.0
3.44	130.43	3.950e+04	537.48	20.83	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	155.99	3.965e+04	642.94	35.68	6.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.43	74.54	3.973e+04	307.45	-0.22	6.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	94.57	3.982e+04	390.17	11.88	6.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	87.44	3.991e+04	361.35	29.78	6.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	173.20	4.008e+04	716.49	20.83	30.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.41	322.58	4.041e+04	1338.37	20.83	30.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	1271.49	4.168e+04	5297.49	20.62	16.75	0.0	1.24	20.15	24.06	0.602	5.3732e-04	0.669
3.05	3451.13	4.513e+04	1.603e+04	23.08	16.50	0.0	1.31	20.94	11.29	0.400	0.139	0.547
2.55	3.14	4.513e+04	17.46	40.58	16.51	0.0	0.09	0.0	0.0	0.0	0.0	0.0
2.49	5.14	4.514e+04	29.22	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	3.99	4.514e+04	23.12	40.58	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	5.01	4.515e+04	29.23	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.37	4.89	4.515e+04	29.22	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.31	4.77	4.516e+04	29.23	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.27	7.45	4.516e+04	46.53	41.63	30.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	4.66	4.517e+04	29.18	41.88	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	4.65	4.517e+04	29.18	41.88	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.25	365.25	4.554e+04	2299.58	13.54	25.06	0.0	1.11	1.11	30.28	0.156	1.958	0.941
2.24	10.90	4.555e+04	68.81	20.83	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.45	4.555e+04	34.40	41.88	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.69	4.556e+04	35.97	-0.60	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	10.86	4.557e+04	68.81	20.83	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.43	4.558e+04	34.40	41.88	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	10.83	4.559e+04	68.81	20.83	26.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	11.07	4.560e+04	70.38	20.59	22.09	0.0	0.41	0.0	0.0	0.0	0.0	0.0
2.23	5.40	4.560e+04	34.40	-0.22	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	10.80	4.561e+04	68.81	20.83	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	5.39	4.562e+04	34.40	41.88	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	14.82	4.564e+04	94.72	11.49	24.21	0.0	0.49	0.0	0.0	0.0	0.0	0.0
2.22	15.36	4.565e+04	98.18	25.27	25.68	0.0	0.16	0.0	0.0	0.0	0.0	0.0
2.21	5.37	4.566e+04	34.40	41.88	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	10.73	4.567e+04	68.81	20.83	23.92	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	10.96	4.568e+04	70.38	21.43	20.94	0.0	0.29	0.0	0.0	0.0	0.0	0.0
2.20	10.70	4.569e+04	68.81	20.83	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	5.34	4.569e+04	34.40	-0.22	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	5.34	4.570e+04	34.40	41.88	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	10.66	4.571e+04	68.81	20.83	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	5.57	4.572e+04	35.97	2.69	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	5.32	4.572e+04	34.40	41.88	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	10.63	4.573e+04	68.81	20.83	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	19.90	4.575e+04	129.12	20.27	23.20	0.0	0.46	0.0	0.0	0.0	0.0	0.0
2.18	14.95	4.577e+04	97.09	25.15	22.67	0.0	0.33	0.0	0.0	0.0	0.0	0.0
2.18	5.29	4.577e+04	34.40	41.88	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	68.38	4.584e+04	445.37	19.22	20.05	0.0	0.04	20.83	19.97	0.076	0.713	0.043
2.17	5.52	4.585e+04	35.97	4.33	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.17	4.81	4.585e+04	31.42	41.88	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	5.49	4.586e+04	35.97	5.16	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	7.68	4.586e+04	50.37	14.98	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	1134.24	4.700e+04	7473.13	22.84	13.76	0.0	1.04	22.55	11.04	0.170	0.025	0.494
2.05	44.03	4.704e+04	304.23	3.74	5.99	0.0	0.06	-0.18	5.90	0.052	6.800	0.099
1.30	986.99	4.803e+04	1.075e+04	20.77	17.75	0.0	1.24	31.02	16.81	0.675	0.866	0.039
0.45	232.67	4.826e+04	7324.35	20.64	16.64	0.0	1.24	20.46	11.88	0.520	0.011	0.459
0.33	20.59	4.828e+04	897.58	20.91	23.25	0.0	0.43	20.83	20.06	0.336	0.029	0.799
Risulta	4.828e+04		1.962e+05									

CDC	Tipo	Sigla Id	Note
12	Esk	CDC=Es (statico SLU) alfa=90.00 (ecc. +)	
			categoria suolo: da R.S.L.
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.422 sec.
			classe di duttilità CD: ND
			ordinata spettro Sd(T1): 0.651

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	daN	daN	m	m	m	m	m	m			
5.40	1.275e+04	1.275e+04	1.264e+04	20.66	19.99	2.10	0.0	20.63	19.99	0.008	0.003	1.8398e-04
5.34	420.25	1.317e+04	421.07	15.49	19.74	2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.26	740.09	1.391e+04	753.74	18.67	19.35	1.49	0.0	0.0	0.0	0.0	0.0	0.0
5.19	596.91	1.451e+04	616.26	15.45	19.04	2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.11	715.68	1.522e+04	749.22	18.66	18.72	1.49	0.0	0.0	0.0	0.0	0.0	0.0
5.03	390.12	1.561e+04	415.41	15.42	18.34	2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.00	1805.87	1.742e+04	1933.82	20.83	18.21	1.19	0.0	0.0	0.0	0.0	0.0	0.0
4.97	772.06	1.819e+04	831.45	16.26	18.09	2.10	0.0	15.79	18.09	4.9874e-04	0.027	0.0
4.94	159.16	1.835e+04	172.42	40.58	17.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.93	231.17	1.858e+04	251.00	35.68	17.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.91	535.21	1.911e+04	583.78	2.75	17.81	0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.75	735.68	1.985e+04	829.09	2.76	17.11	0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.75	231.08	2.008e+04	260.60	40.58	17.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	323.03	2.040e+04	364.48	35.68	17.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.60	2998.95	2.340e+04	3490.68	21.78	17.28	2.10	0.0	24.62	18.67	0.356	0.161	0.191
4.59	785.26	2.419e+04	915.37	2.96	16.41	0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.56	222.11	2.441e+04	260.83	35.68	16.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	133.34	2.454e+04	156.82	40.58	16.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.43	2915.77	2.746e+04	3520.46	18.60	17.65	2.17	0.0	25.46	18.10	1.381	0.236	0.026
4.40	195.31	2.765e+04	237.56	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.39	487.00	2.814e+04	593.31	5.98	15.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	348.16	2.849e+04	426.62	35.68	15.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.28	296.70	2.879e+04	371.52	-1.42	15.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.25	188.10	2.897e+04	236.88	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.20	1982.93	3.096e+04	2527.89	17.34	14.66	1.34	0.0	0.0	0.0	0.0	0.0	0.0
4.18	329.91	3.129e+04	422.62	35.68	14.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.12	285.78	3.157e+04	371.63	-1.42	14.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	181.59	3.176e+04	237.08	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	2656.00	3.441e+04	3555.23	20.63	19.99	2.17	0.0	20.70	19.99	0.001	0.007	9.5900e-05
4.00	443.96	3.486e+04	594.53	5.98	13.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.99	311.82	3.517e+04	418.45	35.68	13.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	1327.33	3.649e+04	1794.94	17.85	20.71	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.96	274.68	3.677e+04	371.52	-1.42	13.59	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	442.11	3.721e+04	598.29	29.78	20.76	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	1315.34	3.853e+04	1780.38	20.85	20.77	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.95	173.62	3.870e+04	235.31	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.93	18.03	3.872e+04	24.54	35.68	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	1300.40	4.002e+04	1780.10	20.83	21.56	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.91	1899.86	4.192e+04	2601.56	20.76	21.58	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.87	1302.13	4.322e+04	1802.89	21.03	22.29	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.86	1859.38	4.508e+04	2578.63	20.83	22.46	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.82	1268.46	4.635e+04	1776.62	20.83	23.13	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.81	879.84	4.723e+04	1235.06	20.83	23.28	0.90	0.0	0.0	0.0	0.0	0.0	0.0
3.81	879.15	4.811e+04	1235.00	20.83	23.33	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.80	1.158e+04	5.969e+04	1.632e+04	20.37	13.23	2.17	0.0	18.24	14.65	2.553	0.112	0.090
3.79	319.09	6.001e+04	451.26	35.68	12.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	295.26	6.030e+04	417.65	29.78	12.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.78	1591.02	6.189e+04	2254.54	18.04	21.49	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.77	1662.02	6.355e+04	2361.97	20.83	24.11	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.76	470.61	6.402e+04	670.47	18.36	12.15	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.76	352.53	6.438e+04	502.33	11.88	12.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	293.53	6.467e+04	418.48	14.98	12.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	355.97	6.503e+04	508.03	20.83	12.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	334.04	6.536e+04	476.83	24.68	12.03	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.74	915.92	6.628e+04	1312.35	32.93	11.78	0.29	0.0	0.0	0.0	0.0	0.0	0.0
3.73	1236.63	6.751e+04	1773.13	20.83	24.70	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.72	2004.25	6.952e+04	2881.86	18.07	22.12	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.72	466.74	6.998e+04	672.44	18.43	11.42	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.72	348.00	7.033e+04	501.54	11.88	11.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	289.46	7.062e+04	417.62	14.98	11.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	350.68	7.097e+04	507.01	20.83	11.19	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	328.95	7.130e+04	475.78	24.68	11.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	400.86	7.170e+04	581.28	29.78	11.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	1220.76	7.292e+04	1771.39	20.83	25.49	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.69	445.30	7.337e+04	646.49	35.68	10.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	350.93	7.372e+04	510.10	7.72	10.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	909.43	7.463e+04	1322.28	23.78	25.62	1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.68	883.18	7.551e+04	1285.10	17.88	25.67	1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.67	418.91	7.593e+04	610.40	16.04	10.69	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.67	343.48	7.627e+04	500.76	11.88	10.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	285.40	7.656e+04	416.75	14.98	10.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.65	345.40	7.690e+04	505.99	20.83	10.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	314.45	7.722e+04	460.91	24.68	10.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	118.45	7.734e+04	173.75	41.88	10.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	395.48	7.773e+04	580.42	29.78	10.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	402.91	7.814e+04	591.58	35.68	10.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	1204.91	7.934e+04	1769.64	20.83	26.28	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.64	346.59	7.969e+04	509.39	7.72	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	254.17	7.994e+04	374.61	-0.22	9.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	338.98	8.028e+04	499.97	11.88	9.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	932.06	8.121e+04	1376.25	20.91	24.50	1.79	0.0	0.0	0.0	0.0	0.0	0.0
3.62	838.84	8.205e+04	1239.56	23.78	26.67	1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.62	281.36	8.233e+04	415.89	14.98	9.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	592.00	8.293e+04	878.87	22.67	9.50	0.19	0.0	0.0	0.0	0.0	0.0	0.0
3.61	397.82	8.332e+04	590.83	35.68	9.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	390.11	8.371e+04	579.57	29.78	9.45	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	342.25	8.406e+04	508.67	7.72	9.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	1344.12	8.540e+04	1998.36	23.26	25.03	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.59	251.24	8.565e+04	374.61	-0.22	9.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	1308.12	8.696e+04	1951.87	20.77	27.29	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.59	381.09	8.734e+04	568.73	11.88	9.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.58	277.33	8.762e+04	415.03	14.98	9.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	185.97	8.780e+04	279.28	20.83	8.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	453.65	8.826e+04	681.57	35.68	8.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	167.56	8.842e+04	251.80	24.68	8.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	337.92	8.876e+04	507.95	7.72	8.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	191.00	8.895e+04	287.16	41.88	8.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	384.75	8.934e+04	578.71	29.78	8.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	1173.32	9.051e+04	1766.16	20.83	27.85	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.55	1317.22	9.183e+04	1986.39	20.83	27.96	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.55	242.97	9.207e+04	366.54	-0.22	8.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	612.83	9.268e+04	928.63	13.26	8.22	0.15	0.0	0.0	0.0	0.0	0.0	0.0
3.52	183.81	9.287e+04	279.28	20.83	8.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	160.04	9.303e+04	243.27	24.68	8.02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	333.61	9.336e+04	507.23	7.72	8.01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	188.83	9.355e+04	287.16	41.88	8.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	446.99	9.400e+04	680.79	29.78	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	2287.74	9.629e+04	3487.06	20.78	28.64	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.51	575.89	9.686e+04	878.63	21.03	7.80	1.79	0.0	0.0	0.0	0.0	0.0	0.0
3.50	255.70	9.712e+04	391.15	11.88	7.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	1100.57	9.822e+04	1688.29	27.38	22.45	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.49	269.31	9.849e+04	413.30	14.98	7.44	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	247.75	9.873e+04	380.36	11.88	29.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	513.87	9.925e+04	789.86	20.83	29.16	0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.48	181.66	9.943e+04	279.28	20.83	7.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	158.18	9.959e+04	243.27	24.68	7.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	515.98	1.001e+05	793.68	20.08	7.30	1.71	0.0	0.0	0.0	0.0	0.0	0.0
3.48	352.54	1.005e+05	543.17	20.83	29.30	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.47	216.57	1.007e+05	334.25	-0.22	7.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	252.94	1.009e+05	390.66	11.88	7.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.46	369.26	1.013e+05	572.17	29.78	6.86	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	508.51	1.018e+05	788.32	20.83	29.68	0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.45	1246.33	1.031e+05	1933.00	20.91	29.71	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.44	265.32	1.033e+05	412.43	14.98	6.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	177.52	1.035e+05	276.19	20.83	6.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	661.97	1.042e+05	1030.18	21.10	6.59	1.71	0.0	0.0	0.0	0.0	0.0	0.0
3.44	345.07	1.045e+05	537.48	20.83	29.97	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.44	412.70	1.049e+05	642.94	35.68	6.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	197.22	1.051e+05	307.45	-0.22	6.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	250.19	1.054e+05	390.17	11.88	6.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	231.33	1.056e+05	361.35	29.78	6.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	458.22	1.060e+05	716.49	20.83	30.21	0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.41	853.43	1.069e+05	1338.37	20.83	30.38	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.40	3363.95	1.103e+05	5297.49	20.62	16.75	2.10	0.0	20.15	24.06	0.602	5.3732e-04	0.669
3.05	9130.57	1.194e+05	1.603e+04	23.08	16.50	2.25	0.0	20.94	11.29	0.400	0.139	0.547
2.55	8.31	1.194e+05	17.46	40.58	16.51	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.49	13.59	1.194e+05	29.22	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	10.57	1.194e+05	23.12	40.58	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	13.26	1.194e+05	29.23	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.37	12.94	1.195e+05	29.22	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.31	12.61	1.195e+05	29.23	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.27	19.71	1.195e+05	46.53	41.63	30.64	0.04	0.0	0.0	0.0	0.0	0.0	0.0
2.26	12.33	1.195e+05	29.18	41.88	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
2.26	12.30	1.195e+05	29.18	41.88	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.25	966.34	1.205e+05	2299.58	13.54	25.06	2.16	0.0	1.11	30.28	0.156	1.958	0.941
2.24	28.83	1.205e+05	68.81	20.83	27.85	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.24	14.41	1.205e+05	34.40	41.88	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	15.04	1.205e+05	35.97	-0.60	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	28.74	1.206e+05	68.81	20.83	27.06	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.24	14.36	1.206e+05	34.40	41.88	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	28.65	1.206e+05	68.81	20.83	26.28	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.23	29.28	1.206e+05	70.38	20.59	22.09	2.08	0.0	0.0	0.0	0.0	0.0	0.0
2.23	14.30	1.207e+05	34.40	-0.22	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	28.56	1.207e+05	68.81	20.83	25.49	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.22	14.27	1.207e+05	34.40	41.88	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	39.21	1.207e+05	94.72	11.49	24.21	1.44	0.0	0.0	0.0	0.0	0.0	0.0
2.22	40.63	1.208e+05	98.18	25.27	25.68	0.88	0.0	0.0	0.0	0.0	0.0	0.0
2.21	14.22	1.208e+05	34.40	41.88	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	28.39	1.208e+05	68.81	20.83	23.92	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.21	28.99	1.208e+05	70.38	21.43	20.94	2.00	0.0	0.0	0.0	0.0	0.0	0.0
2.20	28.30	1.209e+05	68.81	20.83	23.13	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.20	14.14	1.209e+05	34.40	-0.22	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	14.13	1.209e+05	34.40	41.88	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	28.21	1.209e+05	68.81	20.83	22.34	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.19	14.74	1.209e+05	35.97	2.69	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	14.08	1.210e+05	34.40	41.88	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	28.13	1.210e+05	68.81	20.83	21.56	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.18	52.65	1.210e+05	129.12	20.27	23.20	1.92	0.0	0.0	0.0	0.0	0.0	0.0
2.18	39.56	1.211e+05	97.09	25.15	22.67	0.88	0.0	0.0	0.0	0.0	0.0	0.0
2.18	13.98	1.211e+05	34.40	41.88	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	180.92	1.213e+05	445.37	19.22	20.05	1.32	0.0	20.83	19.97	0.076	0.713	0.043
2.17	14.59	1.213e+05	35.97	4.33	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.17	12.73	1.213e+05	31.42	41.88	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	14.52	1.213e+05	35.97	5.16	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	20.31	1.213e+05	50.37	14.98	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	3000.83	1.243e+05	7473.13	22.84	13.76	2.17	0.0	22.55	11.04	0.170	0.025	0.494
2.05	116.48	1.245e+05	304.23	3.74	5.99	0.44	0.0	-0.18	5.90	0.052	6.800	0.099
1.30	2611.26	1.271e+05	1.075e+04	20.77	17.75	2.17	0.0	31.02	16.81	0.675	0.866	0.039
0.45	615.58	1.277e+05	7324.35	20.64	16.64	2.17	0.0	20.46	11.88	0.520	0.011	0.459
0.33	54.48	1.277e+05	897.58	20.91	23.25	0.72	0.0	20.83	20.06	0.336	0.029	0.799
Risulta	1.277e+05		1.962e+05									

CDC	Tipo	Sigla Id	Note
13	Esk	CDC=Es (statico SLU) alfa=90.00 (ecc. -)	
			categoria suolo: da R.S.L.
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.422 sec.
			classe di duttilità CD: ND
			ordinata spettro Sd(T1): 0.651

Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	daN	daN	m	m	m	m	m	m			
5.40	1.275e+04	1.275e+04	1.264e+04	20.66	19.99	-2.10	0.0	20.63	19.99	0.008	0.003	1.8398e-04
5.34	420.25	1.317e+04	421.07	15.49	19.74	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.26	740.09	1.391e+04	753.74	18.67	19.35	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
5.19	596.91	1.451e+04	616.26	15.45	19.04	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.11	715.68	1.522e+04	749.22	18.66	18.72	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
5.03	390.12	1.561e+04	415.41	15.42	18.34	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.00	1805.87	1.742e+04	1933.82	20.83	18.21	-1.19	0.0	0.0	0.0	0.0	0.0	0.0
4.97	772.06	1.819e+04	831.45	16.26	18.09	-2.10	0.0	15.79	18.09	4.9874e-04	0.027	0.0
4.94	159.16	1.835e+04	172.42	40.58	17.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.93	231.17	1.858e+04	251.00	35.68	17.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.91	535.21	1.911e+04	583.78	2.75	17.81	-0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.75	735.68	1.985e+04	829.09	2.76	17.11	-0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.75	231.08	2.008e+04	260.60	40.58	17.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	323.03	2.040e+04	364.48	35.68	17.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
4.60	2998.95	2.340e+04	3490.68	21.78	17.28	-2.10	0.0	24.62	18.67	0.356	0.161	0.191
4.59	785.26	2.419e+04	915.37	2.96	16.41	-0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.56	222.11	2.441e+04	260.83	35.68	16.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	133.34	2.454e+04	156.82	40.58	16.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.43	2915.77	2.746e+04	3520.46	18.60	17.65	-2.17	0.0	25.46	18.10	1.381	0.236	0.026
4.40	195.31	2.765e+04	237.56	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.39	487.00	2.814e+04	593.31	5.98	15.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	348.16	2.849e+04	426.62	35.68	15.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.28	296.70	2.879e+04	371.52	-1.42	15.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.25	188.10	2.897e+04	236.88	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.20	1982.93	3.096e+04	2527.89	17.34	14.66	-1.34	0.0	0.0	0.0	0.0	0.0	0.0
4.18	329.91	3.129e+04	422.62	35.68	14.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.12	285.78	3.157e+04	371.63	-1.42	14.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	181.59	3.176e+04	237.08	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	2656.00	3.441e+04	3555.23	20.63	19.99	-2.17	0.0	20.70	19.99	0.001	0.007	9.5900e-05
4.00	443.96	3.486e+04	594.53	5.98	13.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.99	311.82	3.517e+04	418.45	35.68	13.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	1327.33	3.649e+04	1794.94	17.85	20.71	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.96	274.68	3.677e+04	371.52	-1.42	13.59	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	442.11	3.721e+04	598.29	29.78	20.76	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	1315.34	3.853e+04	1780.38	20.85	20.77	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.95	173.62	3.870e+04	235.31	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.93	18.03	3.872e+04	24.54	35.68	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	1300.40	4.002e+04	1780.10	20.83	21.56	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.91	1899.86	4.192e+04	2601.56	20.76	21.58	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.87	1302.13	4.322e+04	1802.89	21.03	22.29	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.86	1859.38	4.508e+04	2578.63	20.83	22.46	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.82	1268.46	4.635e+04	1776.62	20.83	23.13	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.81	879.84	4.723e+04	1235.06	20.83	23.28	-0.90	0.0	0.0	0.0	0.0	0.0	0.0
3.81	879.15	4.811e+04	1235.00	20.83	23.33	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.80	1.158e+04	5.969e+04	1.632e+04	20.37	13.23	-2.17	0.0	18.24	14.65	2.553	0.112	0.090
3.79	319.09	6.001e+04	451.26	35.68	12.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	295.26	6.030e+04	417.65	29.78	12.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.78	1591.02	6.189e+04	2254.54	18.04	21.49	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.77	1662.02	6.355e+04	2361.97	20.83	24.11	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.76	470.61	6.402e+04	670.47	18.36	12.15	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.76	352.53	6.438e+04	502.33	11.88	12.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	293.53	6.467e+04	418.48	14.98	12.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	355.97	6.503e+04	508.03	20.83	12.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	334.04	6.536e+04	476.83	24.68	12.03	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.74	915.92	6.628e+04	1312.35	32.93	11.78	-0.29	0.0	0.0	0.0	0.0	0.0	0.0
3.73	1236.63	6.751e+04	1773.13	20.83	24.70	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.72	2004.25	6.952e+04	2881.86	18.07	22.12	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.72	466.74	6.998e+04	672.44	18.43	11.42	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.72	348.00	7.033e+04	501.54	11.88	11.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	289.46	7.062e+04	417.62	14.98	11.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	350.68	7.097e+04	507.01	20.83	11.19	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	328.95	7.130e+04	475.78	24.68	11.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	400.86	7.170e+04	581.28	29.78	11.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	1220.76	7.292e+04	1771.39	20.83	25.49	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.69	445.30	7.337e+04	646.49	35.68	10.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	350.93	7.372e+04	510.10	7.72	10.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	909.43	7.463e+04	1322.28	23.78	25.62	-1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.68	883.18	7.551e+04	1285.10	17.88	25.67	-1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.67	418.91	7.593e+04	610.40	16.04	10.69	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.67	343.48	7.627e+04	500.76	11.88	10.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	285.40	7.656e+04	416.75	14.98	10.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	345.40	7.690e+04	505.99	20.83	10.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	314.45	7.722e+04	460.91	24.68	10.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	118.45	7.734e+04	173.75	41.88	10.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	395.48	7.773e+04	580.42	29.78	10.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	402.91	7.814e+04	591.58	35.68	10.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	1204.91	7.934e+04	1769.64	20.83	26.28	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.64	346.59	7.969e+04	509.39	7.72	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	254.17	7.994e+04	374.61	-0.22	9.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	338.98	8.028e+04	499.97	11.88	9.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	932.06	8.121e+04	1376.25	20.91	24.50	-1.79	0.0	0.0	0.0	0.0	0.0	0.0
3.62	838.84	8.205e+04	1239.56	23.78	26.67	-1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.62	281.36	8.233e+04	415.89	14.98	9.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	592.00	8.293e+04	878.87	22.67	9.50	-0.19	0.0	0.0	0.0	0.0	0.0	0.0
3.61	397.82	8.332e+04	590.83	35.68	9.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	390.11	8.371e+04	579.57	29.78	9.45	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.60	342.25	8.406e+04	508.67	7.72	9.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	1344.12	8.540e+04	1998.36	23.26	25.03	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.59	251.24	8.565e+04	374.61	-0.22	9.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	1308.12	8.696e+04	1951.87	20.77	27.29	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.59	381.09	8.734e+04	568.73	11.88	9.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.58	277.33	8.762e+04	415.03	14.98	9.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	185.97	8.780e+04	279.28	20.83	8.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	453.65	8.826e+04	681.57	35.68	8.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	167.56	8.842e+04	251.80	24.68	8.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	337.92	8.876e+04	507.95	7.72	8.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	191.00	8.895e+04	287.16	41.88	8.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	384.75	8.934e+04	578.71	29.78	8.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	1173.32	9.051e+04	1766.16	20.83	27.85	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.55	1317.22	9.183e+04	1986.39	20.83	27.96	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.55	242.97	9.207e+04	366.54	-0.22	8.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	612.83	9.268e+04	928.63	13.26	8.22	-0.15	0.0	0.0	0.0	0.0	0.0	0.0
3.52	183.81	9.287e+04	279.28	20.83	8.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	160.04	9.303e+04	243.27	24.68	8.02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	333.61	9.336e+04	507.23	7.72	8.01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	188.83	9.355e+04	287.16	41.88	8.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	446.99	9.400e+04	680.79	29.78	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	2287.74	9.629e+04	3487.06	20.78	28.64	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.51	575.89	9.686e+04	878.63	21.03	7.80	-1.79	0.0	0.0	0.0	0.0	0.0	0.0
3.50	255.70	9.712e+04	391.15	11.88	7.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	1100.57	9.822e+04	1688.29	27.38	22.45	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.49	269.31	9.849e+04	413.30	14.98	7.44	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	247.75	9.873e+04	380.36	11.88	29.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	513.87	9.925e+04	789.86	20.83	29.16	-0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.48	181.66	9.943e+04	279.28	20.83	7.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	158.18	9.959e+04	243.27	24.68	7.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	515.98	1.001e+05	793.68	20.08	7.30	-1.71	0.0	0.0	0.0	0.0	0.0	0.0
3.48	352.54	1.005e+05	543.17	20.83	29.30	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.47	216.57	1.007e+05	334.25	-0.22	7.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	252.94	1.009e+05	390.66	11.88	7.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.46	369.26	1.013e+05	572.17	29.78	6.86	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	508.51	1.018e+05	788.32	20.83	29.68	-0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.45	1246.33	1.031e+05	1933.00	20.91	29.71	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.44	265.32	1.033e+05	412.43	14.98	6.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	177.52	1.035e+05	276.19	20.83	6.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	661.97	1.042e+05	1030.18	21.10	6.59	-1.71	0.0	0.0	0.0	0.0	0.0	0.0
3.44	345.07	1.045e+05	537.48	20.83	29.97	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.44	412.70	1.049e+05	642.94	35.68	6.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	197.22	1.051e+05	307.45	-0.22	6.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	250.19	1.054e+05	390.17	11.88	6.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	231.33	1.056e+05	361.35	29.78	6.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	458.22	1.060e+05	716.49	20.83	30.21	-0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.41	853.43	1.069e+05	1338.37	20.83	30.38	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.40	3363.95	1.103e+05	5297.49	20.62	16.75	-2.10	0.0	20.15	24.06	0.602	5.3732e-04	0.669
3.05	9130.57	1.194e+05	1.603e+04	23.08	16.50	-2.25	0.0	20.94	11.29	0.400	0.139	0.547
2.55	8.31	1.194e+05	17.46	40.58	16.51	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.49	13.59	1.194e+05	29.22	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	10.57	1.194e+05	23.12	40.58	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	13.26	1.194e+05	29.23	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.37	12.94	1.195e+05	29.22	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.31	12.61	1.195e+05	29.23	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.27	19.71	1.195e+05	46.53	41.63	30.64	-0.04	0.0	0.0	0.0	0.0	0.0	0.0
2.26	12.33	1.195e+05	29.18	41.88	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	12.30	1.195e+05	29.18	41.88	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.25	966.34	1.205e+05	2299.58	13.54	25.06	-2.16	0.0	1.11	30.28	0.156	1.958	0.941
2.24	28.83	1.205e+05	68.81	20.83	27.85	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.24	14.41	1.205e+05	34.40	41.88	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	15.04	1.205e+05	35.97	-0.60	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	28.74	1.206e+05	68.81	20.83	27.06	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.24	14.36	1.206e+05	34.40	41.88	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	28.65	1.206e+05	68.81	20.83	26.28	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.23	29.28	1.206e+05	70.38	20.59	22.09	-2.08	0.0	0.0	0.0	0.0	0.0	0.0
2.23	14.30	1.207e+05	34.40	-0.22	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	28.56	1.207e+05	68.81	20.83	25.49	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.22	14.27	1.207e+05	34.40	41.88	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	39.21	1.207e+05	94.72	11.49	24.21	-1.44	0.0	0.0	0.0	0.0	0.0	0.0
2.22	40.63	1.208e+05	98.18	25.27	25.68	-0.88	0.0	0.0	0.0	0.0	0.0	0.0
2.21	14.22	1.208e+05	34.40	41.88	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
2.21	28.39	1.208e+05	68.81	20.83	23.92	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.21	28.99	1.208e+05	70.38	21.43	20.94	-2.00	0.0	0.0	0.0	0.0	0.0	0.0
2.20	28.30	1.209e+05	68.81	20.83	23.13	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.20	14.14	1.209e+05	34.40	-0.22	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	14.13	1.209e+05	34.40	41.88	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	28.21	1.209e+05	68.81	20.83	22.34	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.19	14.74	1.209e+05	35.97	2.69	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	14.08	1.210e+05	34.40	41.88	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	28.13	1.210e+05	68.81	20.83	21.56	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.18	52.65	1.210e+05	129.12	20.27	23.20	-1.92	0.0	0.0	0.0	0.0	0.0	0.0
2.18	39.56	1.211e+05	97.09	25.15	22.67	-0.88	0.0	0.0	0.0	0.0	0.0	0.0
2.18	13.98	1.211e+05	34.40	41.88	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	180.92	1.213e+05	445.37	19.22	20.05	-1.32	0.0	20.83	19.97	0.076	0.713	0.043
2.17	14.59	1.213e+05	35.97	4.33	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.17	12.73	1.213e+05	31.42	41.88	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	14.52	1.213e+05	35.97	5.16	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	20.31	1.213e+05	50.37	14.98	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	3000.83	1.243e+05	7473.13	22.84	13.76	-2.17	0.0	22.55	11.04	0.170	0.025	0.494
2.05	116.48	1.245e+05	304.23	3.74	5.99	-0.44	0.0	-0.18	5.90	0.052	6.800	0.099
1.30	2611.26	1.271e+05	1.075e+04	20.77	17.75	-2.17	0.0	31.02	16.81	0.675	0.866	0.039
0.45	615.58	1.277e+05	7324.35	20.64	16.64	-2.17	0.0	20.46	11.88	0.520	0.011	0.459
0.33	54.48	1.277e+05	897.58	20.91	23.25	-0.72	0.0	20.83	20.06	0.336	0.029	0.799
Risulta	1.277e+05		1.962e+05									

CDC	Tipo	Sigla Id	Note
14	Esk	CDC=Es (statico SLD) alfa=0.0 (ecc. +)	
			categoria suolo: da R.S.L.
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 1.229 sec.
			ordinata spettro Se(T1): 0.096

Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	daN	daN	m	m	m	m	m	m			
5.40	1882.32	1882.32	1.264e+04	20.66	19.99	0.0	0.0	20.63	19.99	0.008	0.003	1.8398e-04
5.34	62.05	1944.38	421.07	15.49	19.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.26	109.28	2053.65	753.74	18.67	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.19	88.14	2141.79	616.26	15.45	19.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.11	105.68	2247.47	749.22	18.66	18.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.03	57.60	2305.07	415.41	15.42	18.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.00	266.65	2571.72	1933.82	20.83	18.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	114.00	2685.73	831.45	16.26	18.09	0.0	0.0	15.79	18.09	4.9874e-04	0.027	0.0
4.94	23.50	2709.23	172.42	40.58	17.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.93	34.13	2743.36	251.00	35.68	17.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.91	79.03	2822.39	583.78	2.75	17.81	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	108.63	2931.02	829.09	2.76	17.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	34.12	2965.14	260.60	40.58	17.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	47.70	3012.84	364.48	35.68	17.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.60	442.82	3455.65	3490.68	21.78	17.28	0.0	-0.18	24.62	18.67	0.356	0.161	0.191
4.59	115.95	3571.60	915.37	2.96	16.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.56	32.80	3604.40	260.83	35.68	16.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	19.69	3624.09	156.82	40.58	16.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.43	430.54	4054.63	3520.46	18.60	17.65	0.0	-1.24	25.46	18.10	1.381	0.236	0.026
4.40	28.84	4083.47	237.56	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.39	71.91	4155.38	593.31	5.98	15.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	51.41	4206.78	426.62	35.68	15.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.28	43.81	4250.59	371.52	-1.42	15.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.25	27.77	4278.37	236.88	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.20	292.80	4571.16	2527.89	17.34	14.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.18	48.71	4619.88	422.62	35.68	14.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.12	42.20	4662.07	371.63	-1.42	14.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	26.81	4688.89	237.08	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	392.18	5081.07	3555.23	20.63	19.99	0.0	0.0	20.70	19.99	0.001	0.007	9.5900e-05
4.00	65.55	5146.62	594.53	5.98	13.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.99	46.04	5192.66	418.45	35.68	13.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	195.99	5388.66	1794.94	17.85	20.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	40.56	5429.21	371.52	-1.42	13.59	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	65.28	5494.49	598.29	29.78	20.76	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	194.22	5688.71	1780.38	20.85	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	25.64	5714.35	235.31	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.93	2.66	5717.01	24.54	35.68	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	192.01	5909.03	1780.10	20.83	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	280.53	6189.56	2601.56	20.76	21.58	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.87	192.27	6381.83	1802.89	21.03	22.29	0.0	-0.18	0.0	0.0	0.0	0.0	0.0
3.86	274.55	6656.38	2578.63	20.83	22.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	187.30	6843.68	1776.62	20.83	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	129.92	6973.59	1235.06	20.83	23.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	129.81	7103.41	1235.00	20.83	23.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	1709.78	8813.18	1.632e+04	20.37	13.23	0.0	-0.34	18.24	14.65	2.553	0.112	0.090
3.79	47.12	8860.30	451.26	35.68	12.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	43.60	8903.90	417.65	29.78	12.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.78	234.93	9138.82	2254.54	18.04	21.49	0.0	-0.57	0.0	0.0	0.0	0.0	0.0
3.77	245.41	9384.23	2361.97	20.83	24.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	69.49	9453.72	670.47	18.36	12.15	0.0	-7.00e-06	0.0	0.0	0.0	0.0	0.0
3.76	52.05	9505.78	502.33	11.88	12.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	43.34	9549.12	418.48	14.98	12.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	52.56	9601.68	508.03	20.83	12.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	49.32	9651.00	476.83	24.68	12.03	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.74	135.24	9786.25	1312.35	32.93	11.78	0.0	-3.74e-04	0.0	0.0	0.0	0.0	0.0
3.73	182.60	9968.84	1773.13	20.83	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	295.94	1.026e+04	2881.86	18.07	22.12	0.0	-0.67	0.0	0.0	0.0	0.0	0.0
3.72	68.92	1.033e+04	672.44	18.43	11.42	0.0	-1.45e-05	0.0	0.0	0.0	0.0	0.0
3.72	51.39	1.039e+04	501.54	11.88	11.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	42.74	1.043e+04	417.62	14.98	11.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	51.78	1.048e+04	507.01	20.83	11.19	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	48.57	1.053e+04	475.78	24.68	11.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	59.19	1.059e+04	581.28	29.78	11.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	180.25	1.077e+04	1771.39	20.83	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	65.75	1.083e+04	646.49	35.68	10.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	51.82	1.089e+04	510.10	7.72	10.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	134.28	1.102e+04	1322.28	23.78	25.62	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	130.41	1.115e+04	1285.10	17.88	25.67	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	61.86	1.121e+04	610.40	16.04	10.69	0.0	-2.15e-05	0.0	0.0	0.0	0.0	0.0
3.67	50.72	1.126e+04	500.76	11.88	10.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	42.14	1.130e+04	416.75	14.98	10.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	51.00	1.136e+04	505.99	20.83	10.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	46.43	1.140e+04	460.91	24.68	10.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	17.49	1.142e+04	173.75	41.88	10.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	58.40	1.148e+04	580.42	29.78	10.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	59.49	1.154e+04	591.58	35.68	10.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	177.91	1.172e+04	1769.64	20.83	26.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.64	51.18	1.177e+04	509.39	7.72	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	37.53	1.180e+04	374.61	-0.22	9.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	50.05	1.185e+04	499.97	11.88	9.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	137.63	1.199e+04	1376.25	20.91	24.50	0.0	-0.84	0.0	0.0	0.0	0.0	0.0
3.62	123.86	1.212e+04	1239.56	23.78	26.67	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.62	41.54	1.216e+04	415.89	14.98	9.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	87.41	1.224e+04	878.87	22.67	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	58.74	1.230e+04	590.83	35.68	9.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	57.60	1.236e+04	579.57	29.78	9.45	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	50.54	1.241e+04	508.67	7.72	9.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	198.47	1.261e+04	1998.36	23.26	25.03	0.0	-0.88	0.0	0.0	0.0	0.0	0.0
3.59	37.10	1.265e+04	374.61	-0.22	9.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	193.15	1.284e+04	1951.87	20.77	27.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	56.27	1.290e+04	568.73	11.88	9.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.58	40.95	1.294e+04	415.03	14.98	9.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	27.46	1.296e+04	279.28	20.83	8.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	66.99	1.303e+04	681.57	35.68	8.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	24.74	1.306e+04	251.80	24.68	8.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	49.90	1.311e+04	507.95	7.72	8.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	28.20	1.313e+04	287.16	41.88	8.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	56.81	1.319e+04	578.71	29.78	8.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	173.25	1.336e+04	1766.16	20.83	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	194.50	1.356e+04	1986.39	20.83	27.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	35.88	1.360e+04	366.54	-0.22	8.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	90.49	1.369e+04	928.63	13.26	8.22	0.0	-1.27e-04	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.52	27.14	1.371e+04	279.28	20.83	8.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	23.63	1.374e+04	243.27	24.68	8.02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	49.26	1.379e+04	507.23	7.72	8.01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	27.88	1.381e+04	287.16	41.88	8.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	66.00	1.388e+04	680.79	29.78	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	337.80	1.422e+04	3487.06	20.78	28.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	85.03	1.430e+04	878.63	21.03	7.80	0.0	-2.50e-04	0.0	0.0	0.0	0.0	0.0
3.50	37.76	1.434e+04	391.15	11.88	7.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	162.51	1.450e+04	1688.29	27.38	22.45	0.0	-1.08	0.0	0.0	0.0	0.0	0.0
3.49	39.77	1.454e+04	413.30	14.98	7.44	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	36.58	1.458e+04	380.36	11.88	29.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	75.88	1.465e+04	789.86	20.83	29.16	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	26.82	1.468e+04	279.28	20.83	7.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	23.36	1.470e+04	243.27	24.68	7.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	76.19	1.478e+04	793.68	20.08	7.30	0.0	-3.69e-04	0.0	0.0	0.0	0.0	0.0
3.48	52.06	1.483e+04	543.17	20.83	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	31.98	1.487e+04	334.25	-0.22	7.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	37.35	1.490e+04	390.66	11.88	7.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.46	54.52	1.496e+04	572.17	29.78	6.86	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	75.09	1.503e+04	788.32	20.83	29.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	184.03	1.522e+04	1933.00	20.91	29.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	39.18	1.526e+04	412.43	14.98	6.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	26.21	1.528e+04	276.19	20.83	6.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	97.74	1.538e+04	1030.18	21.10	6.59	0.0	-4.00e-04	0.0	0.0	0.0	0.0	0.0
3.44	50.95	1.543e+04	537.48	20.83	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	60.94	1.549e+04	642.94	35.68	6.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	29.12	1.552e+04	307.45	-0.22	6.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	36.94	1.556e+04	390.17	11.88	6.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	34.16	1.559e+04	361.35	29.78	6.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	67.66	1.566e+04	716.49	20.83	30.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.41	126.02	1.579e+04	1338.37	20.83	30.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	496.71	1.628e+04	5297.49	20.62	16.75	0.0	-1.24	20.15	24.06	0.602	5.3732e-04	0.669
3.05	1348.20	1.763e+04	1.603e+04	23.08	16.50	0.0	-1.31	20.94	11.29	0.400	0.139	0.547
2.55	1.23	1.763e+04	17.46	40.58	16.51	0.0	-0.09	0.0	0.0	0.0	0.0	0.0
2.49	2.01	1.763e+04	29.22	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	1.56	1.763e+04	23.12	40.58	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	1.96	1.764e+04	29.23	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.37	1.91	1.764e+04	29.22	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.31	1.86	1.764e+04	29.23	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.27	2.91	1.764e+04	46.53	41.63	30.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	1.82	1.765e+04	29.18	41.88	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	1.82	1.765e+04	29.18	41.88	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.25	142.69	1.779e+04	2299.58	13.54	25.06	0.0	-1.11	1.11	30.28	0.156	1.958	0.941
2.24	4.26	1.779e+04	68.81	20.83	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	2.13	1.780e+04	34.40	41.88	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	2.22	1.780e+04	35.97	-0.60	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	4.24	1.780e+04	68.81	20.83	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	2.12	1.780e+04	34.40	41.88	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	4.23	1.781e+04	68.81	20.83	26.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	4.32	1.781e+04	70.38	20.59	22.09	0.0	-0.41	0.0	0.0	0.0	0.0	0.0
2.23	2.11	1.782e+04	34.40	-0.22	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	4.22	1.782e+04	68.81	20.83	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	2.11	1.782e+04	34.40	41.88	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	5.79	1.783e+04	94.72	11.49	24.21	0.0	-0.49	0.0	0.0	0.0	0.0	0.0
2.22	6.00	1.783e+04	98.18	25.27	25.68	0.0	-0.16	0.0	0.0	0.0	0.0	0.0
2.21	2.10	1.784e+04	34.40	41.88	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	4.19	1.784e+04	68.81	20.83	23.92	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	4.28	1.784e+04	70.38	21.43	20.94	0.0	-0.29	0.0	0.0	0.0	0.0	0.0
2.20	4.18	1.785e+04	68.81	20.83	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	2.09	1.785e+04	34.40	-0.22	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	2.09	1.785e+04	34.40	41.88	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	4.17	1.786e+04	68.81	20.83	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	2.18	1.786e+04	35.97	2.69	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	2.08	1.786e+04	34.40	41.88	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	4.15	1.787e+04	68.81	20.83	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	7.77	1.787e+04	129.12	20.27	23.20	0.0	-0.46	0.0	0.0	0.0	0.0	0.0
2.18	5.84	1.788e+04	97.09	25.15	22.67	0.0	-0.33	0.0	0.0	0.0	0.0	0.0
2.18	2.06	1.788e+04	34.40	41.88	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	26.71	1.791e+04	445.37	19.22	20.05	0.0	-0.04	20.83	19.97	0.076	0.713	0.043
2.17	2.15	1.791e+04	35.97	4.33	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.17	1.88	1.791e+04	31.42	41.88	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	2.14	1.791e+04	35.97	5.16	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
2.16	3.00	1.792e+04	50.37	14.98	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	443.10	1.836e+04	7473.13	22.84	13.76	0.0	-1.04	22.55	11.04	0.170	0.025	0.494
2.05	17.20	1.838e+04	304.23	3.74	5.99	0.0	-0.06	-0.18	5.90	0.052	6.800	0.099
1.30	385.57	1.876e+04	1.075e+04	20.77	17.75	0.0	-1.24	31.02	16.81	0.675	0.866	0.039
0.45	90.89	1.885e+04	7324.35	20.64	16.64	0.0	-1.24	20.46	11.88	0.520	0.011	0.459
0.33	8.04	1.886e+04	897.58	20.91	23.25	0.0	-0.43	20.83	20.06	0.336	0.029	0.799
Risulta	1.886e+04		1.962e+05									

CDC	Tipo	Sigla Id	Note
15	Esk	CDC=Es (statico SLD) alfa=0.0 (ecc. -)	
			categoria suolo: da R.S.L.
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 1.229 sec.
			ordinata spettro Se(T1): 0.096

Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	daN	daN	m	m	m	m	m	m			
5.40	1882.32	1882.32	1.264e+04	20.66	19.99	0.0	0.0	20.63	19.99	0.008	0.003	1.8398e-04
5.34	62.05	1944.38	421.07	15.49	19.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.26	109.28	2053.65	753.74	18.67	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.19	88.14	2141.79	616.26	15.45	19.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.11	105.68	2247.47	749.22	18.66	18.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.03	57.60	2305.07	415.41	15.42	18.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.00	266.65	2571.72	1933.82	20.83	18.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.97	114.00	2685.73	831.45	16.26	18.09	0.0	0.0	15.79	18.09	4.9874e-04	0.027	0.0
4.94	23.50	2709.23	172.42	40.58	17.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.93	34.13	2743.36	251.00	35.68	17.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.91	79.03	2822.39	583.78	2.75	17.81	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	108.63	2931.02	829.09	2.76	17.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	34.12	2965.14	260.60	40.58	17.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	47.70	3012.84	364.48	35.68	17.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.60	442.82	3455.65	3490.68	21.78	17.28	0.0	0.18	24.62	18.67	0.356	0.161	0.191
4.59	115.95	3571.60	915.37	2.96	16.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.56	32.80	3604.40	260.83	35.68	16.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	19.69	3624.09	156.82	40.58	16.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.43	430.54	4054.63	3520.46	18.60	17.65	0.0	1.24	25.46	18.10	1.381	0.236	0.026
4.40	28.84	4083.47	237.56	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.39	71.91	4155.38	593.31	5.98	15.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	51.41	4206.78	426.62	35.68	15.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.28	43.81	4250.59	371.52	-1.42	15.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.25	27.77	4278.37	236.88	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.20	292.80	4571.16	2527.89	17.34	14.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.18	48.71	4619.88	422.62	35.68	14.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.12	42.20	4662.07	371.63	-1.42	14.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	26.81	4688.89	237.08	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	392.18	5081.07	3555.23	20.63	19.99	0.0	0.0	20.70	19.99	0.001	0.007	9.5900e-05
4.00	65.55	5146.62	594.53	5.98	13.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.99	46.04	5192.66	418.45	35.68	13.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	195.99	5388.66	1794.94	17.85	20.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	40.56	5429.21	371.52	-1.42	13.59	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	65.28	5494.49	598.29	29.78	20.76	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	194.22	5688.71	1780.38	20.85	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.95	25.64	5714.35	235.31	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.93	2.66	5717.01	24.54	35.68	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	192.01	5909.03	1780.10	20.83	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	280.53	6189.56	2601.56	20.76	21.58	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.87	192.27	6381.83	1802.89	21.03	22.29	0.0	0.18	0.0	0.0	0.0	0.0	0.0
3.86	274.55	6656.38	2578.63	20.83	22.46	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.82	187.30	6843.68	1776.62	20.83	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	129.92	6973.59	1235.06	20.83	23.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.81	129.81	7103.41	1235.00	20.83	23.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.80	1709.78	8813.18	1.632e+04	20.37	13.23	0.0	0.34	18.24	14.65	2.553	0.112	0.090
3.79	47.12	8860.30	451.26	35.68	12.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.79	43.60	8903.90	417.65	29.78	12.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.78	234.93	9138.82	2254.54	18.04	21.49	0.0	0.57	0.0	0.0	0.0	0.0	0.0
3.77	245.41	9384.23	2361.97	20.83	24.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	69.49	9453.72	670.47	18.36	12.15	0.0	7.00e-06	0.0	0.0	0.0	0.0	0.0
3.76	52.05	9505.78	502.33	11.88	12.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	43.34	9549.12	418.48	14.98	12.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	52.56	9601.68	508.03	20.83	12.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	49.32	9651.00	476.83	24.68	12.03	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.74	135.24	9786.25	1312.35	32.93	11.78	0.0	3.74e-04	0.0	0.0	0.0	0.0	0.0
3.73	182.60	9968.84	1773.13	20.83	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.72	295.94	1.026e+04	2881.86	18.07	22.12	0.0	0.67	0.0	0.0	0.0	0.0	0.0
3.72	68.92	1.033e+04	672.44	18.43	11.42	0.0	1.45e-05	0.0	0.0	0.0	0.0	0.0
3.72	51.39	1.039e+04	501.54	11.88	11.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	42.74	1.043e+04	417.62	14.98	11.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	51.78	1.048e+04	507.01	20.83	11.19	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	48.57	1.053e+04	475.78	24.68	11.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	59.19	1.059e+04	581.28	29.78	11.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	180.25	1.077e+04	1771.39	20.83	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	65.75	1.083e+04	646.49	35.68	10.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	51.82	1.089e+04	510.10	7.72	10.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	134.28	1.102e+04	1322.28	23.78	25.62	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	130.41	1.115e+04	1285.10	17.88	25.67	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	61.86	1.121e+04	610.40	16.04	10.69	0.0	2.15e-05	0.0	0.0	0.0	0.0	0.0
3.67	50.72	1.126e+04	500.76	11.88	10.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	42.14	1.130e+04	416.75	14.98	10.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	51.00	1.136e+04	505.99	20.83	10.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	46.43	1.140e+04	460.91	24.68	10.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	17.49	1.142e+04	173.75	41.88	10.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	58.40	1.148e+04	580.42	29.78	10.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	59.49	1.154e+04	591.58	35.68	10.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	177.91	1.172e+04	1769.64	20.83	26.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.64	51.18	1.177e+04	509.39	7.72	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	37.53	1.180e+04	374.61	-0.22	9.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	50.05	1.185e+04	499.97	11.88	9.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	137.63	1.199e+04	1376.25	20.91	24.50	0.0	0.84	0.0	0.0	0.0	0.0	0.0
3.62	123.86	1.212e+04	1239.56	23.78	26.67	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.62	41.54	1.216e+04	415.89	14.98	9.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	87.41	1.224e+04	878.87	22.67	9.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	58.74	1.230e+04	590.83	35.68	9.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	57.60	1.236e+04	579.57	29.78	9.45	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	50.54	1.241e+04	508.67	7.72	9.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	198.47	1.261e+04	1998.36	23.26	25.03	0.0	0.88	0.0	0.0	0.0	0.0	0.0
3.59	37.10	1.265e+04	374.61	-0.22	9.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	193.15	1.284e+04	1951.87	20.77	27.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	56.27	1.290e+04	568.73	11.88	9.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.58	40.95	1.294e+04	415.03	14.98	9.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	27.46	1.296e+04	279.28	20.83	8.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	66.99	1.303e+04	681.57	35.68	8.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	24.74	1.306e+04	251.80	24.68	8.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	49.90	1.311e+04	507.95	7.72	8.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	28.20	1.313e+04	287.16	41.88	8.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	56.81	1.319e+04	578.71	29.78	8.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	173.25	1.336e+04	1766.16	20.83	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	194.50	1.356e+04	1986.39	20.83	27.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.55	35.88	1.360e+04	366.54	-0.22	8.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	90.49	1.369e+04	928.63	13.26	8.22	0.0	1.27e-04	0.0	0.0	0.0	0.0	0.0
3.52	27.14	1.371e+04	279.28	20.83	8.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	23.63	1.374e+04	243.27	24.68	8.02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	49.26	1.379e+04	507.23	7.72	8.01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	27.88	1.381e+04	287.16	41.88	8.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	66.00	1.388e+04	680.79	29.78	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	337.80	1.422e+04	3487.06	20.78	28.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	85.03	1.430e+04	878.63	21.03	7.80	0.0	2.50e-04	0.0	0.0	0.0	0.0	0.0
3.50	37.76	1.434e+04	391.15	11.88	7.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	162.51	1.450e+04	1688.29	27.38	22.45	0.0	1.08	0.0	0.0	0.0	0.0	0.0
3.49	39.77	1.454e+04	413.30	14.98	7.44	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	36.58	1.458e+04	380.36	11.88	29.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	75.88	1.465e+04	789.86	20.83	29.16	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	26.82	1.468e+04	279.28	20.83	7.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	23.36	1.470e+04	243.27	24.68	7.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	76.19	1.478e+04	793.68	20.08	7.30	0.0	3.69e-04	0.0	0.0	0.0	0.0	0.0
3.48	52.06	1.483e+04	543.17	20.83	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.47	31.98	1.487e+04	334.25	-0.22	7.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	37.35	1.490e+04	390.66	11.88	7.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.46	54.52	1.496e+04	572.17	29.78	6.86	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	75.09	1.503e+04	788.32	20.83	29.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	184.03	1.522e+04	1933.00	20.91	29.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	39.18	1.526e+04	412.43	14.98	6.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	26.21	1.528e+04	276.19	20.83	6.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	97.74	1.538e+04	1030.18	21.10	6.59	0.0	4.00e-04	0.0	0.0	0.0	0.0	0.0
3.44	50.95	1.543e+04	537.48	20.83	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	60.94	1.549e+04	642.94	35.68	6.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	29.12	1.552e+04	307.45	-0.22	6.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	36.94	1.556e+04	390.17	11.88	6.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	34.16	1.559e+04	361.35	29.78	6.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	67.66	1.566e+04	716.49	20.83	30.21	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.41	126.02	1.579e+04	1338.37	20.83	30.38	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.40	496.71	1.628e+04	5297.49	20.62	16.75	0.0	1.24	20.15	24.06	0.602	5.3732e-04	0.669
3.05	1348.20	1.763e+04	1.603e+04	23.08	16.50	0.0	1.31	20.94	11.29	0.400	0.139	0.547
2.55	1.23	1.763e+04	17.46	40.58	16.51	0.0	0.09	0.0	0.0	0.0	0.0	0.0
2.49	2.01	1.763e+04	29.22	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	1.56	1.763e+04	23.12	40.58	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	1.96	1.764e+04	29.23	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.37	1.91	1.764e+04	29.22	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.31	1.86	1.764e+04	29.23	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.27	2.91	1.764e+04	46.53	41.63	30.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	1.82	1.765e+04	29.18	41.88	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	1.82	1.765e+04	29.18	41.88	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.25	142.69	1.779e+04	2299.58	13.54	25.06	0.0	1.11	1.11	30.28	0.156	1.958	0.941
2.24	4.26	1.779e+04	68.81	20.83	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	2.13	1.780e+04	34.40	41.88	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	2.22	1.780e+04	35.97	-0.60	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	4.24	1.780e+04	68.81	20.83	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	2.12	1.780e+04	34.40	41.88	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	4.23	1.781e+04	68.81	20.83	26.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	4.32	1.781e+04	70.38	20.59	22.09	0.0	0.41	0.0	0.0	0.0	0.0	0.0
2.23	2.11	1.782e+04	34.40	-0.22	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	4.22	1.782e+04	68.81	20.83	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	2.11	1.782e+04	34.40	41.88	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	5.79	1.783e+04	94.72	11.49	24.21	0.0	0.49	0.0	0.0	0.0	0.0	0.0
2.22	6.00	1.783e+04	98.18	25.27	25.68	0.0	0.16	0.0	0.0	0.0	0.0	0.0
2.21	2.10	1.784e+04	34.40	41.88	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	4.19	1.784e+04	68.81	20.83	23.92	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	4.28	1.784e+04	70.38	21.43	20.94	0.0	0.29	0.0	0.0	0.0	0.0	0.0
2.20	4.18	1.785e+04	68.81	20.83	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	2.09	1.785e+04	34.40	-0.22	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	2.09	1.785e+04	34.40	41.88	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	4.17	1.786e+04	68.81	20.83	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	2.18	1.786e+04	35.97	2.69	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	2.08	1.786e+04	34.40	41.88	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	4.15	1.787e+04	68.81	20.83	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	7.77	1.787e+04	129.12	20.27	23.20	0.0	0.46	0.0	0.0	0.0	0.0	0.0
2.18	5.84	1.788e+04	97.09	25.15	22.67	0.0	0.33	0.0	0.0	0.0	0.0	0.0
2.18	2.06	1.788e+04	34.40	41.88	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	26.71	1.791e+04	445.37	19.22	20.05	0.0	0.04	20.83	19.97	0.076	0.713	0.043
2.17	2.15	1.791e+04	35.97	4.33	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.17	1.88	1.791e+04	31.42	41.88	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	2.14	1.791e+04	35.97	5.16	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	3.00	1.792e+04	50.37	14.98	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	443.10	1.836e+04	7473.13	22.84	13.76	0.0	1.04	22.55	11.04	0.170	0.025	0.494
2.05	17.20	1.838e+04	304.23	3.74	5.99	0.0	0.06	-0.18	5.90	0.052	6.800	0.099
1.30	385.57	1.876e+04	1.075e+04	20.77	17.75	0.0	1.24	31.02	16.81	0.675	0.866	0.039
0.45	90.89	1.885e+04	7324.35	20.64	16.64	0.0	1.24	20.46	11.88	0.520	0.011	0.459
0.33	8.04	1.886e+04	897.58	20.91	23.25	0.0	0.43	20.83	20.06	0.336	0.029	0.799
Risulta	1.886e+04		1.962e+05									

CDC	Tipo	Sigla Id	Note
16	Esk	CDC=Es (statico SLD) alfa=90.00 (ecc. +)	
			categoria suolo: da R.S.L. angolo di ingresso:90.00

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



CDC	Tipo	Sigla Id	Note
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.422 sec.
			ordinata spettro Se(T1): 0.265

Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	daN	daN	m	m	m	m	m	m			
5.40	5187.06	5187.06	1.264e+04	20.66	19.99	2.10	0.0	20.63	19.99	0.008	0.003	1.8398e-04
5.34	171.00	5358.05	421.07	15.49	19.74	2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.26	301.14	5659.19	753.74	18.67	19.35	1.49	0.0	0.0	0.0	0.0	0.0	0.0
5.19	242.88	5902.07	616.26	15.45	19.04	2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.11	291.21	6193.28	749.22	18.66	18.72	1.49	0.0	0.0	0.0	0.0	0.0	0.0
5.03	158.74	6352.02	415.41	15.42	18.34	2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.00	734.80	7086.82	1933.82	20.83	18.21	1.19	0.0	0.0	0.0	0.0	0.0	0.0
4.97	314.15	7400.97	831.45	16.26	18.09	2.10	0.0	15.79	18.09	4.9874e-04	0.027	0.0
4.94	64.76	7465.73	172.42	40.58	17.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.93	94.06	7559.80	251.00	35.68	17.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.91	217.77	7777.57	583.78	2.75	17.81	0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.75	299.34	8076.91	829.09	2.76	17.11	0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.75	94.02	8170.94	260.60	40.58	17.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	131.44	8302.38	364.48	35.68	17.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.60	1220.26	9522.64	3490.68	21.78	17.28	2.10	0.0	24.62	18.67	0.356	0.161	0.191
4.59	319.52	9842.16	915.37	2.96	16.41	0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.56	90.38	9932.53	260.83	35.68	16.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	54.26	9986.79	156.82	40.58	16.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.43	1186.42	1.117e+04	3520.46	18.60	17.65	2.17	0.0	25.46	18.10	1.381	0.236	0.026
4.40	79.47	1.125e+04	237.56	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.39	198.16	1.145e+04	593.31	5.98	15.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	141.67	1.159e+04	426.62	35.68	15.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.28	120.72	1.171e+04	371.52	-1.42	15.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.25	76.54	1.179e+04	236.88	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.20	806.85	1.260e+04	2527.89	17.34	14.66	1.34	0.0	0.0	0.0	0.0	0.0	0.0
4.18	134.24	1.273e+04	422.62	35.68	14.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.12	116.28	1.285e+04	371.63	-1.42	14.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	73.89	1.292e+04	237.08	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	1080.72	1.400e+04	3555.23	20.63	19.99	2.17	0.0	20.70	19.99	0.001	0.007	9.5900e-05
4.00	180.65	1.418e+04	594.53	5.98	13.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.99	126.88	1.431e+04	418.45	35.68	13.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	540.09	1.485e+04	1794.94	17.85	20.71	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.96	111.77	1.496e+04	371.52	-1.42	13.59	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	179.89	1.514e+04	598.29	29.78	20.76	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	535.21	1.568e+04	1780.38	20.85	20.77	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.95	70.65	1.575e+04	235.31	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.93	7.34	1.575e+04	24.54	35.68	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	529.13	1.628e+04	1780.10	20.83	21.56	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.91	773.05	1.706e+04	2601.56	20.76	21.58	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.87	529.83	1.759e+04	1802.89	21.03	22.29	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.86	756.57	1.834e+04	2578.63	20.83	22.46	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.82	516.13	1.886e+04	1776.62	20.83	23.13	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.81	358.01	1.922e+04	1235.06	20.83	23.28	0.90	0.0	0.0	0.0	0.0	0.0	0.0
3.81	357.72	1.957e+04	1235.00	20.83	23.33	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.80	4711.58	2.429e+04	1.632e+04	20.37	13.23	2.17	0.0	18.24	14.65	2.553	0.112	0.090
3.79	129.84	2.442e+04	451.26	35.68	12.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	120.14	2.454e+04	417.65	29.78	12.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.78	647.38	2.518e+04	2254.54	18.04	21.49	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.77	676.27	2.586e+04	2361.97	20.83	24.11	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.76	191.49	2.605e+04	670.47	18.36	12.15	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.76	143.44	2.619e+04	502.33	11.88	12.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	119.44	2.631e+04	418.48	14.98	12.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	144.84	2.646e+04	508.03	20.83	12.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	135.92	2.659e+04	476.83	24.68	12.03	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.74	372.68	2.697e+04	1312.35	32.93	11.78	0.29	0.0	0.0	0.0	0.0	0.0	0.0
3.73	503.18	2.747e+04	1773.13	20.83	24.70	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.72	815.52	2.829e+04	2881.86	18.07	22.12	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.72	189.91	2.848e+04	672.44	18.43	11.42	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.72	141.60	2.862e+04	501.54	11.88	11.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	117.78	2.874e+04	417.62	14.98	11.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	142.69	2.888e+04	507.01	20.83	11.19	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	133.85	2.901e+04	475.78	24.68	11.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.69	163.11	2.918e+04	581.28	29.78	11.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	496.72	2.967e+04	1771.39	20.83	25.49	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.69	181.19	2.985e+04	646.49	35.68	10.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	142.79	3.000e+04	510.10	7.72	10.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	370.04	3.037e+04	1322.28	23.78	25.62	1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.68	359.36	3.073e+04	1285.10	17.88	25.67	1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.67	170.45	3.090e+04	610.40	16.04	10.69	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.67	139.76	3.104e+04	500.76	11.88	10.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	116.13	3.115e+04	416.75	14.98	10.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	140.54	3.129e+04	505.99	20.83	10.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	127.95	3.142e+04	460.91	24.68	10.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	48.20	3.147e+04	173.75	41.88	10.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	160.92	3.163e+04	580.42	29.78	10.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	163.94	3.179e+04	591.58	35.68	10.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	490.27	3.228e+04	1769.64	20.83	26.28	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.64	141.02	3.242e+04	509.39	7.72	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	103.42	3.253e+04	374.61	-0.22	9.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	137.93	3.267e+04	499.97	11.88	9.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	379.25	3.305e+04	1376.25	20.91	24.50	1.79	0.0	0.0	0.0	0.0	0.0	0.0
3.62	341.32	3.339e+04	1239.56	23.78	26.67	1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.62	114.48	3.350e+04	415.89	14.98	9.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	240.88	3.374e+04	878.87	22.67	9.50	0.19	0.0	0.0	0.0	0.0	0.0	0.0
3.61	161.87	3.390e+04	590.83	35.68	9.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	158.73	3.406e+04	579.57	29.78	9.45	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	139.26	3.420e+04	508.67	7.72	9.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	546.92	3.475e+04	1998.36	23.26	25.03	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.59	102.23	3.485e+04	374.61	-0.22	9.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	532.27	3.538e+04	1951.87	20.77	27.29	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.59	155.06	3.554e+04	568.73	11.88	9.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.58	112.84	3.565e+04	415.03	14.98	9.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	75.67	3.573e+04	279.28	20.83	8.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	184.59	3.591e+04	681.57	35.68	8.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	68.18	3.598e+04	251.80	24.68	8.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	137.50	3.612e+04	507.95	7.72	8.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	77.72	3.619e+04	287.16	41.88	8.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	156.55	3.635e+04	578.71	29.78	8.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	477.42	3.683e+04	1766.16	20.83	27.85	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.55	535.97	3.736e+04	1986.39	20.83	27.96	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.55	98.86	3.746e+04	366.54	-0.22	8.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	249.36	3.771e+04	928.63	13.26	8.22	0.15	0.0	0.0	0.0	0.0	0.0	0.0
3.52	74.79	3.779e+04	279.28	20.83	8.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	65.12	3.785e+04	243.27	24.68	8.02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	135.74	3.799e+04	507.23	7.72	8.01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	76.84	3.807e+04	287.16	41.88	8.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	181.88	3.825e+04	680.79	29.78	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	930.87	3.918e+04	3487.06	20.78	28.64	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.51	234.33	3.941e+04	878.63	21.03	7.80	1.79	0.0	0.0	0.0	0.0	0.0	0.0
3.50	104.04	3.952e+04	391.15	11.88	7.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	447.82	3.996e+04	1688.29	27.38	22.45	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.49	109.58	4.007e+04	413.30	14.98	7.44	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	100.81	4.017e+04	380.36	11.88	29.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	209.09	4.038e+04	789.86	20.83	29.16	0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.48	73.92	4.046e+04	279.28	20.83	7.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	64.36	4.052e+04	243.27	24.68	7.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	209.95	4.073e+04	793.68	20.08	7.30	1.71	0.0	0.0	0.0	0.0	0.0	0.0
3.48	143.45	4.088e+04	543.17	20.83	29.30	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.47	88.12	4.096e+04	334.25	-0.22	7.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	102.92	4.107e+04	390.66	11.88	7.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.46	150.25	4.122e+04	572.17	29.78	6.86	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	206.91	4.142e+04	788.32	20.83	29.68	0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.45	507.13	4.193e+04	1933.00	20.91	29.71	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.44	107.96	4.204e+04	412.43	14.98	6.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	72.23	4.211e+04	276.19	20.83	6.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	269.35	4.238e+04	1030.18	21.10	6.59	1.71	0.0	0.0	0.0	0.0	0.0	0.0
3.44	140.41	4.252e+04	537.48	20.83	29.97	2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.44	167.93	4.269e+04	642.94	35.68	6.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	80.25	4.277e+04	307.45	-0.22	6.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	101.80	4.287e+04	390.17	11.88	6.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	94.13	4.296e+04	361.35	29.78	6.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	186.45	4.315e+04	716.49	20.83	30.21	0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.41	347.26	4.350e+04	1338.37	20.83	30.38	1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.40	1368.78	4.487e+04	5297.49	20.62	16.75	2.10	0.0	20.15	24.06	0.602	5.3732e-04	0.669

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.05	3715.19	4.858e+04	1.603e+04	23.08	16.50	2.25	0.0	20.94	11.29	0.400	0.139	0.547
2.55	3.38	4.859e+04	17.46	40.58	16.51	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.49	5.53	4.859e+04	29.22	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	4.30	4.860e+04	23.12	40.58	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	5.40	4.860e+04	29.23	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.37	5.26	4.861e+04	29.22	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.31	5.13	4.861e+04	29.23	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.27	8.02	4.862e+04	46.53	41.63	30.64	0.04	0.0	0.0	0.0	0.0	0.0	0.0
2.26	5.02	4.862e+04	29.18	41.88	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	5.00	4.863e+04	29.18	41.88	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.25	393.20	4.902e+04	2299.58	13.54	25.06	2.16	0.0	1.11	30.28	0.156	1.958	0.941
2.24	11.73	4.903e+04	68.81	20.83	27.85	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.86	4.904e+04	34.40	41.88	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	6.12	4.905e+04	35.97	-0.60	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	11.69	4.906e+04	68.81	20.83	27.06	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.84	4.906e+04	34.40	41.88	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.23	11.66	4.908e+04	68.81	20.83	26.28	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.23	11.91	4.909e+04	70.38	20.59	22.09	2.08	0.0	0.0	0.0	0.0	0.0	0.0
2.23	5.82	4.909e+04	34.40	-0.22	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	11.62	4.911e+04	68.81	20.83	25.49	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.22	5.81	4.911e+04	34.40	41.88	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	15.96	4.913e+04	94.72	11.49	24.21	1.44	0.0	0.0	0.0	0.0	0.0	0.0
2.22	16.53	4.914e+04	98.18	25.27	25.68	0.88	0.0	0.0	0.0	0.0	0.0	0.0
2.21	5.79	4.915e+04	34.40	41.88	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	11.55	4.916e+04	68.81	20.83	23.92	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.21	11.80	4.917e+04	70.38	21.43	20.94	2.00	0.0	0.0	0.0	0.0	0.0	0.0
2.20	11.52	4.918e+04	68.81	20.83	23.13	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.20	5.75	4.919e+04	34.40	-0.22	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	5.75	4.920e+04	34.40	41.88	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	11.48	4.921e+04	68.81	20.83	22.34	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.19	6.00	4.921e+04	35.97	2.69	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	5.73	4.922e+04	34.40	41.88	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	11.44	4.923e+04	68.81	20.83	21.56	0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.18	21.42	4.925e+04	129.12	20.27	23.20	1.92	0.0	0.0	0.0	0.0	0.0	0.0
2.18	16.10	4.927e+04	97.09	25.15	22.67	0.88	0.0	0.0	0.0	0.0	0.0	0.0
2.18	5.69	4.927e+04	34.40	41.88	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	73.61	4.935e+04	445.37	19.22	20.05	1.32	0.0	20.83	19.97	0.076	0.713	0.043
2.17	5.94	4.935e+04	35.97	4.33	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.17	5.18	4.936e+04	31.42	41.88	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	5.91	4.936e+04	35.97	5.16	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	8.26	4.937e+04	50.37	14.98	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	1221.03	5.059e+04	7473.13	22.84	13.76	2.17	0.0	22.55	11.04	0.170	0.025	0.494
2.05	47.40	5.064e+04	304.23	3.74	5.99	0.44	0.0	-0.18	5.90	0.052	6.800	0.099
1.30	1062.51	5.170e+04	1.075e+04	20.77	17.75	2.17	0.0	31.02	16.81	0.675	0.866	0.039
0.45	250.48	5.195e+04	7324.35	20.64	16.64	2.17	0.0	20.46	11.88	0.520	0.011	0.459
0.33	22.17	5.198e+04	897.58	20.91	23.25	0.72	0.0	20.83	20.06	0.336	0.029	0.799
Risulta	5.198e+04		1.962e+05									

CDC	Tipo	Sigla Id	Note
17	Esk	CDC=Es (statico SLD) alfa=90.00 (ecc. -)	
			categoria suolo: da R.S.L.
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.422 sec.
			ordinata spettro Se(T1): 0.265

Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
m	daN	daN	daN	m	m	m	m	m	m			
5.40	5187.06	5187.06	1.264e+04	20.66	19.99	-2.10	0.0	20.63	19.99	0.008	0.003	1.8398e-04
5.34	171.00	5358.05	421.07	15.49	19.74	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.26	301.14	5659.19	753.74	18.67	19.35	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
5.19	242.88	5902.07	616.26	15.45	19.04	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
5.11	291.21	6193.28	749.22	18.66	18.72	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
5.03	158.74	6352.02	415.41	15.42	18.34	-2.10	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
5.00	734.80	7086.82	1933.82	20.83	18.21	-1.19	0.0	0.0	0.0	0.0	0.0	0.0
4.97	314.15	7400.97	831.45	16.26	18.09	-2.10	0.0	15.79	18.09	4.9874e-04	0.027	0.0
4.94	64.76	7465.73	172.42	40.58	17.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.93	94.06	7559.80	251.00	35.68	17.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.91	217.77	7777.57	583.78	2.75	17.81	-0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.75	299.34	8076.91	829.09	2.76	17.11	-0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.75	94.02	8170.94	260.60	40.58	17.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.75	131.44	8302.38	364.48	35.68	17.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.60	1220.26	9522.64	3490.68	21.78	17.28	-2.10	0.0	24.62	18.67	0.356	0.161	0.191
4.59	319.52	9842.16	915.37	2.96	16.41	-0.37	0.0	0.0	0.0	0.0	0.0	0.0
4.56	90.38	9932.53	260.83	35.68	16.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.55	54.26	9986.79	156.82	40.58	16.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.43	1186.42	1.117e+04	3520.46	18.60	17.65	-2.17	0.0	25.46	18.10	1.381	0.236	0.026
4.40	79.47	1.125e+04	237.56	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.39	198.16	1.145e+04	593.31	5.98	15.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.37	141.67	1.159e+04	426.62	35.68	15.41	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.28	120.72	1.171e+04	371.52	-1.42	15.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.25	76.54	1.179e+04	236.88	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.20	806.85	1.260e+04	2527.89	17.34	14.66	-1.34	0.0	0.0	0.0	0.0	0.0	0.0
4.18	134.24	1.273e+04	422.62	35.68	14.57	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.12	116.28	1.285e+04	371.63	-1.42	14.29	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.10	73.89	1.292e+04	237.08	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	1080.72	1.400e+04	3555.23	20.63	19.99	-2.17	0.0	20.70	19.99	0.001	0.007	9.5900e-05
4.00	180.65	1.418e+04	594.53	5.98	13.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.99	126.88	1.431e+04	418.45	35.68	13.73	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	540.09	1.485e+04	1794.94	17.85	20.71	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.96	111.77	1.496e+04	371.52	-1.42	13.59	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	179.89	1.514e+04	598.29	29.78	20.76	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.96	535.21	1.568e+04	1780.38	20.85	20.77	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.95	70.65	1.575e+04	235.31	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.93	7.34	1.575e+04	24.54	35.68	19.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.91	529.13	1.628e+04	1780.10	20.83	21.56	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.91	773.05	1.706e+04	2601.56	20.76	21.58	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.87	529.83	1.759e+04	1802.89	21.03	22.29	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.86	756.57	1.834e+04	2578.63	20.83	22.46	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.82	516.13	1.886e+04	1776.62	20.83	23.13	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.81	358.01	1.922e+04	1235.06	20.83	23.28	-0.90	0.0	0.0	0.0	0.0	0.0	0.0
3.81	357.72	1.957e+04	1235.00	20.83	23.33	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.80	4711.58	2.429e+04	1.632e+04	20.37	13.23	-2.17	0.0	18.24	14.65	2.553	0.112	0.090
3.79	129.84	2.442e+04	451.26	35.68	12.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.79	120.14	2.454e+04	417.65	29.78	12.63	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.78	647.38	2.518e+04	2254.54	18.04	21.49	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.77	676.27	2.586e+04	2361.97	20.83	24.11	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.76	191.49	2.605e+04	670.47	18.36	12.15	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.76	143.44	2.619e+04	502.33	11.88	12.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.76	119.44	2.631e+04	418.48	14.98	12.11	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	144.84	2.646e+04	508.03	20.83	12.04	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.75	135.92	2.659e+04	476.83	24.68	12.03	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.74	372.68	2.697e+04	1312.35	32.93	11.78	-0.29	0.0	0.0	0.0	0.0	0.0	0.0
3.73	503.18	2.747e+04	1773.13	20.83	24.70	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.72	815.52	2.829e+04	2881.86	18.07	22.12	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.72	189.91	2.848e+04	672.44	18.43	11.42	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.72	141.60	2.862e+04	501.54	11.88	11.40	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.71	117.78	2.874e+04	417.62	14.98	11.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	142.69	2.888e+04	507.01	20.83	11.19	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70	133.85	2.901e+04	475.78	24.68	11.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	163.11	2.918e+04	581.28	29.78	11.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.69	496.72	2.967e+04	1771.39	20.83	25.49	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.69	181.19	2.985e+04	646.49	35.68	10.93	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	142.79	3.000e+04	510.10	7.72	10.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.68	370.04	3.037e+04	1322.28	23.78	25.62	-1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.68	359.36	3.073e+04	1285.10	17.88	25.67	-1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.67	170.45	3.090e+04	610.40	16.04	10.69	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.67	139.76	3.104e+04	500.76	11.88	10.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.67	116.13	3.115e+04	416.75	14.98	10.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	140.54	3.129e+04	505.99	20.83	10.35	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	127.95	3.142e+04	460.91	24.68	10.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	48.20	3.147e+04	173.75	41.88	10.26	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	160.92	3.163e+04	580.42	29.78	10.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	163.94	3.179e+04	591.58	35.68	10.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.65	490.27	3.228e+04	1769.64	20.83	26.28	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.64	141.02	3.242e+04	509.39	7.72	10.14	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
3.63	103.42	3.253e+04	374.61	-0.22	9.96	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	137.93	3.267e+04	499.97	11.88	9.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.63	379.25	3.305e+04	1376.25	20.91	24.50	-1.79	0.0	0.0	0.0	0.0	0.0	0.0
3.62	341.32	3.339e+04	1239.56	23.78	26.67	-1.19	0.0	0.0	0.0	0.0	0.0	0.0
3.62	114.48	3.350e+04	415.89	14.98	9.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.61	240.88	3.374e+04	878.87	22.67	9.50	-0.19	0.0	0.0	0.0	0.0	0.0	0.0
3.61	161.87	3.390e+04	590.83	35.68	9.48	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	158.73	3.406e+04	579.57	29.78	9.45	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	139.26	3.420e+04	508.67	7.72	9.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.60	546.92	3.475e+04	1998.36	23.26	25.03	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.59	102.23	3.485e+04	374.61	-0.22	9.23	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.59	532.27	3.538e+04	1951.87	20.77	27.29	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.59	155.06	3.554e+04	568.73	11.88	9.17	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.58	112.84	3.565e+04	415.03	14.98	9.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.57	75.67	3.573e+04	279.28	20.83	8.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	184.59	3.591e+04	681.57	35.68	8.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	68.18	3.598e+04	251.80	24.68	8.74	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	137.50	3.612e+04	507.95	7.72	8.72	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	77.72	3.619e+04	287.16	41.88	8.71	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	156.55	3.635e+04	578.71	29.78	8.68	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.56	477.42	3.683e+04	1766.16	20.83	27.85	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.55	535.97	3.736e+04	1986.39	20.83	27.96	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.55	98.86	3.746e+04	366.54	-0.22	8.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.53	249.36	3.771e+04	928.63	13.26	8.22	-0.15	0.0	0.0	0.0	0.0	0.0	0.0
3.52	74.79	3.779e+04	279.28	20.83	8.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	65.12	3.785e+04	243.27	24.68	8.02	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	135.74	3.799e+04	507.23	7.72	8.01	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	76.84	3.807e+04	287.16	41.88	8.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.52	181.88	3.825e+04	680.79	29.78	7.91	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.51	930.87	3.918e+04	3487.06	20.78	28.64	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.51	234.33	3.941e+04	878.63	21.03	7.80	-1.79	0.0	0.0	0.0	0.0	0.0	0.0
3.50	104.04	3.952e+04	391.15	11.88	7.64	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	447.82	3.996e+04	1688.29	27.38	22.45	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.49	109.58	4.007e+04	413.30	14.98	7.44	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.49	100.81	4.017e+04	380.36	11.88	29.08	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	209.09	4.038e+04	789.86	20.83	29.16	-0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.48	73.92	4.046e+04	279.28	20.83	7.33	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	64.36	4.052e+04	243.27	24.68	7.31	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.48	209.95	4.073e+04	793.68	20.08	7.30	-1.71	0.0	0.0	0.0	0.0	0.0	0.0
3.48	143.45	4.088e+04	543.17	20.83	29.30	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.47	88.12	4.096e+04	334.25	-0.22	7.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.47	102.92	4.107e+04	390.66	11.88	7.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.46	150.25	4.122e+04	572.17	29.78	6.86	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.45	206.91	4.142e+04	788.32	20.83	29.68	-0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.45	507.13	4.193e+04	1933.00	20.91	29.71	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.44	107.96	4.204e+04	412.43	14.98	6.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	72.23	4.211e+04	276.19	20.83	6.61	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.44	269.35	4.238e+04	1030.18	21.10	6.59	-1.71	0.0	0.0	0.0	0.0	0.0	0.0
3.44	140.41	4.252e+04	537.48	20.83	29.97	-2.10	0.0	0.0	0.0	0.0	0.0	0.0
3.44	167.93	4.269e+04	642.94	35.68	6.53	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	80.25	4.277e+04	307.45	-0.22	6.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	101.80	4.287e+04	390.17	11.88	6.47	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.43	94.13	4.296e+04	361.35	29.78	6.37	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.42	186.45	4.315e+04	716.49	20.83	30.21	-0.32	0.0	0.0	0.0	0.0	0.0	0.0
3.41	347.26	4.350e+04	1338.37	20.83	30.38	-1.49	0.0	0.0	0.0	0.0	0.0	0.0
3.40	1368.78	4.487e+04	5297.49	20.62	16.75	-2.10	0.0	20.15	24.06	0.602	5.3732e-04	0.669
3.05	3715.19	4.858e+04	1.603e+04	23.08	16.50	-2.25	0.0	20.94	11.29	0.400	0.139	0.547
2.55	3.38	4.859e+04	17.46	40.58	16.51	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.49	5.53	4.859e+04	29.22	40.58	15.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.45	4.30	4.860e+04	23.12	40.58	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.43	5.40	4.860e+04	29.23	40.58	14.89	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.37	5.26	4.861e+04	29.22	40.58	14.22	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.31	5.13	4.861e+04	29.23	40.58	13.55	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.27	8.02	4.862e+04	46.53	41.63	30.64	-0.04	0.0	0.0	0.0	0.0	0.0	0.0
2.26	5.02	4.862e+04	29.18	41.88	29.97	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.26	5.00	4.863e+04	29.18	41.88	29.30	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.25	393.20	4.902e+04	2299.58	13.54	25.06	-2.16	0.0	1.11	30.28	0.156	1.958	0.941
2.24	11.73	4.903e+04	68.81	20.83	27.85	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.86	4.904e+04	34.40	41.88	27.85	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	6.12	4.905e+04	35.97	-0.60	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.24	11.69	4.906e+04	68.81	20.83	27.06	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.24	5.84	4.906e+04	34.40	41.88	27.06	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
2.23	11.66	4.908e+04	68.81	20.83	26.28	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.23	11.91	4.909e+04	70.38	20.59	22.09	-2.08	0.0	0.0	0.0	0.0	0.0	0.0
2.23	5.82	4.909e+04	34.40	-0.22	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	11.62	4.911e+04	68.81	20.83	25.49	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.22	5.81	4.911e+04	34.40	41.88	25.49	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.22	15.96	4.913e+04	94.72	11.49	24.21	-1.44	0.0	0.0	0.0	0.0	0.0	0.0
2.22	16.53	4.914e+04	98.18	25.27	25.68	-0.88	0.0	0.0	0.0	0.0	0.0	0.0
2.21	5.79	4.915e+04	34.40	41.88	24.70	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.21	11.55	4.916e+04	68.81	20.83	23.92	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.21	11.80	4.917e+04	70.38	21.43	20.94	-2.00	0.0	0.0	0.0	0.0	0.0	0.0
2.20	11.52	4.918e+04	68.81	20.83	23.13	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.20	5.75	4.919e+04	34.40	-0.22	21.56	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	5.75	4.920e+04	34.40	41.88	23.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.20	11.48	4.921e+04	68.81	20.83	22.34	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.19	6.00	4.921e+04	35.97	2.69	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	5.73	4.922e+04	34.40	41.88	22.34	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.19	11.44	4.923e+04	68.81	20.83	21.56	-0.28	0.0	0.0	0.0	0.0	0.0	0.0
2.18	21.42	4.925e+04	129.12	20.27	23.20	-1.92	0.0	0.0	0.0	0.0	0.0	0.0
2.18	16.10	4.927e+04	97.09	25.15	22.67	-0.88	0.0	0.0	0.0	0.0	0.0	0.0
2.18	5.69	4.927e+04	34.40	41.88	20.77	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.18	73.61	4.935e+04	445.37	19.22	20.05	-1.32	0.0	20.83	19.97	0.076	0.713	0.043
2.17	5.94	4.935e+04	35.97	4.33	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.17	5.18	4.936e+04	31.42	41.88	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	5.91	4.936e+04	35.97	5.16	18.09	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.16	8.26	4.937e+04	50.37	14.98	19.99	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.15	1221.03	5.059e+04	7473.13	22.84	13.76	-2.17	0.0	22.55	11.04	0.170	0.025	0.494
2.05	47.40	5.064e+04	304.23	3.74	5.99	-0.44	0.0	-0.18	5.90	0.052	6.800	0.099
1.30	1062.51	5.170e+04	1.075e+04	20.77	17.75	-2.17	0.0	31.02	16.81	0.675	0.866	0.039
0.45	250.48	5.195e+04	7324.35	20.64	16.64	-2.17	0.0	20.46	11.88	0.520	0.011	0.459
0.33	22.17	5.198e+04	897.58	20.91	23.25	-0.72	0.0	20.83	20.06	0.336	0.029	0.799
Risulta	5.198e+04		1.962e+05									

11. RISULTATI OPERE DI FONDAZIONE

LEGENDA RISULTATI OPERE DI FONDAZIONE

Il controllo dei risultati delle analisi condotte, per quanto concerne le opere di fondazione, è possibile in relazione alle tabelle sotto riportate.

La tabella è riferita alle fondazioni tipo trave su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni alle estremità dell'elemento e la massima (in valore assoluto) pressione lungo lo sviluppo dell'elemento.

Vengono inoltre riportati, con funzione statistica, i valori massimo e minimo delle pressioni che compaiono nella tabella.

Elem.	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2	Cmb	Pt ini daN/cm2	Pt fin daN/cm2	Pt max daN/cm2
105	2	-0.64	-0.64	-0.64	91	-0.50	-0.49	-0.50	123	-0.47	-0.47	-0.47
	132	-0.48	-0.47	-0.48	165	-0.46	-0.45	-0.46	171	-0.45	-0.45	-0.45
106	2	-0.63	-0.63	-0.63	91	-0.49	-0.48	-0.49	123	-0.47	-0.46	-0.47
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45
107	2	-0.62	-0.62	-0.62	76	-0.43	-0.43	-0.43	108	-0.43	-0.43	-0.43
	132	-0.47	-0.46	-0.47	165	-0.44	-0.43	-0.44	171	-0.43	-0.43	-0.43
108	2	-0.59	-0.59	-0.59	98	-0.43	-0.43	-0.43	130	-0.42	-0.42	-0.42
	132	-0.44	-0.44	-0.44	165	-0.42	-0.42	-0.42	171	-0.41	-0.41	-0.41
109	2	-0.62	-0.62	-0.62	92	-0.43	-0.43	-0.44	103	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.44	-0.43	-0.44	171	-0.43	-0.43	-0.43
110	2	-0.64	-0.63	-0.64	89	-0.48	-0.48	-0.48	121	-0.46	-0.46	-0.46
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45
111	2	-0.63	-0.63	-0.63	78	-0.44	-0.44	-0.44	110	-0.43	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
112	2	-0.62	-0.62	-0.62	84	-0.44	-0.43	-0.44	116	-0.43	-0.43	-0.43
	132	-0.46	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
113	2	-0.62	-0.62	-0.62	76	-0.45	-0.45	-0.45	108	-0.44	-0.44	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.44	-0.43	-0.44
114	2	-0.62	-0.62	-0.62	94	-0.43	-0.43	-0.43	126	-0.43	-0.43	-0.43
	132	-0.46	-0.47	-0.47	165	-0.44	-0.43	-0.44	171	-0.43	-0.43	-0.43
115	8	-0.65	-0.64	-0.65	91	-0.50	-0.50	-0.50	123	-0.48	-0.47	-0.48
	135	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.46	-0.46	-0.46
116	8	-0.62	-0.61	-0.62	96	-0.46	-0.46	-0.46	128	-0.44	-0.44	-0.44
	135	-0.46	-0.46	-0.46	165	-0.44	-0.43	-0.44	171	-0.43	-0.43	-0.43
117	2	-0.60	-0.60	-0.60	90	-0.43	-0.43	-0.43	122	-0.42	-0.42	-0.42
	132	-0.45	-0.45	-0.45	165	-0.42	-0.42	-0.42	171	-0.41	-0.41	-0.41
124	2	-0.61	-0.62	-0.62	80	-0.44	-0.44	-0.44	112	-0.43	-0.44	-0.44
	132	-0.46	-0.46	-0.46	165	-0.43	-0.44	-0.44	171	-0.43	-0.43	-0.43
125	2	-0.62	-0.61	-0.62	76	-0.44	-0.44	-0.44	108	-0.44	-0.43	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.43	-0.44	171	-0.43	-0.43	-0.43
126	8	-0.65	-0.64	-0.65	95	-0.47	-0.47	-0.47	127	-0.46	-0.46	-0.46
	135	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.46	-0.45	-0.46
127	8	-0.65	-0.65	-0.65	95	-0.48	-0.47	-0.48	127	-0.47	-0.46	-0.47
	135	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.46	-0.46	-0.46
128	8	-0.71	-0.70	-0.71	95	-0.54	-0.54	-0.54	127	-0.51	-0.51	-0.51
	135	-0.53	-0.52	-0.53	166	-0.50	-0.50	-0.50	171	-0.50	-0.49	-0.50
129	8	-0.71	-0.71	-0.71	95	-0.54	-0.54	-0.54	127	-0.51	-0.51	-0.51
	135	-0.53	-0.53	-0.53	166	-0.50	-0.50	-0.50	171	-0.49	-0.49	-0.49
130	8	-0.69	-0.69	-0.69	85	-0.53	-0.53	-0.53	117	-0.50	-0.50	-0.50
	135	-0.52	-0.52	-0.52	166	-0.49	-0.49	-0.49	171	-0.49	-0.48	-0.49
131	2	-0.65	-0.62	-0.65	95	-0.47	-0.45	-0.47	127	-0.46	-0.44	-0.46
	132	-0.48	-0.47	-0.48	165	-0.46	-0.44	-0.46	171	-0.46	-0.44	-0.46
132	8	-0.61	-0.61	-0.61	96	-0.46	-0.46	-0.46	128	-0.44	-0.44	-0.44
	135	-0.46	-0.46	-0.46	166	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43
133	2	-0.64	-0.64	-0.64	82	-0.45	-0.45	-0.45	114	-0.45	-0.45	-0.45
	132	-0.48	-0.48	-0.48	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
134	2	-0.62	-0.61	-0.62	76	-0.44	-0.44	-0.44	108	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43
135	2	-0.62	-0.62	-0.62	91	-0.45	-0.44	-0.45	123	-0.44	-0.44	-0.44
	132	-0.47	-0.46	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
136	2	-0.62	-0.62	-0.62	98	-0.43	-0.43	-0.43	130	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



137	2	-0.62	-0.62	-0.62	82	-0.43	-0.43	-0.43	114	-0.43	-0.43	-0.43
	132	-0.47	-0.46	-0.47	165	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43
138	8	-0.67	-0.67	-0.67	85	-0.51	-0.51	-0.51	117	-0.49	-0.49	-0.49
	135	-0.50	-0.50	-0.50	165	-0.48	-0.48	-0.48	171	-0.47	-0.47	-0.47
139	2	-0.66	-0.65	-0.66	69	-0.47	-0.47	-0.47	117	-0.46	-0.46	-0.46
	132	-0.49	-0.49	-0.49	165	-0.46	-0.46	-0.46	171	-0.46	-0.45	-0.46
140	2	-0.62	-0.62	-0.62	88	-0.43	-0.43	-0.43	120	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.44	-0.43	-0.44	171	-0.43	-0.43	-0.43
141	2	-0.63	-0.62	-0.63	89	-0.44	-0.42	-0.44	121	-0.44	-0.43	-0.44
	132	-0.47	-0.46	-0.47	165	-0.45	-0.44	-0.45	171	-0.44	-0.43	-0.44
142	2	-0.66	-0.66	-0.66	89	-0.50	-0.50	-0.50	121	-0.48	-0.48	-0.48
	132	-0.49	-0.49	-0.49	165	-0.47	-0.47	-0.47	171	-0.46	-0.46	-0.46
143	2	-0.64	-0.64	-0.64	89	-0.49	-0.48	-0.49	121	-0.47	-0.46	-0.47
	132	-0.48	-0.48	-0.48	165	-0.46	-0.45	-0.46	171	-0.45	-0.45	-0.45
144	2	-0.62	-0.62	-0.62	85	-0.45	-0.42	-0.45	117	-0.44	-0.43	-0.44
	132	-0.47	-0.46	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.43	-0.44
145	2	-0.63	-0.62	-0.63	83	-0.45	-0.43	-0.45	115	-0.45	-0.43	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.44	-0.45	171	-0.44	-0.43	-0.44
146	2	-0.64	-0.63	-0.64	91	-0.49	-0.48	-0.49	123	-0.47	-0.46	-0.47
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45
147	2	-0.63	-0.63	-0.63	91	-0.48	-0.48	-0.48	123	-0.46	-0.46	-0.46
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.44	-0.45
148	2	-0.62	-0.62	-0.62	76	-0.43	-0.43	-0.43	108	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.42	-0.43
149	2	-0.59	-0.58	-0.59	98	-0.43	-0.42	-0.43	130	-0.42	-0.41	-0.42
	132	-0.44	-0.44	-0.44	165	-0.42	-0.41	-0.42	171	-0.41	-0.40	-0.41
150	2	-0.63	-0.63	-0.63	85	-0.48	-0.47	-0.48	117	-0.46	-0.45	-0.46
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.44	-0.45
151	2	-0.63	-0.63	-0.63	82	-0.44	-0.44	-0.44	114	-0.44	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.43	-0.44	-0.44
152	2	-0.62	-0.62	-0.62	76	-0.45	-0.44	-0.45	108	-0.44	-0.44	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
153	8	-0.64	-0.64	-0.64	91	-0.50	-0.49	-0.50	123	-0.47	-0.47	-0.47
	135	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.46	-0.46	-0.46
154	2	-0.61	-0.60	-0.61	96	-0.46	-0.44	-0.46	128	-0.44	-0.42	-0.44
	132	-0.46	-0.45	-0.46	165	-0.43	-0.42	-0.43	171	-0.43	-0.42	-0.43
155	2	-0.60	-0.61	-0.61	90	-0.43	-0.45	-0.45	122	-0.42	-0.43	-0.43
	132	-0.45	-0.46	-0.46	165	-0.42	-0.43	-0.43	171	-0.41	-0.42	-0.42
156	2	-0.62	-0.62	-0.62	80	-0.44	-0.45	-0.45	112	-0.44	-0.44	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
157	2	-0.61	-0.62	-0.62	76	-0.44	-0.44	-0.44	108	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43
158	2	-0.64	-0.64	-0.64	79	-0.47	-0.46	-0.47	127	-0.46	-0.45	-0.46
	132	-0.48	-0.48	-0.48	165	-0.46	-0.45	-0.46	171	-0.45	-0.45	-0.45
159	8	-0.65	-0.65	-0.65	95	-0.47	-0.47	-0.47	127	-0.46	-0.46	-0.46
	135	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.46	-0.46	-0.46
160	8	-0.70	-0.70	-0.70	95	-0.54	-0.53	-0.54	127	-0.51	-0.51	-0.51
	135	-0.52	-0.52	-0.52	166	-0.50	-0.50	-0.50	171	-0.49	-0.49	-0.49
161	8	-0.71	-0.70	-0.71	95	-0.54	-0.54	-0.54	127	-0.51	-0.51	-0.51
	135	-0.53	-0.52	-0.53	166	-0.50	-0.49	-0.50	171	-0.49	-0.49	-0.49
162	8	-0.69	-0.69	-0.69	85	-0.53	-0.52	-0.53	117	-0.50	-0.50	-0.50
	135	-0.52	-0.51	-0.52	165	-0.49	-0.49	-0.49	171	-0.48	-0.48	-0.48
163	2	-0.62	-0.62	-0.62	91	-0.45	-0.45	-0.45	123	-0.44	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
164	8	-0.61	-0.59	-0.61	96	-0.46	-0.44	-0.46	128	-0.44	-0.42	-0.44
	135	-0.46	-0.44	-0.46	165	-0.43	-0.42	-0.43	171	-0.43	-0.41	-0.43
165	2	-0.64	-0.64	-0.64	82	-0.45	-0.45	-0.45	114	-0.45	-0.45	-0.45
	132	-0.48	-0.48	-0.48	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
166	2	-0.61	-0.61	-0.61	80	-0.44	-0.44	-0.44	112	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43
167	2	-0.62	-0.62	-0.62	91	-0.44	-0.44	-0.44	123	-0.44	-0.44	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.44	-0.43	-0.44
168	2	-0.62	-0.62	-0.62	98	-0.43	-0.43	-0.43	130	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.42	-0.43
169	2	-0.62	-0.62	-0.62	98	-0.43	-0.43	-0.43	130	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.42	-0.43
170	2	-0.67	-0.67	-0.67	85	-0.51	-0.50	-0.51	117	-0.49	-0.48	-0.49
	132	-0.50	-0.50	-0.50	165	-0.48	-0.47	-0.48	171	-0.47	-0.47	-0.47
171	2	-0.65	-0.65	-0.65	69	-0.47	-0.47	-0.47	101	-0.46	-0.46	-0.46
	132	-0.49	-0.49	-0.49	165	-0.46	-0.46	-0.46	171	-0.45	-0.45	-0.45
172	2	-0.62	-0.62	-0.62	88	-0.43	-0.43	-0.43	120	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.42	-0.43
173	2	-0.66	-0.65	-0.66	89	-0.50	-0.49	-0.50	121	-0.48	-0.47	-0.48
	132	-0.49	-0.49	-0.49	165	-0.47	-0.46	-0.47	171	-0.46	-0.46	-0.46
174	2	-0.64	-0.64	-0.64	83	-0.48	-0.47	-0.48	115	-0.46	-0.46	-0.46
	132	-0.48	-0.48	-0.48	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



175	2	-0.63	-0.63	-0.63	91	-0.48	-0.48	-0.48	123	-0.46	-0.46	-0.46
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45
176	2	-0.63	-0.63	-0.63	91	-0.48	-0.47	-0.48	123	-0.46	-0.45	-0.46
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
177	2	-0.62	-0.62	-0.62	88	-0.43	-0.43	-0.43	120	-0.43	-0.42	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
178	2	-0.58	-0.58	-0.58	98	-0.42	-0.42	-0.42	130	-0.41	-0.41	-0.41
	132	-0.44	-0.44	-0.44	165	-0.41	-0.41	-0.41	171	-0.40	-0.40	-0.40
179	2	-0.63	-0.63	-0.63	85	-0.47	-0.46	-0.47	117	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
180	2	-0.63	-0.63	-0.63	74	-0.44	-0.44	-0.44	106	-0.44	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
181	2	-0.62	-0.62	-0.62	68	-0.44	-0.44	-0.44	100	-0.44	-0.44	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
182	2	-0.64	-0.64	-0.64	91	-0.49	-0.49	-0.49	123	-0.47	-0.47	-0.47
	132	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.46	-0.45	-0.46
183	2	-0.60	-0.60	-0.60	96	-0.44	-0.44	-0.44	128	-0.42	-0.42	-0.42
	132	-0.45	-0.45	-0.45	165	-0.42	-0.42	-0.42	171	-0.42	-0.42	-0.42
184	2	-0.61	-0.61	-0.61	90	-0.45	-0.45	-0.45	122	-0.43	-0.44	-0.44
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.43	-0.43
185	2	-0.62	-0.62	-0.62	96	-0.44	-0.45	-0.45	128	-0.44	-0.44	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
186	2	-0.64	-0.63	-0.64	79	-0.46	-0.46	-0.46	111	-0.46	-0.45	-0.46
	132	-0.48	-0.47	-0.48	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45
187	8	-0.70	-0.69	-0.70	95	-0.53	-0.52	-0.53	127	-0.51	-0.50	-0.51
	135	-0.52	-0.51	-0.52	166	-0.50	-0.49	-0.50	171	-0.49	-0.48	-0.49
188	8	-0.70	-0.69	-0.70	95	-0.54	-0.53	-0.54	127	-0.51	-0.50	-0.51
	135	-0.52	-0.51	-0.52	166	-0.49	-0.49	-0.49	171	-0.49	-0.48	-0.49
189	8	-0.69	-0.69	-0.69	85	-0.52	-0.52	-0.52	117	-0.50	-0.49	-0.50
	135	-0.51	-0.51	-0.51	165	-0.49	-0.48	-0.49	171	-0.48	-0.48	-0.48
190	2	-0.62	-0.62	-0.62	91	-0.45	-0.45	-0.45	123	-0.44	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
191	2	-0.59	-0.59	-0.59	96	-0.44	-0.44	-0.44	128	-0.42	-0.42	-0.42
	132	-0.44	-0.44	-0.44	165	-0.42	-0.42	-0.42	171	-0.41	-0.41	-0.41
192	2	-0.64	-0.64	-0.64	82	-0.45	-0.45	-0.45	114	-0.45	-0.45	-0.45
	132	-0.48	-0.48	-0.48	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
193	2	-0.61	-0.61	-0.61	80	-0.44	-0.44	-0.44	112	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43
194	2	-0.62	-0.62	-0.62	71	-0.44	-0.44	-0.44	103	-0.44	-0.43	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
195	2	-0.62	-0.62	-0.62	98	-0.43	-0.43	-0.43	130	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
196	2	-0.62	-0.62	-0.62	98	-0.43	-0.43	-0.43	130	-0.43	-0.42	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
197	2	-0.67	-0.66	-0.67	85	-0.50	-0.50	-0.50	117	-0.48	-0.48	-0.48
	132	-0.50	-0.49	-0.50	165	-0.47	-0.47	-0.47	171	-0.47	-0.47	-0.47
198	2	-0.65	-0.65	-0.65	69	-0.47	-0.46	-0.47	101	-0.46	-0.46	-0.46
	132	-0.49	-0.48	-0.49	165	-0.46	-0.46	-0.46	171	-0.45	-0.45	-0.45
199	2	-0.62	-0.61	-0.62	88	-0.43	-0.43	-0.43	120	-0.43	-0.42	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
200	2	-0.65	-0.65	-0.65	89	-0.49	-0.48	-0.49	121	-0.47	-0.47	-0.47
	132	-0.49	-0.48	-0.49	165	-0.46	-0.46	-0.46	171	-0.46	-0.46	-0.46
201	2	-0.64	-0.64	-0.64	83	-0.47	-0.47	-0.47	115	-0.46	-0.45	-0.46
	132	-0.48	-0.47	-0.48	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45
202	2	-0.63	-0.63	-0.63	91	-0.48	-0.47	-0.48	123	-0.46	-0.45	-0.46
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.44	-0.45
203	2	-0.63	-0.63	-0.63	91	-0.47	-0.46	-0.47	123	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
204	2	-0.62	-0.62	-0.62	88	-0.43	-0.43	-0.43	120	-0.42	-0.42	-0.42
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
205	2	-0.58	-0.58	-0.58	98	-0.42	-0.42	-0.42	130	-0.41	-0.41	-0.41
	132	-0.44	-0.44	-0.44	165	-0.41	-0.41	-0.41	171	-0.40	-0.40	-0.40
206	2	-0.63	-0.63	-0.63	85	-0.46	-0.46	-0.46	117	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.44	-0.45	171	-0.44	-0.44	-0.44
207	2	-0.63	-0.63	-0.63	74	-0.44	-0.44	-0.44	106	-0.44	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
208	2	-0.62	-0.62	-0.62	68	-0.44	-0.44	-0.44	100	-0.44	-0.43	-0.44
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
209	2	-0.64	-0.64	-0.64	91	-0.49	-0.48	-0.49	123	-0.47	-0.46	-0.47
	132	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.45	-0.45	-0.45
210	2	-0.62	-0.62	-0.62	96	-0.45	-0.45	-0.45	128	-0.44	-0.44	-0.44
	132	-0.46	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.43	-0.44	-0.44
211	2	-0.63	-0.63	-0.63	79	-0.46	-0.46	-0.46	111	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.44	-0.45
212	8	-0.69	-0.68	-0.69	95	-0.52	-0.51	-0.52	127	-0.50	-0.49	-0.50
	135	-0.51	-0.51	-0.51	166	-0.49	-0.48	-0.49	171	-0.48	-0.48	-0.48

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



213	8	-0.69	-0.68	-0.69	95	-0.53	-0.53	-0.53	127	-0.50	-0.50	-0.50
	135	-0.51	-0.51	-0.51	166	-0.49	-0.48	-0.49	171	-0.48	-0.48	-0.48
214	8	-0.69	-0.68	-0.69	85	-0.52	-0.51	-0.52	117	-0.49	-0.49	-0.49
	135	-0.51	-0.51	-0.51	165	-0.48	-0.48	-0.48	171	-0.48	-0.48	-0.48
215	2	-0.62	-0.62	-0.62	91	-0.45	-0.45	-0.45	123	-0.44	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
216	2	-0.59	-0.59	-0.59	96	-0.44	-0.44	-0.44	128	-0.42	-0.42	-0.42
	132	-0.44	-0.44	-0.44	165	-0.42	-0.42	-0.42	171	-0.41	-0.41	-0.41
217	2	-0.64	-0.64	-0.64	78	-0.45	-0.45	-0.45	110	-0.45	-0.44	-0.45
	132	-0.48	-0.48	-0.48	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
218	2	-0.61	-0.61	-0.61	80	-0.44	-0.43	-0.44	112	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43
219	2	-0.62	-0.62	-0.62	71	-0.44	-0.43	-0.44	103	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
220	2	-0.62	-0.61	-0.62	98	-0.43	-0.43	-0.43	130	-0.43	-0.42	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
221	2	-0.62	-0.62	-0.62	98	-0.43	-0.43	-0.43	130	-0.42	-0.42	-0.42
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
222	2	-0.66	-0.66	-0.66	85	-0.50	-0.49	-0.50	117	-0.48	-0.47	-0.48
	132	-0.49	-0.49	-0.49	165	-0.47	-0.47	-0.47	171	-0.47	-0.46	-0.47
223	2	-0.65	-0.65	-0.65	69	-0.46	-0.46	-0.46	101	-0.46	-0.45	-0.46
	132	-0.48	-0.48	-0.48	165	-0.46	-0.45	-0.46	171	-0.45	-0.45	-0.45
224	2	-0.61	-0.61	-0.61	88	-0.43	-0.43	-0.43	120	-0.42	-0.42	-0.42
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
225	2	-0.65	-0.65	-0.65	89	-0.48	-0.47	-0.48	121	-0.47	-0.46	-0.47
	132	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.46	-0.45	-0.46
226	2	-0.64	-0.63	-0.64	83	-0.47	-0.46	-0.47	115	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.44	-0.45
227	2	-0.63	-0.63	-0.63	91	-0.47	-0.46	-0.47	123	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
228	2	-0.63	-0.63	-0.63	91	-0.46	-0.46	-0.46	123	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.44	-0.45	171	-0.44	-0.44	-0.44
229	2	-0.62	-0.61	-0.62	88	-0.43	-0.43	-0.43	120	-0.42	-0.42	-0.42
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
230	2	-0.58	-0.58	-0.58	98	-0.42	-0.42	-0.42	130	-0.41	-0.41	-0.41
	132	-0.44	-0.44	-0.44	165	-0.41	-0.41	-0.41	171	-0.40	-0.40	-0.40
231	2	-0.63	-0.62	-0.63	85	-0.46	-0.45	-0.46	117	-0.45	-0.44	-0.45
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
232	2	-0.63	-0.64	-0.64	69	-0.44	-0.45	-0.45	101	-0.44	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.45	-0.45	171	-0.44	-0.44	-0.44
233	2	-0.62	-0.62	-0.62	68	-0.44	-0.44	-0.44	100	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
234	2	-0.64	-0.64	-0.64	91	-0.48	-0.47	-0.48	123	-0.46	-0.46	-0.46
	132	-0.48	-0.47	-0.48	165	-0.46	-0.45	-0.46	171	-0.45	-0.45	-0.45
235	2	-0.62	-0.62	-0.62	96	-0.45	-0.45	-0.45	128	-0.44	-0.44	-0.44
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
236	2	-0.63	-0.63	-0.63	79	-0.46	-0.45	-0.46	111	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
237	8	-0.68	-0.67	-0.68	95	-0.51	-0.50	-0.51	127	-0.49	-0.49	-0.49
	135	-0.51	-0.50	-0.51	166	-0.48	-0.48	-0.48	171	-0.48	-0.48	-0.48
238	8	-0.68	-0.68	-0.68	95	-0.53	-0.52	-0.53	127	-0.50	-0.49	-0.50
	135	-0.51	-0.50	-0.51	166	-0.48	-0.48	-0.48	171	-0.48	-0.48	-0.48
239	8	-0.68	-0.68	-0.68	85	-0.51	-0.51	-0.51	117	-0.49	-0.49	-0.49
	135	-0.51	-0.51	-0.51	165	-0.48	-0.48	-0.48	171	-0.48	-0.47	-0.48
240	2	-0.62	-0.62	-0.62	91	-0.45	-0.45	-0.45	123	-0.44	-0.44	-0.44
	132	-0.47	-0.46	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
241	2	-0.59	-0.59	-0.59	96	-0.44	-0.43	-0.44	128	-0.42	-0.42	-0.42
	132	-0.44	-0.44	-0.44	165	-0.42	-0.42	-0.42	171	-0.41	-0.41	-0.41
242	2	-0.64	-0.64	-0.64	90	-0.45	-0.45	-0.45	110	-0.44	-0.44	-0.44
	132	-0.48	-0.47	-0.48	165	-0.45	-0.44	-0.45	171	-0.44	-0.44	-0.44
243	2	-0.61	-0.61	-0.61	80	-0.43	-0.43	-0.43	112	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.43	-0.43	-0.43
244	2	-0.62	-0.62	-0.62	72	-0.44	-0.43	-0.44	104	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.44	-0.43	-0.44	171	-0.43	-0.43	-0.43
245	2	-0.61	-0.61	-0.61	98	-0.43	-0.43	-0.43	130	-0.42	-0.42	-0.42
	132	-0.46	-0.45	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
246	2	-0.62	-0.61	-0.62	98	-0.43	-0.43	-0.43	130	-0.42	-0.42	-0.42
	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
247	2	-0.66	-0.66	-0.66	85	-0.49	-0.48	-0.49	117	-0.47	-0.47	-0.47
	132	-0.49	-0.49	-0.49	165	-0.47	-0.47	-0.47	171	-0.46	-0.46	-0.46
248	2	-0.65	-0.65	-0.65	69	-0.46	-0.46	-0.46	101	-0.45	-0.45	-0.45
	132	-0.48	-0.48	-0.48	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45
249	2	-0.61	-0.61	-0.61	88	-0.43	-0.43	-0.43	120	-0.42	-0.42	-0.42
	132	-0.46	-0.45	-0.46	165	-0.43	-0.42	-0.43	171	-0.42	-0.42	-0.42
250	2	-0.65	-0.64	-0.65	89	-0.47	-0.47	-0.47	121	-0.46	-0.46	-0.46
	132	-0.48	-0.48	-0.48	165	-0.46	-0.46	-0.46	171	-0.45	-0.45	-0.45

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



251	2	-0.63	-0.63	-0.63	83	-0.46	-0.45	-0.46	115	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
252	2	-0.63	-0.62	-0.63	91	-0.46	-0.45	-0.46	123	-0.45	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.45	-0.44	-0.45	171	-0.44	-0.44	-0.44
253	2	-0.63	-0.62	-0.63	91	-0.46	-0.45	-0.46	123	-0.45	-0.44	-0.45
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
254	2	-0.61	-0.61	-0.61	88	-0.43	-0.42	-0.43	120	-0.42	-0.42	-0.42
	132	-0.46	-0.45	-0.46	165	-0.43	-0.42	-0.43	171	-0.42	-0.42	-0.42
255	2	-0.58	-0.58	-0.58	98	-0.42	-0.42	-0.42	130	-0.41	-0.41	-0.41
	132	-0.44	-0.44	-0.44	165	-0.41	-0.41	-0.41	171	-0.40	-0.40	-0.40
256	2	-0.64	-0.64	-0.64	69	-0.45	-0.45	-0.45	101	-0.44	-0.44	-0.44
	132	-0.47	-0.48	-0.48	165	-0.45	-0.45	-0.45	171	-0.44	-0.44	-0.44
257	2	-0.62	-0.62	-0.62	68	-0.44	-0.44	-0.44	100	-0.43	-0.43	-0.43
	132	-0.46	-0.46	-0.46	165	-0.44	-0.44	-0.44	171	-0.43	-0.43	-0.43
258	2	-0.64	-0.63	-0.64	91	-0.47	-0.47	-0.47	123	-0.46	-0.45	-0.46
	132	-0.47	-0.47	-0.47	165	-0.45	-0.45	-0.45	171	-0.45	-0.45	-0.45
259	2	-0.62	-0.63	-0.63	96	-0.45	-0.46	-0.46	128	-0.44	-0.45	-0.45
	132	-0.47	-0.47	-0.47	165	-0.44	-0.44	-0.44	171	-0.44	-0.44	-0.44
...												
566	132	-0.46	-0.46	-0.46	165	-0.43	-0.43	-0.43	171	-0.42	-0.42	-0.42
Elem.		Pt ini	Pt fin	Pt max		Pt ini	Pt fin	Pt max		Pt ini	Pt fin	Pt max
		-0.71										
		-0.39										

12. RISULTATI ELEMENTI TIPO TRAVE

LEGENDA RISULTATI ELEMENTI TIPO TRAVE

Il controllo dei risultati delle analisi condotte, per quanto concerne gli elementi tipo trave, è possibile in relazione alle tabelle sotto riportate.

Gli elementi vengono suddivisi in relazione alle proprietà in elementi:

- tipo **pilastro**
- tipo **trave in elevazione**
- tipo **trave in fondazione**

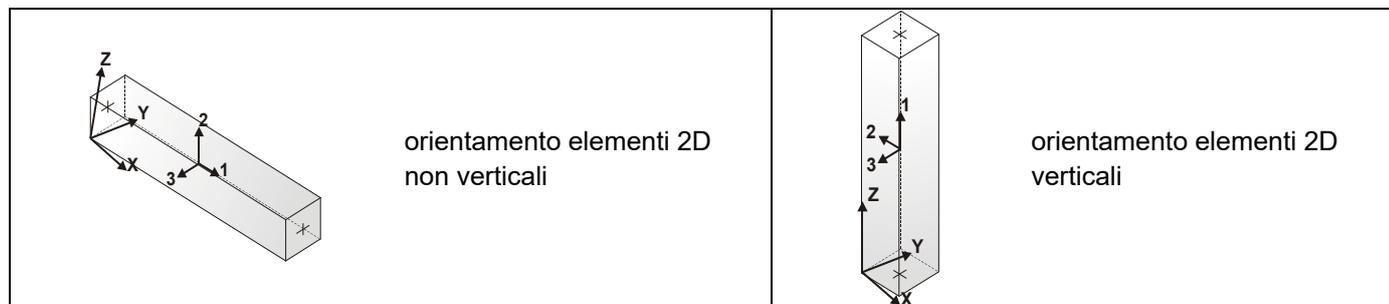
Per ogni elemento e per ogni combinazione (o caso di carico) vengono riportati i risultati più significativi.

Per gli elementi tipo *pilastro* sono riportati in tabella i seguenti valori:

Pilas.	numero dell'elemento pilastro
Cmb	combinazione in cui si verificano i valori riportati
M3 mx/mn	momento flettente in campata M3 max (prima riga) / min (seconda riga)
M2 mx/mn	momento flettente in campata M2 max (prima riga) / min (seconda riga)
D2/D3	freccia massima in direzione 2 (prima riga) / direzione 3 (seconda riga)
Q2/Q3	carico totale in direzione 2 (prima riga) / direzione 3 (seconda riga)
Pos.	ascissa del punto iniziale e finale dell'elemento
N, V2, ecc..	sei componenti di sollecitazione al piede ed in sommità dell'elemento

Per gli elementi tipo *trave in elevazione* sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri.

Per gli elementi tipo *trave in fondazione* (trave f.) sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri e la massima pressione sul terreno.



Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Trave f.	Cmb M3 mx/mn		D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3	
	daN cm	daN cm										cm
105	12	7.207e+04	-8118.40	9.28e-03	-0.63	0.0	71.57	-4521.57	109.21	2.285e+04	-1.450e+04	7.207e+04
		-1.181e+05	-1.450e+04	3.75e-04		58.4	71.57	-1993.27	109.21	2.278e+04	-8118.40	-1.181e+05
105	42	6.376e+04	-4741.48	7.26e-03	-0.48	0.0	-130.70	-3441.44	47.59	1.794e+04	-7520.67	6.376e+04
		-8.191e+04	-7520.67	2.44e-04		58.4	-130.70	-1549.73	47.59	1.788e+04	-4741.48	-8.191e+04
105	45	8.982e+04	-1.048e+04	0.01	-0.59	0.0	-260.28	-4586.28	61.37	2.547e+04	-1.407e+04	8.982e+04
		-1.113e+05	-1.407e+04	4.16e-04		58.4	-260.28	-2303.54	61.37	2.537e+04	-1.048e+04	-1.113e+05
105	47	7.197e+04	-8267.78	9.75e-03	-0.44	0.0	-329.01	-3551.72	58.27	1.877e+04	-1.167e+04	7.197e+04
		-8.670e+04	-1.167e+04	2.65e-04		58.4	-329.01	-1885.07	58.27	1.869e+04	-8267.78	-8.670e+04
105	59	6.702e+04	-1.697e+04	0.01	-0.60	0.0	-66.53	-4755.12	90.48	2.071e+04	-2.226e+04	6.702e+04
		-1.418e+05	-2.226e+04	3.77e-04		58.4	-66.53	-2401.57	90.48	2.061e+04	-1.697e+04	-1.418e+05
105	63	7.282e+04	-1.540e+04	0.02	-0.62	0.0	-128.52	-4998.19	94.11	2.188e+04	-2.089e+04	7.282e+04
		-1.477e+05	-2.089e+04	3.57e-04		58.4	-128.52	-2560.48	94.11	2.177e+04	-1.540e+04	-1.477e+05
105	83	6.905e+04	-3.048e+04	0.02	-0.49	0.0	-197.25	-4058.51	10.40	-3046.77	-3.109e+04	6.905e+04
		-1.103e+05	-3.109e+04	2.81e-04		58.4	-197.25	-2091.19	10.40	-3116.46	-3.048e+04	-1.103e+05
105	91	6.932e+04	-3.814e+04	0.02	-0.50	0.0	-228.70	-4071.04	111.01	419.26	-4.463e+04	6.932e+04
		-1.101e+05	-4.463e+04	5.82e-05		58.4	-228.70	-2081.47	111.01	334.06	-3.814e+04	-1.101e+05
105	92	3.874e+04	3.195e+04	5.66e-03	-0.41	0.0	122.19	-2656.94	-190.41	3.190e+04	3.195e+04	3.874e+04
		-7.227e+04	2.084e+04	4.90e-04		58.4	122.19	-1143.41	-190.41	3.183e+04	2.084e+04	-7.227e+04
105	93	6.809e+04	-3.827e+04	0.02	-0.49	0.0	-147.63	-4024.62	288.04	3406.10	-5.509e+04	6.809e+04
		-1.091e+05	-5.509e+04	1.03e-04		58.4	-147.63	-2049.40	288.04	3339.67	-3.827e+04	-1.091e+05
105	94	3.750e+04	2.149e+04	6.14e-03	-0.41	0.0	203.26	-2610.53	-13.37	3.489e+04	2.149e+04	3.750e+04
		-7.122e+04	2.071e+04	5.35e-04		58.4	203.26	-1111.35	-13.37	3.484e+04	2.071e+04	-7.122e+04
105	115	5.977e+04	-1.757e+04	0.01	-0.47	0.0	-87.15	-3632.75	34.62	9254.50	-1.960e+04	5.977e+04
		-9.868e+04	-1.960e+04	2.91e-04		58.4	-87.15	-1797.78	34.62	9187.36	-1.757e+04	-9.868e+04
105	123	5.988e+04	-2.069e+04	0.01	-0.47	0.0	-99.94	-3637.84	75.56	1.066e+04	-2.510e+04	5.988e+04
		-9.859e+04	-2.510e+04	2.00e-04		58.4	-99.94	-1793.82	75.56	1.059e+04	-2.069e+04	-9.859e+04
105	124	4.742e+04	6056.98	2.40e-03	-0.44	0.0	42.83	-3061.85	-47.09	2.347e+04	6056.98	4.742e+04
		-8.317e+04	3307.35	3.76e-04		58.4	42.83	-1411.52	-47.09	2.341e+04	3307.35	-8.317e+04
105	125	5.940e+04	-2.074e+04	0.01	-0.47	0.0	-68.27	-3619.71	144.72	1.183e+04	-2.919e+04	5.940e+04
		-9.818e+04	-2.919e+04	2.17e-04		58.4	-68.27	-1781.29	144.72	1.177e+04	-2.074e+04	-9.818e+04
105	126	4.694e+04	3259.00	2.21e-03	-0.43	0.0	74.50	-3043.72	22.07	2.464e+04	3259.00	4.694e+04
		-8.276e+04	1969.93	3.93e-04		58.4	74.50	-1399.00	22.07	2.458e+04	1969.93	-8.276e+04
105	137	5.351e+04	-6529.16	6.94e-03	-0.47	0.0	44.58	-3354.42	79.22	1.712e+04	-1.116e+04	5.351e+04
		-8.791e+04	-1.116e+04	2.78e-04		58.4	44.58	-1490.79	79.22	1.707e+04	-6529.16	-8.791e+04
105	151	5.987e+04	-5753.85	6.01e-03	-0.47	0.0	-44.45	-3324.05	40.20	1.831e+04	-8101.62	5.987e+04
		-8.018e+04	-8101.62	2.90e-04		58.4	-44.45	-1474.08	40.20	1.825e+04	-5753.85	-8.018e+04
105	153	6.534e+04	-8104.72	7.68e-03	-0.44	0.0	-176.65	-3397.57	47.32	1.887e+04	-1.087e+04	6.534e+04
		-8.337e+04	-1.087e+04	3.05e-04		58.4	-176.65	-1697.64	47.32	1.879e+04	-8104.72	-8.337e+04
105	160	5.014e+04	-1.243e+04	0.01	-0.45	0.0	-47.49	-3510.13	66.73	1.570e+04	-1.633e+04	5.014e+04
		-1.037e+05	-1.633e+04	2.79e-04		58.4	-47.49	-1762.99	66.73	1.562e+04	-1.243e+04	-1.037e+05
105	162	5.401e+04	-1.138e+04	0.01	-0.46	0.0	-88.82	-3672.17	69.15	1.648e+04	-1.542e+04	5.401e+04
		-1.077e+05	-1.542e+04	2.66e-04		58.4	-88.82	-1868.93	69.15	1.640e+04	-1.138e+04	-1.077e+05
105	165	5.321e+04	-8186.79	7.52e-03	-0.46	0.0	1.90	-3325.21	47.05	1.764e+04	-1.093e+04	5.321e+04
		-8.924e+04	-1.093e+04	2.95e-04		58.4	1.90	-1555.73	47.05	1.758e+04	-8186.79	-8.924e+04
105	166	5.417e+04	-8843.87	8.56e-03	-0.46	0.0	-28.97	-3408.36	51.64	1.765e+04	-1.186e+04	5.417e+04
		-9.337e+04	-1.186e+04	2.90e-04		58.4	-28.97	-1647.16	51.64	1.758e+04	-8843.87	-9.337e+04
105	169	5.565e+04	-8568.27	7.75e-03	-0.45	0.0	-42.26	-3338.62	47.95	1.790e+04	-1.137e+04	5.565e+04
		-8.868e+04	-1.137e+04	2.99e-04		58.4	-42.26	-1606.50	47.95	1.783e+04	-8568.27	-8.868e+04
105	170	5.261e+04	-9433.97	8.33e-03	-0.45	0.0	-16.43	-3361.13	51.84	1.726e+04	-1.246e+04	5.261e+04
		-9.275e+04	-1.246e+04	2.94e-04		58.4	-16.43	-1619.57	51.84	1.720e+04	-9433.97	-9.275e+04
105	171	5.341e+04	-8716.10	7.93e-03	-0.45	0.0	-12.72	-3340.78	48.82	1.765e+04	-1.157e+04	5.341e+04
		-9.068e+04	-1.157e+04	2.97e-04		58.4	-12.72	-1596.41	48.82	1.759e+04	-8716.10	-9.068e+04
106	9	-2.425e+04	-1.037e+04	0.01	-0.46	0.0	-30.75	-1034.15	71.72	-2529.34	-1.595e+04	-2.425e+04
		-6.420e+04	-1.595e+04	-1.32e-04		77.8	-30.75	1.35	71.72	-2593.17	-1.037e+04	-6.420e+04
106	23	-2.437e+04	-9981.89	0.02	-0.46	0.0	-78.97	-1049.08	125.28	-3069.21	-1.973e+04	-2.437e+04
		-6.725e+04	-1.973e+04	-1.48e-04		77.8	-78.97	-59.59	125.28	-3132.72	-9981.89	-6.725e+04
106	40	-2.382e+04	6133.19	5.22e-03	-0.62	0.0	-244.47	-811.21	-7.22	5697.88	6133.19	-2.382e+04
		-4.238e+04	5571.67	7.04e-05		77.8	-244.47	560.91	-7.22	5628.37	5571.67	-4.238e+04
106	47	4502.33	-1787.39	9.15e-03	-0.44	0.0	-163.04	-918.15	39.06	1272.34	-4825.46	4502.33
		-3.502e+04	-4825.46	-1.16e-04		77.8	-163.04	-101.81	39.06	1211.08	-1787.39	-3.502e+04
106	60	-5.655e+04	-3916.13	0.01	-0.61	0.0	-410.44	-753.48	24.28	4965.75	-5804.83	-5.655e+04
		-7.361e+04	-5804.83	1.43e-04		77.8	-410.44	529.82	24.28	4874.51	-3916.13	-7.361e+04
106	63	-4.658e+04	-9325.37	0.02	-0.61	0.0	-262.55	-1030.04	57.06	2697.40	-1.376e+04	-4.658e+04
		-7.907e+04	-1.376e+04	5.13e-05		77.8	-262.55	231.15	57.06	2594.84	-9325.37	-7.907e+04
106	83	-4.243e+04	2.342e+04	0.02	-0.49	0.0	-1807.31	-368.13	-164.90	-4789.77	2.342e+04	-4.243e+04
		-6.320e+04	1.059e+04	8.88e-05		77.8	-1807.31	777.03	-164.90	-4880.70	1.059e+04	-6.320e+04
106	86	1392.27	-1.397e+04	9.86e-03	-0.41	0.0	1566.68	-685.86	184.91	1.605e+04	-2.835e+04	1392.27
		-3.003e+04	-2.835e+04	1.81e-04		77.8	1566.68	-118.19	184.91	1.601e+04	-1.397e+04	-3.003e+04
106	92	4702.45	-1.130e+04	0.01	-0.41	0.0	1786.04	-783.01	-61.55	7660.70	-1.130e+04	4702.45
		-3.471e+04	-1.609e+04	4.24e-04		77.8	1786.04	-226.45	-61.55	7622.55	-1.609e+04	-3.471e+04
106	93	-3.775e+04	1.271e+04	-0.02	-0.49	0.0	-2026.68	-270.99	81.57	3601.09	6369.76	-3.775e+04
		-6.440e+04	6369.76	-1.54e-04		77.8	-2026.68	885.29	81.57	3507.64	1.271e+04	-6.440e+04

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



106	97	-3.781e+04	1.354e+04	-0.02	-0.49	0.0	-2025.29	-272.05	74.95	3252.05	7707.70	-6.198e+04
		-6.440e+04	7707.70	-1.53e-04		77.8	-2025.29	884.31	74.95	3158.25	1.354e+04	-3.781e+04
106	115	-3.874e+04	7971.11	0.01	-0.46	0.0	-807.20	-461.86	-59.72	1409.31	7971.11	-4.089e+04
		-4.928e+04	3325.97	1.16e-04		77.8	-807.20	511.96	-59.72	1333.47	3325.97	-4.089e+04
106	118	-1.640e+04	-6703.66	9.74e-05	-0.43	0.0	566.56	-592.14	79.74	9852.48	-1.291e+04	-1.640e+04
		-3.485e+04	-1.291e+04	1.53e-04		77.8	566.56	146.87	79.74	9796.72	-6703.66	-3.372e+04
106	121	-3.810e+04	4544.03	0.01	-0.46	0.0	-828.07	-441.77	6.88	2164.97	4009.02	-4.165e+04
		-4.939e+04	4009.02	1.27e-04		77.8	-828.07	528.22	6.88	2097.77	4544.03	-3.810e+04
106	124	-1.509e+04	-6156.08	3.04e-04	-0.43	0.0	654.93	-630.74	-17.67	6475.36	-6156.08	-1.509e+04
		-3.616e+04	-7530.64	2.53e-04		77.8	654.93	103.58	-17.67	6420.99	-7530.64	-3.560e+04
106	125	-3.686e+04	4152.96	0.01	-0.47	0.0	-895.57	-423.25	37.69	4786.44	1221.78	-4.220e+04
		-4.923e+04	1221.78	1.72e-05		77.8	-895.57	555.26	37.69	4709.20	4152.96	-3.686e+04
106	134	-2.741e+04	-5062.92	9.83e-03	-0.46	0.0	-88.80	-739.63	33.80	2640.30	-7691.73	-2.741e+04
		-4.983e+04	-7691.73	3.83e-05		77.8	-88.80	202.21	33.80	2572.16	-5062.92	-4.816e+04
106	141	-2.749e+04	-4805.32	0.01	-0.46	0.0	-120.95	-749.59	69.50	2280.38	-1.021e+04	-2.749e+04
		-5.132e+04	-1.021e+04	2.76e-05		77.8	-120.95	161.58	69.50	2212.46	-4805.32	-5.020e+04
106	151	-1.887e+04	3655.18	4.07e-03	-0.47	0.0	-172.89	-587.70	-2.78	4193.23	3655.18	-1.887e+04
		-3.220e+04	3438.90	5.09e-05		77.8	-172.89	415.40	-2.78	4143.40	3438.90	-2.551e+04
106	153	-8240.09	657.68	6.32e-03	-0.44	0.0	-176.99	-662.30	12.02	5174.76	-277.48	-8240.09
		-2.958e+04	-277.48	4.94e-05		77.8	-176.99	133.44	12.02	5108.33	657.68	-2.871e+04
106	161	-4.069e+04	-2886.30	8.61e-03	-0.46	0.0	-283.54	-549.21	18.22	3705.14	-4303.92	-4.069e+04
		-5.303e+04	-4303.50	9.91e-05		77.8	-283.54	394.68	18.22	3640.82	-2886.30	-4.657e+04
106	162	-3.404e+04	-6492.46	0.01	-0.46	0.0	-184.94	-733.59	40.07	2192.91	-9609.15	-3.404e+04
		-5.639e+04	-9609.15	3.82e-05		77.8	-184.94	195.56	40.07	2121.04	-6492.46	-5.479e+04
106	165	-2.916e+04	-877.39	6.06e-03	-0.45	0.0	-124.66	-518.65	6.73	5457.91	-1400.95	-2.916e+04
		-4.083e+04	-1400.95	1.30e-04		77.8	-124.66	372.68	6.73	5395.42	-877.39	-3.475e+04
106	166	-2.834e+04	-2532.36	7.40e-03	-0.45	0.0	-112.44	-580.16	15.95	4883.25	-3773.29	-2.834e+04
		-4.314e+04	-3773.29	1.11e-04		77.8	-112.44	297.62	15.95	4816.86	-2532.36	-3.921e+04
106	169	-2.463e+04	-1050.83	6.38e-03	-0.45	0.0	-133.23	-543.43	9.22	5689.20	-1767.99	-2.463e+04
		-3.822e+04	-1767.99	1.23e-04		77.8	-133.23	296.58	9.22	5623.39	-1050.83	-3.413e+04
106	170	-3.086e+04	-2165.35	7.10e-03	-0.45	0.0	-152.37	-524.98	12.10	5481.77	-3106.29	-3.086e+04
		-4.336e+04	-3106.29	1.35e-04		77.8	-152.37	327.20	12.10	5414.72	-2165.35	-3.844e+04
106	171	-2.865e+04	-1688.84	6.59e-03	-0.45	0.0	-120.32	-527.00	10.01	5630.90	-2467.15	-2.865e+04
		-4.119e+04	-2467.15	1.35e-04		77.8	-120.32	329.42	10.01	5565.09	-1688.84	-3.623e+04
107	2	7.576e+05	2.616e+04	3.91e-03	-0.62	0.0	2883.09	-832.04	-79.66	-4468.70	2.616e+04	7.576e+05
		7.364e+05	1.989e+04	-1.51e-05		78.6	2883.09	446.07	-79.66	-4474.44	1.989e+04	7.425e+05
107	15	4.300e+05	5544.63	5.14e-03	-0.55	0.0	1250.18	-1013.60	59.23	-7527.78	886.76	4.300e+05
		3.790e+05	886.76	-2.07e-04		78.6	1250.18	-286.16	59.23	-7526.62	5544.63	3.790e+05
107	34	3.760e+05	5.116e+04	1.85e-03	-0.43	0.0	935.72	-589.90	-216.28	-5760.53	5.116e+04	3.760e+05
		3.576e+05	3.415e+04	7.50e-05		78.6	935.72	152.43	-216.28	-5748.76	3.415e+04	3.588e+05
107	51	1.412e+05	3.471e+04	1.79e-03	-0.41	0.0	-471.05	-538.62	-110.04	-7170.45	3.471e+04	1.412e+05
		1.216e+05	2.606e+04	-5.36e-05		78.6	-471.05	43.27	-110.04	-7152.64	2.606e+04	1.217e+05
107	54	7.840e+05	2.972e+04	4.23e-03	-0.62	0.0	2293.39	-929.57	-88.96	-4484.58	2.972e+04	7.840e+05
		7.562e+05	2.273e+04	-3.39e-05		78.6	2293.39	287.32	-88.96	-4490.26	2.273e+04	7.588e+05
107	65	2.203e+05	3.949e+04	2.35e-03	-0.41	0.0	-832.58	-673.97	-122.85	-6743.06	3.949e+04	2.203e+05
		1.903e+05	2.983e+04	-7.65e-05		78.6	-832.58	-90.66	-122.85	-6727.03	2.983e+04	1.903e+05
107	79	4.962e+05	1.110e+05	4.78e-03	-0.43	0.0	1194.54	-962.59	-530.45	-1.469e+04	1.110e+05	4.962e+05
		4.454e+05	6.930e+04	1.14e-04		78.6	1194.54	-331.10	-530.45	-1.466e+04	6.930e+04	4.454e+05
107	82	2.325e+05	-4.295e+04	3.45e-03	-0.43	0.0	1304.71	-532.90	425.13	3842.79	-7.638e+04	2.325e+05
		2.143e+05	-7.638e+04	-2.28e-04		78.6	1304.71	80.00	425.13	3819.95	-4.295e+04	2.147e+05
107	84	3.236e+04	2.165e+04	1.56e-03	-0.43	0.0	2196.75	-239.00	-134.39	-8478.48	2.165e+04	3.236e+04
		2.273e+04	1.108e+04	-2.30e-05		78.6	2196.75	392.89	-134.39	-8456.20	1.108e+04	3.236e+04
107	85	7.025e+05	1.526e+04	6.66e-03	-0.43	0.0	302.50	-1256.49	29.06	-2366.07	1.526e+04	7.025e+05
		6.278e+05	1.298e+04	-9.39e-05		78.6	302.50	-645.98	29.06	-2386.18	1.526e+04	6.278e+05
107	87	7.198e+05	6.296e+04	6.63e-03	-0.43	0.0	413.40	-1288.85	-237.49	-8117.79	6.296e+04	7.198e+05
		6.428e+05	4.428e+04	4.16e-05		78.6	413.40	-671.45	-237.49	-8122.86	4.428e+04	6.428e+05
107	90	1.735e+04	-1.794e+04	1.59e-03	-0.43	0.0	2085.85	-206.64	132.17	-2726.76	-2.833e+04	9001.40
		6328.88	-2.833e+04	-1.56e-04		78.6	2085.85	418.35	132.17	-2719.52	-1.794e+04	1.735e+04
107	111	4.176e+05	5.407e+04	4.38e-03	-0.43	0.0	1224.22	-834.28	-239.77	-9030.55	5.407e+04	4.176e+05
		3.766e+05	3.521e+04	-2.62e-05		78.6	1224.22	-209.08	-239.77	-9020.14	3.521e+04	3.766e+05
107	114	3.112e+05	-8870.03	3.84e-03	-0.43	0.0	1275.04	-661.21	134.45	-1814.00	-1.944e+04	3.112e+05
		2.835e+05	-1.944e+04	-1.23e-04		78.6	1275.04	-44.02	134.45	-1822.24	-8870.03	2.835e+05
107	116	2.267e+05	1.868e+04	3.07e-03	-0.43	0.0	1634.11	-540.48	-83.78	-6620.91	1.868e+04	2.267e+05
		2.084e+05	1.209e+04	-4.32e-05		78.6	1634.11	85.01	-83.78	-6611.32	1.209e+04	2.088e+05
107	117	5.021e+05	1.595e+04	5.15e-03	-0.43	0.0	865.15	-955.01	-21.55	-4223.64	1.595e+04	5.021e+05
		4.513e+05	1.426e+04	-7.09e-05		78.6	865.15	-338.11	-21.55	-4231.06	1.426e+04	4.513e+05
107	119	5.088e+05	3.548e+04	5.14e-03	-0.43	0.0	908.47	-967.65	-125.68	-6470.58	3.548e+04	5.088e+05
		4.572e+05	2.559e+04	-3.04e-05		78.6	908.47	-348.05	-125.68	-6472.12	2.559e+04	4.572e+05
107	122	2.199e+05	751.09	3.08e-03	-0.43	0.0	1590.78	-527.84	20.35	-4373.97	-849.40	2.199e+05
		2.024e+05	-849.40	-9.61e-05		78.6	1590.78	94.96	20.35	-4370.26	751.09	2.029e+05
107	132	5.415e+05	1.930e+04	2.96e-03	-0.47	0.0	2048.84	-625.77	-59.05	-3398.50	1.930e+04	5.415e+05
		5.248e+05	1.466e+04	-1.21e-05		78.6	2048.84	294.62	-59.05	-3402.96	1.466e+04	5.285e+05
107	138	3.231e+05	5088.84	3.78e-03	-0.42	0.0	960.24	-746.81	33.54	-5437.89	2451.34	3.231e+05
		2.862e+05	2451.34	-1.40e-04		78.6	960.24	-193.53	33.54	-5437.75	5088.84	2.862e+05
107	147	4.261e+05	3.503e+04	3.29e-03	-0.44	0.0	1473.50	-706.37	-145.66	-5468.16	3.503e+04	4.261e+05
		3.983e+05	2.358e+04	2.50e-05		78.6	1473.50	-2.30	-145.66	-5463.58	2.358e+04	3.983e+05

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



107	155	2.695e+05	2.406e+04	3.25e-03	-0.42	0.0	535.65	-672.19	-74.83	-6408.10	2.406e+04	2.695e+05
		2.402e+05	1.818e+04	-5.90e-05		78.6	535.65	-75.07	-74.83	-6399.50	1.818e+04	2.402e+05
107	158	5.591e+05	2.167e+04	3.18e-03	-0.46	0.0	1655.71	-690.79	-65.26	-3409.08	2.167e+04	5.591e+05
		5.378e+05	1.654e+04	-2.49e-05		78.6	1655.71	188.79	-65.26	-3413.50	1.654e+04	5.394e+05
107	162	3.223e+05	2.725e+04	3.62e-03	-0.42	0.0	294.62	-762.42	-83.37	-6123.18	2.725e+04	3.223e+05
		2.859e+05	2.070e+04	-7.56e-05		78.6	294.62	-164.36	-83.37	-6115.75	2.070e+04	2.859e+05
107	165	4.028e+05	1.733e+04	3.92e-03	-0.44	0.0	1437.56	-725.87	-52.72	-4983.00	1.733e+04	4.028e+05
		3.725e+05	1.319e+04	-4.59e-05		78.6	1437.56	-45.71	-52.72	-4983.34	1.319e+04	3.725e+05
107	166	3.494e+05	1.920e+04	3.94e-03	-0.43	0.0	1109.16	-735.16	-58.79	-5594.86	1.920e+04	3.494e+05
		3.163e+05	1.458e+04	-5.69e-05		78.6	1109.16	-109.54	-58.79	-5592.19	1.458e+04	3.163e+05
107	167	3.591e+05	1.396e+04	4.08e-03	-0.43	0.0	1219.84	-750.08	-34.20	-5390.88	1.396e+04	3.591e+05
		3.240e+05	1.127e+04	-7.37e-05		78.6	1219.84	-143.34	-34.20	-5390.30	1.127e+04	3.240e+05
107	168	3.605e+05	2.047e+04	4.08e-03	-0.43	0.0	1228.53	-752.93	-70.01	-5616.57	2.047e+04	3.605e+05
		3.252e+05	1.496e+04	-4.62e-05		78.6	1228.53	-145.51	-70.01	-5614.39	1.496e+04	3.252e+05
107	171	3.644e+05	1.731e+04	4.11e-03	-0.43	0.0	1249.63	-747.74	-52.66	-5422.27	1.731e+04	3.644e+05
		3.301e+05	1.317e+04	-5.70e-05		78.6	1249.63	-126.55	-52.66	-5421.19	1.317e+04	3.301e+05
108	12	8.030e+04	-6.840e+04	3.56e-03	-0.59	0.0	-370.16	-4992.39	270.72	2.927e+04	-7.544e+04	8.030e+04
		-3.639e+04	-7.544e+04	3.04e-04		26.0	-370.16	-3984.13	270.72	2.940e+04	-6.840e+04	-3.639e+04
108	21	6.136e+04	-5.594e+04	3.60e-03	-0.55	0.0	-535.49	-4782.44	208.58	2.598e+04	-6.137e+04	6.136e+04
		-5.108e+04	-6.137e+04	3.04e-04		26.0	-535.49	-3867.82	208.58	2.602e+04	-5.594e+04	-5.108e+04
108	35	5.659e+04	-4.298e+04	3.56e-03	-0.55	0.0	-468.89	-4771.11	170.23	2.515e+04	-4.741e+04	5.659e+04
		-5.559e+04	-4.741e+04	2.63e-04		26.0	-468.89	-3858.06	170.23	2.565e+04	-4.298e+04	-5.559e+04
108	42	5.765e+04	-4.678e+04	2.78e-03	-0.45	0.0	-286.37	-3820.03	96.25	2.492e+04	-4.929e+04	5.765e+04
		-3.157e+04	-4.929e+04	2.60e-04		26.0	-286.37	-3043.49	96.25	2.499e+04	-4.678e+04	-3.157e+04
108	61	4.204e+04	-8383.57	2.58e-03	-0.40	0.0	-373.70	-3399.04	-68.67	2.415e+04	-8383.57	4.204e+04
		-3.807e+04	-1.017e+04	2.86e-04		26.0	-373.70	-2764.05	-68.67	2.418e+04	-1.017e+04	-3.807e+04
108	76	2.140e+04	1.243e+04	2.32e-03	-0.41	0.0	-278.94	-3357.61	-216.83	1.911e+04	1.243e+04	2.140e+04
		-5.712e+04	6789.44	6.91e-05		26.0	-278.94	-2682.55	-216.83	1.916e+04	6789.44	-5.712e+04
108	77	6.935e+04	-7.909e+04	2.53e-03	-0.41	0.0	-239.53	-3432.21	486.59	1.861e+04	-9.174e+04	6.935e+04
		-1.129e+04	-9.174e+04	3.08e-04		26.0	-239.53	-2771.65	486.59	1.869e+04	-7.909e+04	-1.129e+04
108	91	4.920e+04	-2.960e+04	2.24e-03	-0.39	0.0	88.33	-3388.49	992.22	1.157e+04	-5.540e+04	4.920e+04
		-3.083e+04	-5.540e+04	-2.90e-05		26.0	88.33	-2768.36	992.22	1.168e+04	-2.960e+04	-3.083e+04
108	94	4.155e+04	-2.392e+04	2.61e-03	-0.43	0.0	-606.80	-3401.33	-722.46	2.615e+04	-2.392e+04	4.155e+04
		-3.758e+04	-4.270e+04	4.06e-04		26.0	-606.80	-2685.84	-722.46	2.616e+04	-4.270e+04	-3.758e+04
108	108	3.594e+04	-1.915e+04	2.38e-03	-0.41	0.0	-268.18	-3379.97	-6.42	1.897e+04	-1.915e+04	3.594e+04
		-4.322e+04	-1.932e+04	1.42e-04		26.0	-268.18	-2709.13	-6.42	1.903e+04	-1.932e+04	-4.322e+04
108	109	5.481e+04	-5.298e+04	2.47e-03	-0.41	0.0	-250.28	-3409.85	276.18	1.875e+04	-6.016e+04	5.481e+04
		-2.520e+04	-6.016e+04	2.35e-04		26.0	-250.28	-2745.07	276.18	1.881e+04	-5.298e+04	-2.520e+04
108	123	4.703e+04	-3.367e+04	2.35e-03	-0.40	0.0	-118.10	-3392.75	484.24	1.590e+04	-4.626e+04	4.703e+04
		-3.275e+04	-4.626e+04	1.01e-04		26.0	-118.10	-2744.32	484.24	1.598e+04	-3.367e+04	-3.275e+04
108	126	4.372e+04	-3.306e+04	2.50e-03	-0.42	0.0	-400.37	-3397.07	-214.48	2.182e+04	-3.306e+04	4.372e+04
		-3.566e+04	-3.864e+04	2.77e-04		26.0	-400.37	-2709.88	-214.48	2.187e+04	-3.864e+04	-3.566e+04
108	137	5.789e+04	-4.973e+04	2.61e-03	-0.44	0.0	-276.33	-3673.09	195.72	2.191e+04	-5.482e+04	5.789e+04
		-2.795e+04	-5.482e+04	2.24e-04		26.0	-276.33	-2930.90	195.72	2.200e+04	-4.973e+04	-2.795e+04
108	141	4.527e+04	-4.142e+04	2.64e-03	-0.41	0.0	-386.55	-3533.12	154.30	1.972e+04	-4.543e+04	4.527e+04
		-3.775e+04	-4.543e+04	2.25e-04		26.0	-386.55	-2853.36	154.30	1.975e+04	-4.142e+04	-3.775e+04
108	148	4.209e+04	-3.278e+04	2.61e-03	-0.41	0.0	-342.15	-3525.57	128.73	1.947e+04	-3.613e+04	4.209e+04
		-4.075e+04	-3.613e+04	1.98e-04		26.0	-342.15	-2846.85	128.73	1.950e+04	-3.278e+04	-4.075e+04
108	151	5.543e+04	-4.288e+04	2.60e-03	-0.44	0.0	-225.19	-3667.87	110.08	2.224e+04	-4.575e+04	5.543e+04
		-3.026e+04	-4.575e+04	2.21e-04		26.0	-225.19	-2924.07	110.08	2.232e+04	-4.288e+04	-3.026e+04
108	160	4.503e+04	-1.848e+04	2.47e-03	-0.40	0.0	-283.41	-3387.21	0.13	2.173e+04	-1.848e+04	4.503e+04
		-3.459e+04	-1.848e+04	2.38e-04		26.0	-283.41	-2737.77	0.13	2.178e+04	-1.848e+04	-3.459e+04
108	165	4.786e+04	-3.804e+04	2.45e-03	-0.42	0.0	-249.43	-3448.25	143.55	1.947e+04	-4.177e+04	4.786e+04
		-3.290e+04	-4.177e+04	1.92e-04		26.0	-249.43	-2764.63	143.55	1.954e+04	-3.804e+04	-3.290e+04
108	166	4.531e+04	-3.653e+04	2.48e-03	-0.41	0.0	-279.64	-3437.15	135.52	1.914e+04	-4.005e+04	4.531e+04
		-3.530e+04	-4.005e+04	1.95e-04		26.0	-279.64	-2763.80	135.52	1.920e+04	-3.653e+04	-3.530e+04
108	170	4.532e+04	-3.254e+04	2.42e-03	-0.41	0.0	-259.99	-3384.92	107.80	1.938e+04	-3.534e+04	4.532e+04
		-3.406e+04	-3.534e+04	1.97e-04		26.0	-259.99	-2721.89	107.80	1.944e+04	-3.254e+04	-3.406e+04
108	171	4.538e+04	-3.615e+04	2.42e-03	-0.41	0.0	-259.23	-3394.91	134.88	1.886e+04	-3.966e+04	4.538e+04
		-3.421e+04	-3.966e+04	1.89e-04		26.0	-259.23	-2727.10	134.88	1.892e+04	-3.615e+04	-3.421e+04
109	2	9.817e+05	3.094e+04	9.27e-03	-0.62	0.0	689.28	-5181.01	94.16	1.391e+04	-3.592e+04	9.817e+05
		-4.157e+05	-3.592e+04	3.97e-04		710.0	689.28	6928.31	94.16	1.410e+04	3.094e+04	-4.157e+05
109	12	9.490e+05	3.022e+04	9.62e-03	-0.61	0.0	740.44	-4867.96	96.52	1.381e+04	-3.832e+04	9.490e+05
		-4.176e+05	-3.832e+04	4.29e-04		710.0	740.44	6699.43	96.52	1.397e+04	3.022e+04	-4.176e+05
109	51	2.304e+05	9747.69	0.03	-0.42	0.0	-1907.33	-2869.22	27.71	5944.93	-9923.46	2.304e+05
		-4.187e+05	-9923.46	5.11e-04		710.0	-1907.33	3321.07	27.71	5464.99	9747.69	-4.187e+05
109	54	9.805e+05	3.296e+04	9.86e-03	-0.61	0.0	712.39	-4716.51	102.32	1.593e+04	-3.969e+04	9.805e+05
		-4.447e+05	-3.969e+04	5.88e-04		710.0	712.39	6840.82	102.32	1.605e+04	3.296e+04	-4.447e+05
109	66	5.166e+05	1.846e+04	0.01	-0.45	0.0	-1018.61	-3061.46	57.08	1.176e+04	-2.206e+04	-1.082e+05
		-5.234e+05	-2.206e+04	8.94e-04		710.0	-1018.61	4784.00	57.08	1.141e+04	1.846e+04	-5.234e+05
109	85	7.169e+05	4.975e+04	0.03	-0.43	0.0	2866.60	-1224.57	181.60	2.730e+04	-7.918e+04	7.169e+05
		-7.133e+05	-7.918e+04	2.33e-03		710.0	2866.60	4941.31	181.60	2.712e+04	4.975e+04	-7.133e+05
109	92	1.214e+06	1.823e+04	-0.01	-0.44	0.0	-2788.30	-4965.52	-23.23	-1.492e+04	1.823e+04	1.214e+06
		-6.696e+04	1734.56	-1.61e-03		710.0	-2788.30	1795.31	-23.23	-1.482e+04	1734.56	-6.696e+04
109	93	7.281e+05	3.131e+04	0.03	-0.43	0.0	3148.34	-1084.65	126.85	3.007e+04	-5.875e+04	7.281e+05
		-7.682e+05	-5.875e+04	2.26e-03		710.0	3148.34	5027.51	126.85	2.987e+04	3.131e+04	-7.682e+05

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



109	117	5.384e+05	3.001e+04	0.02	-0.43	0.0	1272.40	-2293.15	104.39	1.562e+04	-4.410e+04	-1.062e+05
		-3.896e+05	-4.410e+04	1.16e-03		710.0	1272.40	4033.14	104.39	1.552e+04	3.001e+04	5.384e+05
109	123	5.270e+05	2.118e+04	0.03	-0.43	0.0	1349.61	-2269.12	71.02	1.777e+04	-2.924e+04	-1.300e+05
		-4.067e+05	-2.924e+04	1.92e-03		710.0	1349.61	4030.67	71.02	1.759e+04	2.118e+04	5.270e+05
109	124	6.448e+05	1.053e+04	0.02	-0.43	0.0	-1027.00	-3813.96	21.51	-1602.43	-4737.34	6.448e+05
		-1.275e+05	-4737.34	-5.38e-04		710.0	-1027.00	2754.60	21.51	-1582.44	1.053e+04	2.900e+05
109	125	5.429e+05	2.251e+04	0.03	-0.43	0.0	1387.04	-2236.21	82.11	1.675e+04	-3.579e+04	-1.360e+05
		-4.047e+05	-3.579e+04	1.13e-03		710.0	1387.04	4068.21	82.11	1.664e+04	2.251e+04	5.429e+05
109	132	6.999e+05	2.206e+04	6.30e-03	-0.46	0.0	473.27	-3767.84	67.20	9965.39	-2.565e+04	2.743e+05
		-3.018e+05	-2.565e+04	2.86e-04		710.0	473.27	4983.15	67.20	1.010e+04	2.206e+04	6.999e+05
109	137	6.781e+05	2.158e+04	6.52e-03	-0.46	0.0	507.38	-3559.14	68.78	9894.83	-2.725e+04	2.328e+05
		-3.031e+05	-2.725e+04	3.08e-04		710.0	507.38	4830.56	68.78	1.002e+04	2.158e+04	6.781e+05
109	155	3.310e+05	1.369e+04	0.03	-0.43	0.0	-778.69	-2987.55	41.40	6552.41	-1.570e+04	1.827e+05
		-3.018e+05	-1.570e+04	3.64e-04		710.0	-778.69	3318.16	41.40	6320.80	1.369e+04	3.310e+05
109	158	6.990e+05	2.341e+04	6.73e-03	-0.46	0.0	488.67	-3458.17	72.65	1.131e+04	-2.817e+04	1.831e+05
		-3.211e+05	-2.817e+04	4.12e-04		710.0	488.67	4924.82	72.65	1.140e+04	2.341e+04	6.990e+05
109	163	5.218e+05	1.950e+04	0.01	-0.45	0.0	-186.21	-3115.71	60.98	1.043e+04	-2.380e+04	8.844e+04
		-3.668e+05	-2.380e+04	6.19e-04		710.0	-186.21	4293.45	60.98	1.028e+04	1.950e+04	5.218e+05
109	165	4.752e+05	1.769e+04	0.02	-0.44	0.0	268.85	-3171.98	55.11	8032.15	-2.144e+04	2.632e+05
		-2.447e+05	-2.144e+04	2.97e-04		710.0	268.85	3716.93	55.11	8034.03	1.769e+04	4.752e+05
109	166	4.063e+05	1.619e+04	0.02	-0.43	0.0	29.09	-3033.35	50.67	7662.09	-1.978e+04	2.302e+05
		-2.585e+05	-1.978e+04	3.67e-04		710.0	29.09	3455.55	50.67	7576.62	1.619e+04	4.063e+05
109	171	4.164e+05	1.652e+04	0.02	-0.43	0.0	180.02	-3025.08	51.81	7571.49	-2.026e+04	2.544e+05
		-2.360e+05	-2.026e+04	3.28e-04		710.0	180.02	3411.41	51.81	7529.21	1.652e+04	4.164e+05
110	2	1.281e+04	6536.54	6.92e-03	-0.64	0.0	227.18	-436.75	20.17	-1.262e+04	5077.84	-4563.22
		-9640.10	5077.84	-3.62e-04		72.3	227.18	914.77	20.17	-1.254e+04	6536.54	1.281e+04
110	32	1229.20	7602.56	0.01	-0.61	0.0	69.60	-785.77	-66.19	-6155.93	7602.56	1229.20
		-1.811e+04	2815.84	-2.18e-04		72.3	69.60	362.24	-66.19	-6086.89	2815.84	-1.395e+04
110	47	3.483e+04	-1.817e+04	9.21e-03	-0.44	0.0	-326.68	-809.38	62.83	-4533.04	-2.271e+04	3.483e+04
		3867.40	-2.271e+04	-2.25e-05		72.3	-326.68	-50.14	62.83	-4479.18	-1.817e+04	3867.40
110	51	3.025e+04	-1.963e+04	0.01	-0.45	0.0	-305.78	-1013.51	76.14	-4199.35	-2.513e+04	3.025e+04
		-1.048e+04	-2.513e+04	-8.40e-05		72.3	-305.78	-117.90	76.14	-4142.35	-1.963e+04	-1.048e+04
110	59	-1.034e+04	3095.85	0.01	-0.60	0.0	-40.03	-1033.32	0.88	-1651.95	3032.43	-1.034e+04
		-4.675e+04	3032.43	-1.51e-04		72.3	-40.03	21.05	0.88	-1596.29	3095.85	-4.675e+04
110	72	1.243e+04	3.341e+04	2.22e-03	-0.44	0.0	0.71	-547.88	-361.57	-5080.27	3.341e+04	1.243e+04
		-2719.25	7257.38	-6.18e-05		72.3	0.71	167.17	-361.57	-5024.84	7257.38	-1308.33
110	73	-1.145e+04	-1226.17	0.01	-0.46	0.0	137.12	-534.18	363.24	-3807.86	-2.749e+04	-1.145e+04
		-2.325e+04	-2.749e+04	-2.46e-04		72.3	137.12	332.51	363.24	-3765.94	-1226.17	-1.859e+04
110	83	-2.273e+04	660.38	0.02	-0.48	0.0	-410.03	-1287.83	-94.76	6014.80	660.38	-2.273e+04
		-7.808e+04	-6192.26	2.48e-04		72.3	-410.03	-251.45	-94.76	6036.53	-6192.26	-7.808e+04
110	86	5.818e+04	1.222e+04	0.01	-0.41	0.0	547.87	205.77	96.43	-1.490e+04	5249.96	2.371e+04
		2.371e+04	5249.96	-5.56e-04		72.3	547.87	751.13	96.43	-1.483e+04	1.222e+04	5.818e+04
110	104	5266.70	1.493e+04	4.95e-03	-0.44	0.0	44.08	-540.55	-141.14	-4782.11	1.493e+04	5266.70
		-8569.27	4726.76	-1.19e-04		72.3	44.08	219.49	-141.14	-4730.53	4726.76	-6277.71
110	105	-4287.12	1304.45	8.72e-03	-0.45	0.0	93.76	-541.51	142.81	-4106.02	-9023.51	-4287.12
		-1.708e+04	-9023.51	-1.89e-04		72.3	93.76	280.19	142.81	-4060.25	1304.45	-1.362e+04
110	115	-8980.32	1898.05	0.01	-0.46	0.0	-125.09	-844.02	-36.42	-212.15	1898.05	-8980.32
		-3.772e+04	-735.48	9.03e-06		72.3	-125.09	46.75	-36.42	-174.39	-735.48	-3.763e+04
110	118	1.773e+04	6766.69	1.34e-04	-0.43	0.0	262.93	-238.04	38.09	-8675.98	4012.28	9959.90
		7017.39	4012.28	-3.17e-04		72.3	262.93	452.93	38.09	-8616.39	6766.69	1.773e+04
110	132	8761.74	4320.78	5.23e-03	-0.47	0.0	162.25	-332.41	15.96	-8907.70	3166.67	-2855.83
		-6876.76	3166.67	-2.62e-04		72.3	162.25	651.81	15.96	-8847.55	4320.78	8761.74
110	147	1005.79	4849.81	7.44e-03	-0.46	0.0	57.20	-565.09	-41.62	-4597.76	4849.81	1005.79
		-1.251e+04	1840.31	-1.66e-04		72.3	57.20	283.47	-41.62	-4546.16	1840.31	-9080.14
110	153	1.951e+04	-6674.19	6.46e-03	-0.44	0.0	-139.31	-614.54	24.62	-4700.76	-8454.50	1.951e+04
		1029.92	-8454.50	-6.26e-05		72.3	-139.31	120.88	24.62	-4650.09	-6674.19	1741.91
110	155	1.646e+04	-7646.58	9.34e-03	-0.45	0.0	-125.37	-750.63	33.50	-4478.30	-1.007e+04	1.646e+04
		-8052.36	-1.007e+04	-1.04e-04		72.3	-125.37	75.71	33.50	-4425.54	-7646.58	-7825.53
110	160	-6704.72	2026.98	0.01	-0.45	0.0	-15.89	-730.12	3.10	-1595.11	1803.06	-6704.72
		-3.109e+04	1803.06	-1.21e-04		72.3	-15.89	56.00	3.10	-1552.43	2026.98	-3.095e+04
110	165	-447.34	3561.83	6.36e-03	-0.45	0.0	91.66	-489.57	2.78	-5343.84	3360.89	-447.34
		-1.087e+04	3360.89	-1.75e-04		72.3	91.66	335.93	2.78	-5293.04	3561.83	-5919.91
110	169	4025.32	1362.84	6.60e-03	-0.45	0.0	31.35	-546.00	4.51	-4502.45	1036.66	4025.32
		-9796.58	1036.66	-1.35e-04		72.3	31.35	229.74	4.51	-4453.55	1362.84	-7323.87
110	170	-1217.12	3103.07	7.34e-03	-0.45	0.0	56.04	-569.11	0.21	-3881.32	3088.17	-1217.12
		-1.602e+04	3088.17	-1.47e-04		72.3	56.04	216.76	0.21	-3834.02	3103.07	-1.386e+04
110	171	489.79	3015.60	6.84e-03	-0.45	0.0	68.92	-541.03	0.84	-4444.06	2955.17	489.79
		-1.282e+04	2955.17	-1.54e-04		72.3	68.92	249.84	0.84	-4395.39	3015.60	-9949.93
111		-2.5939e+04	-1.796e+04	3.14e-03	-0.63	0.0	-554.17	-1197.68	95.69	9952.08	-2.245e+04	-5.939e+04
		-9.269e+04	-2.245e+04	1.62e-04		47.0	-554.17	-218.72	95.69	1.004e+04	-1.796e+04	-9.269e+04
111		-12.6009e+04	-1.828e+04	3.51e-03	-0.62	0.0	-584.22	-1180.43	98.98	9926.20	-2.294e+04	-6.009e+04
		-9.337e+04	-2.294e+04	1.65e-04		47.0	-584.22	-234.72	98.98	1.001e+04	-1.828e+04	-9.337e+04
111		-33.4406e+04	-2.624e+04	3.82e-03	-0.42	0.0	-1380.49	-333.09	125.75	6956.87	-3.215e+04	-4.406e+04
		-4.916e+04	-3.215e+04	2.14e-04		47.0	-1380.49	178.88	125.75	7052.66	-2.624e+04	-4.770e+04

...

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



566	171	-1.228e+05	-2.439e+04	-1.86e-03	-0.42	590.0	-81.14	-2646.09	74.65	-1.074e+04	1.965e+04	-1.228e+05
Trave f.	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt			N	V 2	V 3	T		
	-1.031e+06	-2.491e+05	-0.09	-0.69			-6300.51	-1.075e+04	-3978.48	-8.537e+05		
	1.467e+06	2.821e+05	0.08	-0.37			4120.34	1.063e+04	3478.40	1.289e+06		

13. VERIFICHE ELEMENTI TRAVE E/O PILASTRO IN C.A.

LEGENDA TABELLA VERIFICHE ELEMENTI TRAVE E/O PILASTRO IN C.A.

In tabella vengono riportati per ogni elemento il numero identificativo ed il codice di verifica con le sigle **Ok** o **NV**.

Nel caso in cui si sia proceduto alla progettazione con il metodo degli stati limite (**S.L.**) vengono riportati: il rapporto x/d , le verifiche per sollecitazioni proporzionali e la verifica per compressione media con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

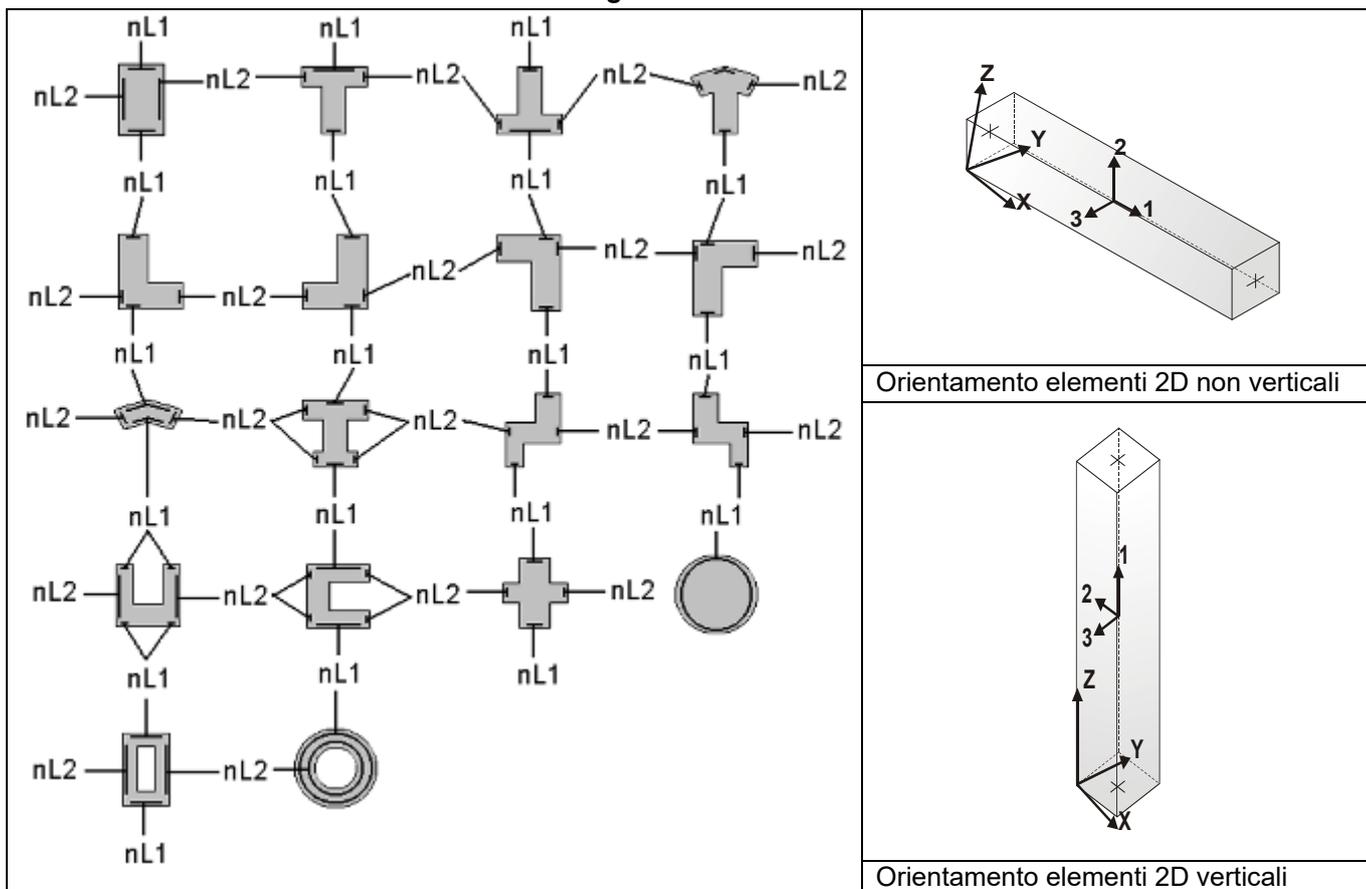
Nel caso in cui si sia proceduto alla progettazione con le tensioni ammissibili (**T.A.**) vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima compressione media nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale) con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Nel caso in cui la struttura abbia comportamento dissipativo e sia prevista la progettazione con il criterio della gerarchia delle resistenze (**G.R.**) vengono riportate le verifiche di sovraresistenza e del nodo.

Per gli elementi tipo pilastro sono riportati numero e diametro dei ferri di vertice, numero e diametro di ferri disposti lungo i lati L1 (paralleli alla base della sezione) e lungo i lati L2 (paralleli all'altezza della sezione).

Per gli elementi tipo trave sono riportati infine le quantità di armatura inferiore e superiore.

Schema della distribuzione delle armature longitudinali



PROGETTAZIONE DELLE FONDAZIONI

Il D.M.17/01/2018 - par: 7.2.5 prevede:

"Sia per CD"A" sia per CD"B" il dimensionamento delle strutture di fondazione e la verifica di sicurezza del complesso fondazione-terreno devono essere eseguiti assumendo come azione in fondazione, trasmessa dagli elementi soprastanti, una tra le seguenti:

- quella derivante dall'analisi strutturale eseguita ipotizzando comportamento strutturale non dissipativo;
- [...];
- quella trasferita dagli elementi soprastanti nell'ipotesi di comportamento strutturale dissipativo, amplificata di un coefficiente pari a 1,30 in CD"A" e 1,10 in CD"B";

Nel contesto visualizzazione risultati e nella stampa della relazione sulle fondazioni PRO_SAP mostra le sollecitazioni che derivano dall'analisi non incrementate sia in termini di pressioni sul terreno che in termini di sollecitazioni.

La progettazione degli elementi strutturali con proprietà fondazione è effettuata da PRO_SAP (per travi e platee) o da PRO_CAD Plinti (per plinti e pali di fondazione) incrementando le sollecitazioni delle combinazioni con sisma di un coefficiente pari 1.1 in CDB e 1.3 in CDA per pali, plinti, travi e platee.

Per i bicchieri dei plinti di fondazione prefabbricati l'incremento delle sollecitazioni ha un fattore pari a 1.2 in CDB e 1.35 in CDA.

N.B.: nel caso di comportamento strutturale non dissipativo la progettazione viene effettuata senza nessun incremento.

Le verifiche geotecniche vengono effettuate dal modulo geotecnico incrementando automaticamente le sollecitazioni del fattore 1.1 in CDB e 1.3 in CDA per pali, plinti, travi e platee.

N.B.: nel caso di comportamento strutturale non dissipativo le verifiche geotecniche vengono effettuate senza nessun incremento.

Simbologia adottata nelle tabelle di verifica

Per le verifiche agli S.L. dei pilastri è presente una tabella con i simboli di seguito descritti:

M_P X Y	Numero della pilastrata (P) e posizione in pianta (X,Y)
Pilas.	numero identificativo dell'elemento D2
Note	Codici identificativi delle sezione (s) e materiale (m) pilastro
Stato	Codici relativi all'esito delle verifiche effettuate appresso descritte
Quota	Quota sezione di verifica
%Af	Percentuale di area di armatura rispetto a quella di calcestruzzo
r. snell.	Rapporto di snellezza λ su λ^* : valore superiore a 1 per elementi snelli nel caso in cui viene effettuata la verifica con il metodo diretto dello stato di equilibrio
Armat. long.	Numero e diametro (d) dei ferri di armatura longitudinale distinti in ferri di vertice + ferri di lato nelle posizioni nL1 e nL2, come da schemi in figura precedente
V N/M	Verifica a pressoflessione con rapporto Ed/Rd: valore minore o uguale a 1 per verifica positiva
V N sis	Verifica a compressione solo calcestruzzo con rapporto Nsd/Nrd ed Nrd calcolato come al punto 7.4.4.2.1: valore minore o uguale a 1 per verifica positiva
Staffe	Dati tratto di staffatura oggetto di verifica, nello specifico: numero delle braccia, diametro, passo, lunghezza L tratto
V V/T cls	Verifica a taglio/torsione con rapporto Ved/Vrd: valore minore o uguale a 1 per verifica positiva
Rif. cmb.	Riferimento combinazioni da cui si generano le verifiche più gravose per il pilastro

Per le verifiche alla G.R. dei pilastri è presente una tabella con i simboli di seguito descritti:

Pilas.	numero identificativo dell'elemento D2 pilastro
sovr. Xi (Xf)	Verifica sovreresistenza come da formula 7.4.4 in direzione X, alla base (i) ed alla sommità (f):



	rapporto tra i momenti resistenti dei pilastri e delle travi. La verifica è positiva se maggiore del γ_{Rd} adottato
sovr. Y_i (Y_f)	Verifica sovreresistenza come da formula 7.4.4 in direzione Y, alla base (i) ed alla sommità (f): rapporto tra i momenti resistenti dei pilastri e delle travi. La verifica è positiva se maggiore del γ_{Rd} adottato
M 2-2 i (f)	Valore del momento resistente 2-2 alla base (i) ed alla sommità (f) con massimo momento in presenza dello sforzo normale di calcolo
M 3-3 i (f)	Valore del momento resistente 3-3 alla base (i) ed alla sommità (f) con massimo momento in presenza dello sforzo normale di calcolo
Luce per V	Luce di calcolo per la definizione del taglio (generato dai momenti resistenti)
V M2-2 (M3-3)	Valore del taglio generato dai momenti resistenti 2-2 (3-3)

Per le verifiche dei dettagli costruttivi per la duttilità è presente una tabella con i simboli di seguito descritti:
 (Non presente nel caso di comportamento strutturale non dissipativo)

Pilas	Numero identificativo D2 pilastro
ni	Sforzo assiale adimensionalizzato di progetto relativo alla combinazione sismica SLV
alfaomega	Prodotto tra il coefficiente di efficacia del confinamento e il rapporto meccanico dell'armatura trasversale di confinamento all'interno del nodo
V.7.4.29 2-2 (3-3)	Rapporto tra la domanda di staffe minima nel nodo e il rapporto meccanico dell'armatura trasversale di confinamento inserito all'interno del nodo in direzione 2 (3)
V. 7.4.29 Stato	Codici relativi all'esito della verifica 7.4.29
d μ_{fi} 2-2 (3-3)	Domanda in duttilità di curvatura in direzione 2 (3)
c μ_{fi} 2-2 (3-3)	Capacità in duttilità di curvatura in direzione 2 (3)
V. dutt. 2-2 (3-3)	Rapporto tra la domanda in duttilità di curvatura e la capacità in duttilità di curvatura in direzione 2 (3)

Per le verifiche nodi trave-pilastro di elementi nuovi è presente una tabella con i simboli di seguito descritti:

Nodo	Numero identificativo del nodo trave-pilastro
Stato	Esito delle verifiche
Pilastro	Numero identificativo D2 pilastro
Diam st	Diametro staffe nodo
Passo	Passo staffe nodo
n. br. 2 (3)	Numero braccia staffe per il taglio in direzione 2 (3)
Bj2 (3)	Larghezza effettiva del nodo per il taglio in direzione 2 (3)
Hjc2 (3)	Distanza tra le giaciture più esterne delle armature del pilastro per il taglio in direzione 2 (3)
V. 7.4.8	Rapporto tra il taglio V_{jbd} e il taglio resistente come da formula 7.4.8
V. Ash	Rapporto tra il passo staffe calcolato secondo il capitolo 7.4.4.3.1. e il passo staffe effettivamente inserita nel nodo. Nel caso di valore indica passo staffe utilizzato deriva dalle formule presenti nel paragrafo 7.4.4.3.1. Nel caso di valore minore di 1 il passo staffe utilizzato deriva del pilastro superiore o inferiore al nodo
7.4.10	Check passo staffe valutato in funzione della formula 7.4.10: <ul style="list-style-type: none"> • SI il passo staffe è calcolato utilizzando la formula 7.4.10; • NO il passo staffe è calcolato utilizzando le formule 7.4.11 e/o 7.4.12; • NR calcolo passo staffe non richiesto;
Rif. comb.	Riferimento combinazioni da cui si generano le verifiche più gravose per il nodo

Per le verifiche nodi trave-pilastro di elementi esistenti è presente una tabella con i simboli di seguito descritti:

Pilastro I	Numero identificativo D2 del pilastro inferiore.
Pilastro S	Numero identificativo D2 del pilastro superiore.
Nodo	Numero identificativo del nodo trave-pilastro.
SL cod	Stato limite di riferimento e relativo esito delle verifiche.
ver. (+)	Fattore di sicurezza nei riguardi della verifica di resistenza a compressione (verificato se < 1.00).
V +	Azione di Taglio presente al di sopra del nodo nella verifica di resistenza a compressione.
V + af s	Sollecitazione di trazione presente nell' armatura longitudinale superiore della trave nella verifica di resistenza a compressione.
N +	Azione Assiale presente al di sopra del nodo nella verifica di resistenza a compressione.
ver. (-)	Fattore di sicurezza nei riguardi della verifica di resistenza a trazione (verificato se < 1.00).
V -	Azione di Taglio presente al di sopra del nodo nella verifica di resistenza a trazione.
V - af s	Sollecitazione di trazione presente nell' armatura longitudinale superiore della trave nella verifica di resistenza a trazione.
N -	Azione Assiale presente al di sopra del nodo nella verifica di resistenza a trazione.
AreaV2	Area resistente del nodo in direzione 2 ($A_{j2}=b_{j2}*h_{jc2}$).
AreaV3	Area resistente del nodo in direzione 3 ($A_{j3}=b_{j3}*h_{jc3}$).
Rif. comb.	Combinazione (direzione) di riferimento nella verifica di trazione.

Per le verifiche agli S.L. delle travi è presente una tabella con i simboli di seguito descritti:

M_T Z P P	Numero della travata (T), quota media (Z), n° pilastrata iniziale (P) e finale (P) (nodo in assenza di pilastrata)
Trave	numero identificativo dell'elemento D2
Note	Codici identificativi sezione (s) e materiale (m) trave; sono inoltre presenti le sigle relative all'esito delle verifiche effettuate appresso descritte
%Af	Percentuale di area di armatura rispetto a quella di calcestruzzo
Af inf.	Area di armatura longitudinale posta all'intradosso
Af sup	Area di armatura longitudinale posta all'estradosso
Af long.	Area complessiva armatura longitudinale
x/d	rapporto tra posizione dell'asse neutro e altezza utile
V N/M	Verifica a pressoflessione rapporto E_d/R_d : valore minore o uguale a 1 per verifica positiva
Staffe	Dati tratto di staffatura oggetto di verifica, nello specifico: numero delle braccia, diametro, passo, lunghezza L tratto
V V/T cls	Verifica a taglio/torsione con rapporto V_{ed}/V_{rd} : valore minore o uguale a 1 per verifica positiva
Rif. cmb.	Riferimento combinazioni da cui si generano le verifiche più gravose per la trave

Per le verifiche alla G.R. delle travi è presente una tabella con i simboli di seguito descritti:

Trave	numero identificativo dell'elemento D2 trave
M negativo i (f)	Valore del momento resistente negativo all' estremità iniziale i (finale f) della trave
M positivo i (f)	Valore del momento resistente positivo all' estremità iniziale i (finale f) della trave
Luce per V	Luce di calcolo per la definizione del taglio (generato dai momenti resistenti)
V M-i M+f	Taglio generato dai momenti resistenti negativo i e positivo f
V M+i M-f	Taglio generato dai momenti resistenti positivo i e negativo f
VEd, min	Valore di taglio minimo per verifica condizioni p.to 7.4.4.1.1 armatura diagonale (solo per CD "A")
VEd, max	Valore di taglio massimo per verifica condizioni p.to 7.4.4.1.1 armatura diagonale (solo per CD "A")
Vr1	Valore di taglio come da formula 7.4.1 per armatura diagonale (solo per CD "A")
As	Area singolo ordine armature diagonali come da formula 7.4.2 (solo per CD "A")

Per le verifiche a taglio ciclico di travi e pilastri esistenti è presente una tabella con i simboli di seguito descritti:

Trave/Pilastro	Numero identificativo dell'elemento D2 trave/pilastro
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V. SLV	Codice relativo all'esito delle verifiche
Nodo	Numero identificativo del nodo di verifica
Ver. VC	Fattore di sicurezza nei confronti della verifica a taglio ciclico (verificato se < 1.00)
Direz.	Direzione di verifica
N fr	Valore di sforzo normale calcolato con fattore di comportamento fragile
V fr	Valore di taglio calcolato con fattore di comportamento fragile
M fr	Valore di momento calcolato con fattore di comportamento fragile
N dutt	Valore di sforzo normale calcolato con fattore di comportamento duttile
LV	Lunghezza di taglio
Mud,pl	Parte plastica della domanda di duttilità
V cic	Resistenza a taglio in condizioni cicliche (C8.7.2.8)
Cmb	Riferimento combinazioni da cui si generano le verifiche più gravose

Per le verifiche alle T.A. di pilastri e travi è presente una tabella con i simboli di seguito descritti:

M_P X Y	Numero della pilastrata (P) e posizione in pianta (X,Y)
M_T Z P P	Numero della travata, quota media pilastrata iniziale e finale (nodo in assenza di pilastrata)
Pilas. o Trave	numero identificativo dell'elemento D2
Note	Viene riportato il codice relativo alla sezione(s) e relativo al materiale(m); nella terza riga viene riportato il valore delle snellezze in direzione 2-2 e 3-3
Stato	Codici di verifica relativi alle tensioni normali e alle tensioni tangenziali
Quota	Ascissa del punto di verifica
%Af	Percentuale di area di armatura rispetto a quella di calcestruzzo
Armat. long.	Numero e diametro dei ferri di armatura longitudinale: ferri di vertice + ferri di lato (come da fig. precedente)
Af inf.	Area di armatura longitudinale posta all'intradosso della trave
Af sup	Area di armatura longitudinale posta all'estradosso della trave
Sc max	Massima tensione di compressione del calcestruzzo
Sc med	Massima tensione media di compressione del calcestruzzo
Sf max	Tensione massima nell'acciaio
staffe	Vengono riportati i dati del tratto di staffatura in cui cade la sezione di verifica; in particolare: numero dei bracci, diametro, passo, lunghezza tratto
Tau max	Tensione massima tangenziale nel cls
Rif. comb	Combinazioni in cui si generano i seguenti valori di tensione: Sc max, Sc med, Sf max, Tau max
AfV	area dell'armatura atta ad assorbire le azioni di taglio
AfT	area dell'armatura atta ad assorbire le azioni di torsione
Scorr. P	Scorrimento dei piegati
Af long.	Area del ferro longitudinale aggiuntivo per assorbire la torsione

Trave	Note	Pos. cm	%Af	Af inf.	Af. sup	Af long.	M_T= 10 x/d	Z=0.0 V N/M	P=2 V V/T cls	P=11 V V/T acc	Staffe Rif. cmb L=cm
105	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.07	0.08	2d8/15 L=58 45,21,63
	s=5,m=3	58.4	0.21	12.6	12.6	0.0	0.05	0.03	0.04	0.04	2d8/15 L=58 63,21,63
146	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.06	0.07	2d8/15 L=45 63,21,63
	s=5,m=3	58.4	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.04	2d8/20 L=13 63,21,63
175	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.05	0.08	2d8/20 L=58 63,21,64
	s=5,m=3	58.4	0.21	12.6	12.6	0.0	0.05	0.09	0.02	0.02	2d8/20 L=58 63,21,63
202	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.05	0.07	2d8/20 L=58 63,50,64
	s=5,m=3	58.4	0.21	12.6	12.6	0.0	0.05	0.11	0.02	0.02	2d8/20 L=58 63,49,65
227	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.11	0.05	0.06	2d8/20 L=95 91,50,64

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



	s=5,m=3	95.0	0.21	12.6	12.6	0.0	0.05	0.12	0.03	0.03	2d8/20 L=95	63,2,2
252	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.12	0.03	0.03	2d8/20 L=74	97,64,64
	s=5,m=3	74.3	0.21	12.6	12.6	0.0	0.05	0.13	0.04	0.04	2d8/20 L=74	97,90,2
275	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.13	0.02	0.03	2d8/20 L=45	93,90,93
	s=5,m=3	74.3	0.21	12.6	12.6	0.0	0.05	0.13	0.05	0.06	2d8/20 L=74	97,90,92
298	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.14	0.03	0.03	2d8/20 L=74	97,90,92
	s=5,m=3	74.3	0.21	12.6	12.6	0.0	0.05	0.14	0.06	0.07	2d8/20 L=74	93,90,92
320	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.15	0.04	0.04	2d8/20 L=74	93,90,92
	s=5,m=3	74.3	0.21	12.6	12.6	0.0	0.05	0.15	0.06	0.07	2d8/15 L=29	93,90,92
342	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.16	0.05	0.05	2d8/15 L=74	93,92,92
	s=5,m=3	74.3	0.21	12.6	12.6	0.0	0.07	0.15	0.08	0.08	2d8/15 L=74	93,92,92
109	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.23	0.07	0.09	2d8/15 L=103	92,2,2
	s=5,m=3	355.0	0.21	12.6	12.6	0.0	0.05	0.13	0.04	0.04	2d8/20 L=503	91,93,93
		710.0	0.21	12.6	12.6	0.0	0.07	0.20	0.09	0.11	2d8/15 L=103	2,2,2
136	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.02	0.01	2d8/15 L=72	93,26,2
	s=5,m=3	72.1	0.21	12.6	12.6	0.0	0.07	0.09	0.02	8.58e-03	2d8/15 L=72	93,76,84
168	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.03	0.02	2d8/15 L=31	54,2,2
	s=5,m=3	257.5	0.21	12.6	12.6	0.0	0.07	0.15	0.05	0.06	2d8/20 L=226	93,2,2
195	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.13	0.02	8.82e-03	2d8/20 L=58	93,31,68
	s=5,m=3	83.0	0.21	12.6	12.6	0.0	0.07	0.14	0.03	0.02	2d8/15 L=25	93,26,2
220	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.14	0.02	0.01	2d8/15 L=78	93,54,4
	s=5,m=3	78.0	0.21	12.6	12.6	0.0	0.07	0.14	0.03	0.02	2d8/15 L=78	93,31,92
245	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.14	0.07	0.04	2d8/15 L=73	2,2,2
	s=5,m=3	73.0	0.21	12.6	12.6	0.0	0.07	0.11	0.06	0.03	2d8/15 L=73	2,2,59
269	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.08	0.05	2d8/15 L=30	2,2,2
	s=5,m=3	105.0	0.21	12.6	12.6	0.0	0.07	0.07	0.06	0.03	2d8/20 L=75	93,2,46
292	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.07	0.05	2d8/20 L=62	93,2,2
	s=5,m=3	62.1	0.21	12.6	12.6	0.0	0.07	0.05	0.06	0.04	2d8/20 L=62	93,2,54
314	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.08	0.06	2d8/20 L=31	93,2,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.07	0.05	0.07	0.03	2d8/15 L=36	51,2,54
336	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.08	0.06	2d8/15 L=67	51,2,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.05	0.07	0.07	0.04	2d8/15 L=67	49,2,2
354	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.05	0.03	2d8/15 L=45	49,21,63
	s=5,m=3	44.9	0.21	12.6	12.6	0.0	0.05	0.06	0.06	0.04	2d8/15 L=45	49,21,63
369	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.05	0.03	2d8/15 L=130	23,21,65
	s=5,m=3	130.0	0.21	12.6	12.6	0.0	0.05	0.02	0.06	0.05	2d8/15 L=130	95,21,65
381	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.05	0.03	2d8/15 L=25	95,21,65
	s=5,m=3	25.2	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.04	2d8/15 L=25	95,21,65
							M_T= 11	Z=0.0	N=24	N=142		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
106	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.02	0.02	2d8/15 L=78	92,86,49
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.01	2d8/15 L=78	92,73,93
147	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/15 L=26	92,86,49
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=52	65,83,93
176	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=78	63,86,50
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=78	65,83,93
203	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=78	65,86,50
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=78	65,83,91
228	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=78	65,88,40
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=78	65,89,91
253	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.01	0.02	2d8/20 L=78	91,84,40
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=78	65,85,91
276	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.01	0.02	2d8/20 L=78	91,84,2
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.03	0.01	0.02	2d8/20 L=78	91,85,91
299	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.01	0.02	2d8/20 L=52	91,84,2
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.03	0.01	0.01	2d8/15 L=26	91,85,93
321	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.01	0.01	2d8/15 L=78	91,84,2
	s=5,m=3	77.8	0.21	12.6	12.6	0.0	0.05	0.04	0.01	0.01	2d8/15 L=78	91,68,54
							M_T= 12	Z=0.0	P=6	P=15		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
112	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.13	0.08	0.09	2d8/15 L=103	90,2,2
	s=5,m=3	355.0	0.21	12.6	12.6	0.0	0.05	0.07	0.04	0.04	2d8/20 L=503	8,87,87
		710.0	0.21	12.6	12.6	0.0	0.07	0.29	0.12	0.14	2d8/15 L=103	54,2,2
107	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.17	0.02	0.02	2d8/15 L=79	54,75,95
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.16	0.02	0.01	2d8/15 L=79	54,75,95
148	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.16	0.02	0.02	2d8/15 L=25	54,75,95
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.15	0.01	0.01	2d8/20 L=54	54,75,4
177	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.15	0.02	0.02	2d8/20 L=79	2,75,54
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.14	0.01	8.95e-03	2d8/20 L=79	2,75,95
204	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.14	0.02	0.03	2d8/20 L=79	2,26,54
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.13	9.13e-03	7.28e-03	2d8/20 L=79	2,75,95
229	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.13	0.02	0.03	2d8/20 L=79	2,75,54
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.12	7.68e-03	6.21e-03	2d8/20 L=79	2,75,95
254	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.12	0.02	0.03	2d8/20 L=79	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.10	7.34e-03	8.54e-03	2d8/20 L=79	2,26,54
277	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.10	0.02	0.04	2d8/20 L=79	2,2,2



	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.09	9.04e-03	0.01	2d8/20 L=79	2,54,54
300	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.02	0.04	2d8/20 L=79	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.07	0.01	0.01	2d8/20 L=79	2,54,54
322	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.03	0.04	2d8/20 L=79	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.05	0.01	0.02	2d8/20 L=79	83,2,2
343	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.03	0.05	2d8/20 L=54	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.04	0.02	0.02	2d8/15 L=25	89,2,2
360	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.04	0.04	2d8/15 L=79	89,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.03	2d8/15 L=79	87,2,2
562	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.04	0.02	2d8/15 L=157	85,88,90
	s=5,m=3	157.4	0.21	12.6	12.6	0.0	0.07	0.05	0.06	0.04	2d8/15 L=157	65,63,63
555	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.04	0.02	2d8/15 L=43	87,12,90
	s=5,m=3	43.1	0.21	12.6	12.6	0.0	0.07	0.02	0.04	0.02	2d8/15 L=43	85,63,65
M_T= 13 Z=0.0 N=360 N=371												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
108	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.08	0.08	2d8/15 L=26	12,2,2
	s=5,m=3	26.0	0.21	12.6	12.6	0.0	0.05	0.01	0.06	0.07	2d8/15 L=26	35,2,8
149	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.14	0.17	2d8/15 L=77	2,2,2
	s=5,m=3	260.0	0.21	12.6	12.6	0.0	0.05	0.18	0.02	8.04e-03	2d8/20 L=413	2,12,63
		520.0	0.21	12.6	12.6	0.0	0.07	0.06	0.14	0.16	2d8/15 L=29	2,2,2
178	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.06	0.06	2d8/15 L=25	63,2,2
	s=5,m=3	25.0	0.21	12.6	12.6	0.0	0.05	0.03	0.07	0.07	2d8/15 L=25	63,2,2
205	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.05	0.05	2d8/15 L=49	63,40,22
	s=5,m=3	49.0	0.21	12.6	12.6	0.0	0.07	0.03	0.08	0.08	2d8/15 L=49	2,2,2
230	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.01	0.03	0.03	2d8/15 L=14	2,83,59
	s=5,m=3	14.0	0.21	12.6	12.6	0.0	0.07	0.01	0.03	0.03	2d8/15 L=14	2,83,59
255	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.02	0.02	2d8/15 L=89	4,59,59
	s=5,m=3	260.0	0.21	12.6	12.6	0.0	0.07	0.03	5.02e-03	4.31e-03	2d8/20 L=343	59,78,82
		520.0	0.21	12.6	12.6	0.0	0.07	0.02	0.02	0.02	2d8/15 L=87	4,59,59
278	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	8.49e-03	0.02	0.02	2d8/15 L=16	26,87,59
	s=5,m=3	16.0	0.21	12.6	12.6	0.0	0.07	7.07e-03	0.02	0.02	2d8/15 L=16	2,87,59
301	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.07	0.08	2d8/15 L=49	2,40,2
	s=5,m=3	49.0	0.21	12.6	12.6	0.0	0.05	0.03	0.05	0.05	2d8/15 L=49	63,40,36
323	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.07	0.07	2d8/15 L=25	63,2,2
	s=5,m=3	25.0	0.21	12.6	12.6	0.0	0.05	0.04	0.05	0.06	2d8/15 L=25	63,40,2
344	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.13	0.16	2d8/15 L=29	2,2,2
	s=5,m=3	260.0	0.21	12.6	12.6	0.0	0.05	0.18	0.01	7.53e-03	2d8/20 L=413	2,26,63
		520.0	0.21	12.6	12.6	0.0	0.07	0.09	0.14	0.17	2d8/15 L=77	2,2,2
361	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.01	0.06	0.07	2d8/15 L=26	21,54,8
	s=5,m=3	26.0	0.21	12.6	12.6	0.0	0.07	0.01	0.07	0.08	2d8/15 L=26	26,54,2
M_T= 14 Z=0.0 N=32 N=150												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
110	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.01	0.02	0.02	2d8/15 L=72	86,91,83
	s=5,m=3	72.3	0.21	12.6	12.6	0.0	0.07	0.02	0.02	0.02	2d8/15 L=72	86,94,2
150	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.02	0.02	2d8/15 L=31	86,91,91
	s=5,m=3	72.3	0.21	12.6	12.6	0.0	0.07	0.03	0.02	0.02	2d8/20 L=41	83,94,2
179	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.02	0.03	2d8/20 L=72	83,95,97
	s=5,m=3	72.3	0.21	12.6	12.6	0.0	0.07	0.05	0.02	0.02	2d8/20 L=72	83,98,96
206	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.02	0.03	2d8/20 L=72	83,95,93
	s=5,m=3	72.3	0.21	12.6	12.6	0.0	0.07	0.07	0.02	0.01	2d8/20 L=72	83,98,92
231	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.08	0.02	0.03	2d8/20 L=72	83,2,2
	s=5,m=3	72.3	0.21	12.6	12.6	0.0	0.05	0.08	8.90e-03	4.28e-03	2d8/20 L=72	83,98,42
144	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.10	0.04	0.07	2d8/20 L=235	83,2,2
	s=5,m=3	338.4	0.21	12.6	12.6	0.0	0.05	0.05	0.04	0.05	2d8/15 L=103	85,91,2
M_T= 15 Z=0.0 N=212 N=219												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
111	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.01	0.02	0.02	2d8/15 L=47	22,54,2
	s=5,m=3	47.0	0.21	12.6	12.6	0.0	0.05	0.02	0.01	4.24e-03	2d8/15 L=47	12,89,77
151	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.02	2d8/15 L=56	12,2,2
	s=5,m=3	105.0	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.02	2d8/20 L=49	12,64,36
180	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.01	0.02	2d8/20 L=68	12,54,12
	s=5,m=3	67.6	0.21	12.6	12.6	0.0	0.05	0.03	0.02	0.02	2d8/20 L=68	12,36,26
207	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.01	0.01	2d8/20 L=68	12,22,12
	s=5,m=3	67.6	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.02	2d8/20 L=68	12,8,2
232	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.01	7.93e-03	2d8/20 L=68	12,88,12
	s=5,m=3	67.6	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.02	2d8/20 L=68	12,8,2
256	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.02	4.10e-03	2d8/20 L=32	12,88,90
	s=5,m=3	67.6	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.02	2d8/15 L=36	22,8,2
279	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.02	5.62e-03	2d8/15 L=68	22,88,37
	s=5,m=3	67.6	0.21	12.6	12.6	0.0	0.05	8.00e-03	0.03	0.03	2d8/15 L=68	16,8,8
M_T= 16 Z=0.0 N=202 N=211												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
113	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.03	0.03	2d8/15 L=82	82,94,10
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	0.02	0.03	8.48e-03	2d8/15 L=82	82,94,24
152	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.01	0.03	0.02	2d8/15 L=21	82,22,2
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	0.02	0.02	4.66e-03	2d8/20 L=61	36,94,80

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



181	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.03	0.02	2d8/20 L=82	26,22,2
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	0.03	0.02	6.19e-03	2d8/20 L=82	2,94,80
208	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.02	2d8/20 L=82	2,22,2
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	0.03	0.02	0.01	2d8/20 L=82	2,8,26
233	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.02	0.01	2d8/20 L=82	2,22,12
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	0.03	0.02	0.02	2d8/20 L=82	2,8,2
257	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.02	0.01	2d8/20 L=82	2,93,22
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.02	2d8/20 L=82	2,2,2
280	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.03	8.12e-03	2d8/20 L=82	2,93,15
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	0.02	0.03	0.02	2d8/20 L=82	2,93,2
302	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.03	8.46e-03	2d8/20 L=61	2,93,15
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	9.36e-03	0.03	0.02	2d8/15 L=21	68,93,2
324	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.01	0.03	9.80e-03	2d8/15 L=82	68,93,82
	s=5,m=3	82.2	0.21	12.6	12.6	0.0	0.05	0.01	0.04	0.02	2d8/15 L=82	84,93,2
M_T= 17 Z=0.0 P=4 P=13												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
114	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.07	0.08	2d8/15 L=103	94,2,2
	s=5,m=3	355.0	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.04	2d8/20 L=503	8,91,97
		710.0	0.21	12.6	12.6	0.0	0.07	0.30	0.11	0.14	2d8/15 L=103	54,2,2
137	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.18	0.02	0.02	2d8/15 L=79	54,87,89
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.17	0.01	0.01	2d8/15 L=79	54,87,89
169	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.16	0.02	0.02	2d8/15 L=25	54,81,89
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.16	0.01	0.01	2d8/20 L=54	2,87,89
196	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.16	0.02	0.03	2d8/20 L=79	2,54,54
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.15	8.45e-03	8.94e-03	2d8/20 L=79	2,87,89
221	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.15	0.02	0.03	2d8/20 L=79	2,54,54
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.13	7.08e-03	7.34e-03	2d8/20 L=79	2,87,89
246	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.13	0.02	0.03	2d8/20 L=79	2,54,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.12	6.05e-03	6.61e-03	2d8/20 L=79	2,87,54
270	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.12	0.02	0.03	2d8/20 L=79	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.11	6.26e-03	9.32e-03	2d8/20 L=79	2,54,54
293	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.02	0.04	2d8/20 L=79	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.09	7.80e-03	0.01	2d8/20 L=79	2,54,54
315	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.02	0.04	2d8/20 L=79	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.07	9.83e-03	0.02	2d8/20 L=79	2,54,54
337	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.08	0.03	0.04	2d8/20 L=79	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.06	0.01	0.02	2d8/20 L=79	91,2,2
355	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.03	0.05	2d8/20 L=54	2,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.04	0.02	0.02	2d8/15 L=25	91,2,2
370	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.04	0.05	2d8/15 L=79	91,2,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.03	2d8/15 L=79	97,2,2
554	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.06	0.04	2d8/15 L=157	65,63,63
	s=5,m=3	157.4	0.21	12.6	12.6	0.0	0.05	0.02	0.05	0.02	2d8/15 L=157	91,12,96
561	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.04	0.02	2d8/15 L=43	91,21,65
	s=5,m=3	43.1	0.21	12.6	12.6	0.0	0.07	0.02	0.05	0.02	2d8/15 L=43	97,12,96
M_T= 18 Z=0.0 N=13 N=131												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
115	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.02	0.01	2d8/15 L=71	92,86,2
	s=5,m=3	70.9	0.21	12.6	12.6	0.0	0.07	0.03	0.03	0.03	2d8/15 L=71	92,2,2
153	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.02	0.01	2d8/15 L=33	92,86,2
	s=5,m=3	70.9	0.21	12.6	12.6	0.0	0.07	0.04	0.03	0.03	2d8/20 L=38	92,2,2
182	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.02	7.62e-03	2d8/20 L=71	92,86,2
	s=5,m=3	70.9	0.21	12.6	12.6	0.0	0.07	0.05	0.02	0.02	2d8/20 L=71	94,2,2
209	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.02	6.68e-03	2d8/20 L=71	94,86,51
	s=5,m=3	70.9	0.21	12.6	12.6	0.0	0.07	0.05	0.02	0.02	2d8/20 L=71	94,86,2
234	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.02	8.78e-03	2d8/20 L=71	94,86,52
	s=5,m=3	70.9	0.21	12.6	12.6	0.0	0.07	0.05	0.02	9.23e-03	2d8/20 L=71	94,86,2
258	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.02	0.01	2d8/20 L=71	94,90,40
	s=5,m=3	70.9	0.21	12.6	12.6	0.0	0.07	0.05	0.02	4.55e-03	2d8/20 L=71	94,98,98
281	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.02	0.02	2d8/20 L=71	94,98,2
	s=5,m=3	70.9	0.21	12.6	12.6	0.0	0.07	0.04	0.02	0.01	2d8/20 L=71	96,98,98
303	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.03	0.03	2d8/20 L=71	96,98,2
	s=5,m=3	70.9	0.21	12.6	12.6	0.0	0.07	0.02	0.03	0.03	2d8/20 L=71	96,98,98
325	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.04	0.05	2d8/20 L=30	93,98,98
	s=5,m=3	95.0	0.21	12.6	12.6	0.0	0.05	0.03	0.04	0.03	2d8/15 L=65	93,98,98
345	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.04	2d8/15 L=38	93,98,98
	s=5,m=3	37.9	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.03	2d8/15 L=38	93,98,98
M_T= 19 Z=0.0 N=356 N=359												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
116	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.08	0.10	2d8/15 L=82	15,36,2
	s=5,m=3	82.0	0.21	12.6	12.6	0.0	0.05	0.06	0.04	0.04	2d8/15 L=82	26,95,2
154	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.13	0.17	2d8/15 L=21	16,8,8
	s=5,m=3	257.5	0.21	12.6	12.6	0.0	0.05	0.20	0.01	7.62e-03	2d8/20 L=413	2,37,26
		515.0	0.21	12.6	12.6	0.0	0.07	0.08	0.14	0.17	2d8/15 L=80	2,2,2
183	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.06	0.07	2d8/15 L=23	35,63,2
	s=5,m=3	23.0	0.21	12.6	12.6	0.0	0.07	0.01	0.07	0.08	2d8/15 L=23	51,63,2

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
RELAZIONE DI CALCOLO DELLA FONDAZIONE



		M_T= 20						Z=0.0	N=372	N=375	Staffe	Rif. cmb
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc		
117	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	6.66e-03	0.08	0.09	2d8/15 L=23	51,64,2
	s=5,m=3	23.0	0.21	12.6	12.6	0.0	0.05	0.02	0.07	0.07	2d8/15 L=23	49,63,2
155	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.15	0.18	2d8/15 L=80	2,8,2
	s=5,m=3	262.5	0.21	12.6	12.6	0.0	0.05	0.20	0.02	7.43e-03	2d8/20 L=413	2,23,12
		525.0	0.21	12.6	12.6	0.0	0.07	0.06	0.14	0.17	2d8/15 L=31	32,64,2
184	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.05	0.05	2d8/15 L=72	12,21,2
	s=5,m=3	72.0	0.21	12.6	12.6	0.0	0.07	0.02	0.09	0.10	2d8/15 L=72	31,50,2
		M_T= 21						Z=0.0	N=226	N=392	Staffe	Rif. cmb
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc		
124	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.09	0.12	0.11	2d8/15 L=79	21,36,64
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.02	0.10	0.08	2d8/15 L=79	54,36,64
156	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.10	0.08	2d8/15 L=25	51,36,64
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.08	0.08	0.08	2d8/20 L=54	54,36,64
185	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.08	0.09	2d8/20 L=79	2,35,63
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.11	0.06	0.05	2d8/20 L=79	54,36,64
210	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.07	0.07	2d8/20 L=79	2,35,63
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.14	0.05	0.03	2d8/20 L=79	54,36,64
235	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.13	0.05	0.05	2d8/20 L=79	2,35,63
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.15	0.03	0.01	2d8/20 L=79	2,36,93
259	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.14	0.04	0.03	2d8/20 L=79	2,21,63
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.15	0.03	0.01	2d8/20 L=79	2,98,92
282	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.15	0.04	0.02	2d8/20 L=79	2,21,93
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.14	0.04	0.02	2d8/20 L=79	64,16,50
304	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.14	0.04	0.01	2d8/20 L=79	2,16,92
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.13	0.06	0.04	2d8/20 L=79	93,16,50
326	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.13	0.06	0.03	2d8/20 L=79	93,16,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.11	0.08	0.06	2d8/20 L=79	93,16,22
346	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.08	0.05	2d8/20 L=54	93,16,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.09	0.09	0.06	2d8/15 L=25	93,16,22
362	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.08	0.09	0.05	2d8/15 L=79	93,16,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.05	0.05	0.11	0.07	2d8/15 L=79	93,16,22
374	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.02	2d8/15 L=67	93,63,21
	s=5,m=3	66.7	0.21	12.6	12.6	0.0	0.07	0.03	0.03	4.15e-03	2d8/15 L=67	93,95,97
384	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.04	8.34e-03	2d8/15 L=67	93,35,21
	s=5,m=3	66.7	0.21	12.6	12.6	0.0	0.07	0.03	0.04	0.01	2d8/15 L=67	93,35,63
392	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.04	9.70e-03	2d8/15 L=67	93,35,2
	s=5,m=3	66.7	0.21	12.6	12.6	0.0	0.05	0.01	0.05	0.03	2d8/15 L=67	93,35,63
		M_T= 22						Z=0.0	P=10	P=18	Staffe	Rif. cmb
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc		
125	ok,ok	0.0	0.21	12.6	12.6	9.4	0.07	2.63e-03	0.21	0.79	2d8/15 L=60	92,60,21
	s=5,m=3	60.0	0.21	12.6	12.6	9.4	0.07	0.02	0.24	0.88	2d8/15 L=60	64,60,21
157	ok,ok	0.0	0.21	12.6	12.6	9.4	0.07	0.02	0.22	0.82	2d8/15 L=60	64,60,21
	s=5,m=3	60.0	0.21	12.6	12.6	9.4	0.07	0.05	0.25	0.92	2d8/15 L=60	64,60,21
134	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.10	0.08	2d8/15 L=65	22,21,8
	s=5,m=3	64.8	0.21	12.6	12.6	0.0	0.07	0.02	0.07	0.04	2d8/15 L=65	96,21,22
166	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.01	0.09	0.07	2d8/15 L=39	24,21,8
	s=5,m=3	64.8	0.21	12.6	12.6	0.0	0.05	0.04	0.06	0.04	2d8/20 L=26	31,21,22
193	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.08	0.07	2d8/20 L=65	32,21,22
	s=5,m=3	64.8	0.21	12.6	12.6	0.0	0.05	0.06	0.05	0.02	2d8/20 L=65	26,21,21
218	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.07	0.06	2d8/20 L=65	26,21,64
	s=5,m=3	64.8	0.21	12.6	12.6	0.0	0.05	0.07	0.04	8.46e-03	2d8/20 L=65	26,21,94
243	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.06	0.04	2d8/20 L=65	26,21,64
	s=5,m=3	64.8	0.21	12.6	12.6	0.0	0.05	0.08	0.05	0.02	2d8/20 L=65	26,49,94
267	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.05	0.03	2d8/20 L=65	26,49,64
	s=5,m=3	64.8	0.21	12.6	12.6	0.0	0.05	0.08	0.06	0.04	2d8/20 L=65	26,49,2
290	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.05	0.01	2d8/20 L=65	26,49,66
	s=5,m=3	64.8	0.21	12.6	12.6	0.0	0.05	0.06	0.07	0.05	2d8/20 L=65	36,49,2
312	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.04	0.01	2d8/20 L=27	26,49,66
	s=5,m=3	130.0	0.21	12.6	12.6	0.0	0.07	0.02	0.10	0.09	2d8/15 L=103	38,49,2
334	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.02	0.09	0.05	2d8/10 L=36	38,49,2
	s=6,m=3	36.5	0.23	18.8	18.8	0.0	0.07	0.02	0.10	0.07	2d8/10 L=36	74,49,2
352	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.02	6.97e-03	2d8/10 L=74	74,95,23
	s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.01	2d8/10 L=74	74,95,2
367	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.01	5.92e-03	2d8/10 L=30	74,23,77
	s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.02	0.01	0.01	2d8/10 L=44	74,54,2
379	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.01	5.10e-03	2d8/10 L=44	74,23,76
	s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.02	0.01	0.01	2d8/10 L=30	2,2,2
389	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.01	6.26e-03	2d8/10 L=74	12,2,79
	s=6,m=3	73.7	0.23	18.8	18.8	0.0	0.07	0.03	0.02	0.01	2d8/10 L=74	2,2,2
397	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.04	0.01	2d8/10 L=74	2,93,12
	s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.02	0.04	6.43e-03	2d8/10 L=74	2,93,69
403	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	8.95e-03	2d8/10 L=30	94,93,22
	s=6,m=3	73.7	0.23	18.8	18.8	0.0	0.07	0.02	0.04	4.18e-03	2d8/10 L=44	37,93,69
409	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	6.27e-03	2d8/10 L=44	37,93,22



s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.02	0.04	5.02e-03	2d8/10 L=30	37,93,68
415 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	4.81e-03	2d8/10 L=74	37,93,69
s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.02	0.04	7.01e-03	2d8/10 L=74	37,97,68
421 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.04	9.72e-03	2d8/10 L=56	79,97,87
s=6,m=3	56.5	0.23	18.8	18.8	0.0	0.07	0.02	0.04	9.38e-03	2d8/10 L=56	98,97,87
427 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	0.01	2d8/10 L=47	79,95,95
s=6,m=3	130.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	0.01	2d8/10 L=83	98,95,2
433 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	0.01	2d8/10 L=20	98,97,87
s=6,m=3	61.7	0.23	18.8	18.8	0.0	0.07	0.02	0.03	0.01	2d8/10 L=42	12,97,2
438 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.03	9.61e-03	2d8/10 L=62	12,97,97
s=6,m=3	61.8	0.23	18.8	18.8	0.0	0.07	0.03	0.03	0.01	2d8/10 L=62	2,97,2
443 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.02	0.02	2d8/10 L=61	12,2,2
s=6,m=3	61.0	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.01	2d8/10 L=61	82,2,2
448 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.02	2d8/10 L=42	82,2,98
s=6,m=3	63.3	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.02	2d8/10 L=21	76,2,98
453 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.02	2d8/10 L=63	76,2,98
s=6,m=3	63.3	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.02	2d8/10 L=63	76,2,98
458 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.02	0.01	2d8/10 L=19	76,2,98
s=6,m=3	63.3	0.23	18.8	18.8	0.0	0.06	0.03	0.01	0.01	2d8/10 L=44	80,40,98
463 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.03	0.02	0.01	2d8/10 L=35	80,2,98
s=6,m=3	35.5	0.23	18.8	18.8	0.0	0.06	0.03	0.02	0.01	2d8/10 L=35	80,84,98
468 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.03	0.02	0.01	2d8/10 L=23	96,2,98
s=6,m=3	23.5	0.23	18.8	18.8	0.0	0.06	0.04	0.02	0.01	2d8/10 L=23	96,2,98
473 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.04	0.01	2d8/10 L=12	80,83,75
s=6,m=3	12.0	0.23	18.8	18.8	0.0	0.06	0.04	0.04	0.01	2d8/10 L=12	80,83,75
478 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.04	0.03	2d8/10 L=91	80,83,31
s=6,m=3	131.5	0.23	18.8	18.8	0.0	0.07	0.01	0.03	0.02	2d8/10 L=68	97,83,75
482 ok,ok	263.0	0.23	18.8	18.8	0.0	0.07	0.03	0.03	0.01	2d8/10 L=103	2,54,2
s=6,m=3	131.5	0.23	18.8	18.8	0.0	0.07	0.01	0.03	0.02	2d8/10 L=103	2,54,2
485 ok,ok	263.0	0.23	18.8	18.8	0.0	0.06	0.04	0.03	0.03	2d8/10 L=68	95,93,81
s=6,m=3	12.0	0.23	18.8	18.8	0.0	0.06	0.03	0.03	0.02	2d8/10 L=91	78,93,15
488 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.03	0.02	2d8/10 L=12	78,93,15
s=6,m=3	33.0	0.23	18.8	18.8	0.0	0.06	0.03	0.03	0.01	2d8/10 L=12	78,93,15
491 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.03	0.03	0.01	2d8/10 L=33	90,83,31
s=6,m=3	33.0	0.23	18.8	18.8	0.0	0.06	0.02	0.02	0.01	2d8/10 L=33	90,83,31
494 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.02	0.02	0.01	2d8/10 L=33	78,83,31
s=6,m=3	61.7	0.23	18.8	18.8	0.0	0.06	0.02	0.02	0.01	2d8/10 L=37	78,83,76
497 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.02	0.02	0.01	2d8/10 L=24	82,83,76
s=6,m=3	61.7	0.23	18.8	18.8	0.0	0.06	0.02	0.02	0.01	2d8/10 L=62	82,83,76
500 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.02	2d8/10 L=62	82,2,76
s=6,m=3	61.7	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.02	2d8/10 L=17	82,2,76
503 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.01	2d8/10 L=44	79,2,76
s=6,m=3	59.0	0.23	18.8	18.8	0.0	0.07	0.03	0.03	0.02	2d8/10 L=59	79,2,2
506 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.02	0.01	2d8/10 L=59	79,2,2
s=6,m=3	76.3	0.23	18.8	18.8	0.0	0.07	0.02	0.02	7.98e-03	2d8/10 L=76	79,95,2
509 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.03	0.01	2d8/10 L=76	76,95,87
s=6,m=3	76.3	0.23	18.8	18.8	0.0	0.07	0.02	0.03	8.86e-03	2d8/10 L=27	76,85,2
512 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.03	0.01	2d8/10 L=49	76,85,64
s=6,m=3	130.0	0.23	18.8	18.8	0.0	0.06	0.03	0.03	0.01	2d8/10 L=54	23,85,2
515 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.03	0.03	8.70e-03	2d8/10 L=76	24,85,81
s=6,m=3	27.5	0.23	18.8	18.8	0.0	0.06	0.03	0.03	8.78e-03	2d8/10 L=27	24,85,81
518 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	9.46e-03	2d8/10 L=74	23,85,2
s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.06	0.02	0.04	4.99e-03	2d8/10 L=74	23,85,69
521 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	7.91e-03	2d8/10 L=30	23,87,2
s=6,m=3	73.7	0.23	18.8	18.8	0.0	0.06	0.02	0.04	3.46e-03	2d8/10 L=44	23,85,68
524 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	5.34e-03	2d8/10 L=44	23,85,69
s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.02	0.03	5.14e-03	2d8/10 L=30	23,83,68
527 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.03	3.74e-03	2d8/10 L=74	23,85,74
s=6,m=3	73.7	0.23	18.8	18.8	0.0	0.07	0.02	0.03	7.71e-03	2d8/10 L=74	23,87,2
530 ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.02	2d8/10 L=80	23,2,2
s=6,m=3	80.0	0.23	18.8	18.8	0.0	0.06	0.03	0.01	0.01	2d8/10 L=80	23,89,2
533 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.03	0.02	0.02	2d8/10 L=23	23,89,2
s=6,m=3	80.0	0.23	18.8	18.8	0.0	0.06	0.03	0.02	8.86e-03	2d8/10 L=57	24,89,12
536 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.02	0.02	2d8/10 L=32	24,89,2
s=6,m=3	67.5	0.23	18.8	18.8	0.0	0.06	0.04	0.02	0.01	2d8/10 L=36	24,89,12
539 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.03	0.02	2d8/10 L=67	24,89,2
s=6,m=3	67.5	0.23	18.8	18.8	0.0	0.06	0.05	0.02	0.01	2d8/10 L=67	24,89,12
542 ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.05	0.05	0.06	2d8/10 L=29	24,63,2
s=6,m=3	29.5	0.23	18.8	18.8	0.0	0.06	0.07	0.04	0.05	2d8/10 L=29	22,63,2
544 ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.07	0.08	2d8/15 L=103	24,54,2
s=5,m=3	140.0	0.21	12.6	12.6	0.0	0.05	0.10	0.03	0.03	2d8/20 L=37	12,65,38
546 ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.10	0.04	0.05	2d8/20 L=80	12,63,2
s=5,m=3	80.1	0.21	12.6	12.6	0.0	0.05	0.11	0.03	0.03	2d8/20 L=80	12,63,8
548 ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.11	0.03	0.03	2d8/20 L=80	12,63,2

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



	s=5,m=3	80.1	0.21	12.6	12.6	0.0	0.05	0.10	0.04	0.05	2d8/20 L=80	12,35,8
550	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.11	0.02	0.01	2d8/20 L=57	12,21,2
	s=5,m=3	80.1	0.21	12.6	12.6	0.0	0.05	0.09	0.05	0.05	2d8/15 L=23	12,7,8
551	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.09	0.02	0.01	2d8/15 L=80	12,35,35
	s=5,m=3	80.1	0.21	12.6	12.6	0.0	0.05	0.06	0.06	0.07	2d8/15 L=80	12,8,8
552	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.16	0.03	2d8/15 L=65	12,35,89
	s=5,m=3	65.0	0.21	12.6	12.6	0.0	0.05	0.04	0.19	0.07	2d8/15 L=65	12,35,54
553	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.18	0.04	2d8/15 L=65	12,35,83
	s=5,m=3	65.0	0.21	12.6	12.6	0.0	0.07	0.01	0.21	0.09	2d8/15 L=65	32,35,54
							M_T=23	Z=0.0	N=125	N=224		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
126	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.08	0.06	2d8/15 L=70	66,16,50
	s=5,m=3	70.4	0.21	12.6	12.6	0.0	0.05	0.06	0.06	0.03	2d8/15 L=70	64,15,49
158	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.07	0.05	2d8/15 L=33	64,16,64
	s=5,m=3	70.4	0.21	12.6	12.6	0.0	0.05	0.08	0.04	0.02	2d8/20 L=37	64,15,63
186	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.06	0.05	2d8/20 L=70	64,22,64
	s=5,m=3	70.4	0.21	12.6	12.6	0.0	0.05	0.10	0.03	0.01	2d8/20 L=70	64,21,93
211	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.10	0.05	0.04	2d8/20 L=70	64,22,64
	s=5,m=3	70.4	0.21	12.6	12.6	0.0	0.05	0.11	0.02	8.32e-03	2d8/20 L=70	64,23,92
236	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.11	0.04	0.04	2d8/20 L=70	64,36,8
	s=5,m=3	70.4	0.21	12.6	12.6	0.0	0.05	0.12	0.03	0.01	2d8/20 L=70	64,32,95
260	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.14	0.05	0.05	2d8/20 L=65	95,36,98
	s=5,m=3	140.0	0.21	12.6	12.6	0.0	0.05	0.13	0.05	0.04	2d8/15 L=75	64,32,95
283	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.13	0.03	0.02	2d8/15 L=28	64,97,95
	s=5,m=3	28.0	0.21	12.6	12.6	0.0	0.05	0.12	0.04	0.03	2d8/15 L=28	64,32,95
305	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.12	0.06	0.04	2d8/15 L=25	64,24,93
	s=5,m=3	25.1	0.21	12.6	12.6	0.0	0.05	0.11	0.05	0.04	2d8/15 L=25	64,24,93
327	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.11	0.05	0.04	2d8/15 L=140	64,66,93
	s=5,m=3	140.0	0.21	12.6	12.6	0.0	0.05	0.07	0.05	0.03	2d8/15 L=140	21,66,95
347	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.05	0.03	2d8/15 L=25	21,66,93
	s=5,m=3	24.9	0.21	12.6	12.6	0.0	0.05	0.07	0.04	0.03	2d8/15 L=25	21,66,93
							M_T=24	Z=0.0	P=1	P=9		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
127	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	9.73e-03	0.17	0.05	2d8/15 L=60	16,64,49
	s=5,m=3	60.0	0.21	12.6	12.6	0.0	0.07	0.05	0.19	0.07	2d8/15 L=60	21,64,49
159	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.17	0.05	2d8/15 L=60	21,64,49
	s=5,m=3	60.0	0.21	12.6	12.6	0.0	0.07	0.10	0.19	0.07	2d8/15 L=60	21,64,49
131	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.16	0.15	0.12	2d8/15 L=103	22,8,8
	s=5,m=3	310.0	0.21	12.6	12.6	0.0	0.05	0.10	0.08	0.03	2d8/20 L=413	8,22,21
		620.0	0.21	12.6	12.6	0.0	0.05	0.06	0.11	0.07	2d8/15 L=103	94,2,2
163	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.10	0.13	0.02	2d8/10 L=65	49,66,92
	s=6,m=3	65.3	0.23	18.8	18.8	0.0	0.06	0.09	0.14	0.03	2d8/10 L=65	49,66,92
190	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.08	0.14	0.03	2d8/10 L=65	49,65,98
	s=6,m=3	65.3	0.23	18.8	18.8	0.0	0.06	0.06	0.15	0.05	2d8/10 L=65	51,66,98
215	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.06	0.14	0.04	2d8/10 L=44	49,65,98
	s=6,m=3	43.9	0.23	18.8	18.8	0.0	0.06	0.04	0.15	0.05	2d8/10 L=44	65,66,98
240	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.09	0.02	2d8/10 L=21	65,50,49
	s=6,m=3	21.4	0.23	18.8	18.8	0.0	0.06	0.04	0.09	0.02	2d8/10 L=21	65,50,50
264	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.08	0.01	2d8/10 L=65	65,50,49
	s=6,m=3	65.3	0.23	18.8	18.8	0.0	0.07	0.03	0.08	0.01	2d8/10 L=65	65,50,8
287	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.08	0.01	2d8/10 L=34	65,50,49
	s=6,m=3	33.8	0.23	18.8	18.8	0.0	0.07	0.03	0.08	0.01	2d8/10 L=34	65,50,50
309	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.06	0.02	2d8/10 L=31	65,97,2
	s=6,m=3	31.5	0.23	18.8	18.8	0.0	0.07	0.03	0.06	0.02	2d8/10 L=31	65,97,2
331	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.06	0.02	2d8/10 L=72	37,97,2
	s=6,m=3	100.0	0.23	18.8	18.8	0.0	0.06	0.04	0.06	0.02	2d8/10 L=28	65,93,69
349	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.03	0.06	0.02	2d8/10 L=60	37,93,2
	s=6,m=3	81.8	0.23	18.8	18.8	0.0	0.06	0.04	0.06	0.01	2d8/10 L=22	49,93,74
364	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.06	0.02	2d8/10 L=82	49,93,2
	s=6,m=3	81.8	0.23	18.8	18.8	0.0	0.06	0.05	0.06	0.02	2d8/10 L=82	49,93,45
376	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.05	0.09	0.07	2d8/10 L=77	88,87,45
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.07	0.02	0.07	0.05	2d8/10 L=77	94,87,92
386	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.08	0.05	2d8/10 L=26	94,95,92
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.07	0.05	0.07	0.03	2d8/10 L=52	94,93,92
394	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.05	0.07	0.03	2d8/10 L=52	94,95,92
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.07	0.08	0.08	0.02	2d8/10 L=26	94,93,93
401	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.08	0.08	0.02	2d8/10 L=78	94,93,92
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.07	0.08	0.09	0.03	2d8/10 L=78	94,93,93
407	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.09	0.18	0.03	2d8/10 L=77	94,91,2
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.07	0.05	0.18	0.03	2d8/10 L=77	94,91,94
413	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.06	0.18	0.03	2d8/10 L=26	94,91,2
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.06	0.02	0.18	0.03	2d8/10 L=52	94,91,94
419	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.03	0.18	0.03	2d8/10 L=52	94,91,50
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.06	0.04	0.18	0.03	2d8/10 L=26	35,91,49
425	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.04	0.18	0.03	2d8/10 L=77	35,91,8
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.06	0.07	0.18	0.03	2d8/10 L=77	35,91,49

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



431	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.07	0.17	0.04	2d8/10 L=76	35,89,60		
	s=6,m=3	76.5	0.23	18.8	18.8	0.0	0.06	0.09	0.16	0.01	2d8/10 L=76	35,89,85		
436	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.09	0.17	0.03	2d8/10 L=27	35,85,69		
	s=6,m=3	95.0	0.23	18.8	18.8	0.0	0.06	0.09	0.15	0.02	2d8/10 L=68	35,83,68		
441	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.09	0.16	0.01	2d8/10 L=0	35,89,84		
	s=6,m=3	51.7	0.23	18.8	18.8	0.0	0.06	0.08	0.16	0.03	2d8/10 L=52	35,83,84		
446	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.08	0.16	0.02	2d8/10 L=52	63,83,84		
	s=6,m=3	51.8	0.23	18.8	18.8	0.0	0.06	0.07	0.16	0.03	2d8/10 L=68	63,83,84		
451	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.08	0.15	0.02	2d8/10 L=21	63,91,71		
	s=6,m=3	21.0	0.23	18.8	18.8	0.0	0.06	0.07	0.15	0.02	2d8/10 L=21	63,91,71		
456	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.08	0.15	0.03	2d8/10 L=82	63,91,71		
	s=6,m=3	127.0	0.23	18.8	18.8	0.0	0.06	0.05	0.15	0.03	2d8/10 L=68	63,91,71		
		254.0	0.23	18.8	18.8	0.0	0.06	0.03	0.15	0.03	2d8/10 L=103	21,91,71		
461	ok,ok	0.0	0.23	18.8	18.8	12.6	0.06	0.03	0.20	0.78	2d8/10 L=86	21,83,83		
	s=6,m=3	86.0	0.23	18.8	18.8	12.5	0.06	0.02	0.19	0.76	2d8/10 L=86	69,85,85		
466	ok,ok	0.0	0.23	18.8	18.8	12.4	0.06	0.02	0.19	0.75	2d8/10 L=24	24,85,85		
	s=6,m=3	24.0	0.23	18.8	18.8	12.4	0.06	0.02	0.19	0.76	2d8/10 L=24	69,85,85		
471	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.03	0.03	0.02	2d8/10 L=78	69,89,83		
	s=6,m=3	78.1	0.23	18.8	18.8	0.0	0.07	0.03	0.03	0.02	2d8/10 L=78	84,89,2		
476	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.02	0.02	2d8/10 L=95	84,89,71		
	s=6,m=3	95.0	0.23	18.8	18.8	0.0	0.07	0.04	0.02	0.02	2d8/10 L=95	68,89,71		
481	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.02	0.02	2d8/10 L=27	84,38,71		
	s=6,m=3	26.9	0.23	18.8	18.8	0.0	0.07	0.03	0.02	0.02	2d8/10 L=27	68,38,71		
484	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.05	0.01	2d8/10 L=78	84,96,90		
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.07	0.03	0.05	0.01	2d8/10 L=78	68,96,86		
487	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.05	0.01	2d8/10 L=26	68,92,2		
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.07	0.02	0.05	8.78e-03	2d8/10 L=52	68,98,90		
490	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.05	9.90e-03	2d8/10 L=52	68,98,2		
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.07	0.01	0.05	8.41e-03	2d8/10 L=23	23,86,94		
493	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.01	0.05	9.58e-03	2d8/10 L=78	68,90,94		
	s=6,m=3	77.5	0.23	18.8	18.8	0.0	0.06	0.02	0.05	8.72e-03	2d8/10 L=78	74,90,94		
496	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.02	0.05	0.02	2d8/10 L=74	23,83,83		
	s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.06	0.02	0.04	0.01	2d8/10 L=74	23,83,83		
499	ok,ok	0.0	0.23	18.8	18.8	0.0	0.06	0.02	0.04	0.01	2d8/10 L=30	23,83,83		
	s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.01	0.04	0.01	2d8/10 L=44	23,83,83		
502	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.01	0.04	0.01	2d8/10 L=44	23,83,83		
	s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.01	0.04	0.01	2d8/10 L=30	26,83,83		
505	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.01	0.04	9.08e-03	2d8/10 L=74	2,87,83		
	s=6,m=3	73.8	0.23	18.8	18.8	0.0	0.07	0.02	0.04	8.80e-03	2d8/10 L=74	2,87,2		
508	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.04	0.02	2d8/10 L=80	2,86,86		
	s=6,m=3	80.5	0.23	18.8	18.8	0.0	0.07	0.02	0.04	0.02	2d8/10 L=80	23,86,86		
511	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.02	0.05	0.02	2d8/10 L=23	23,86,86		
	s=6,m=3	80.5	0.23	18.8	18.8	0.0	0.07	0.02	0.05	0.02	2d8/10 L=58	52,86,86		
514	ok,ok	0.0	0.23	18.8	18.8	0.0	0.07	0.03	0.05	0.02	2d8/10 L=31	52,86,86		
	s=6,m=3	134.0	0.23	18.8	18.8	0.0	0.06	0.04	0.05	0.02	2d8/10 L=103	86,86,86		
517	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.03	0.03	2d8/15 L=70	86,50,2		
	s=5,m=3	70.0	0.21	12.6	12.6	0.0	0.05	0.04	0.01	5.87e-03	2d8/15 L=70	86,49,15		
520	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.03	2d8/15 L=33	86,22,2		
	s=5,m=3	70.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	5.14e-03	2d8/20 L=37	86,51,95		
523	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.03	2d8/20 L=70	86,22,2		
	s=5,m=3	70.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.01	2d8/20 L=70	22,51,38		
526	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.02	2d8/20 L=70	22,89,2		
	s=5,m=3	70.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.02	2d8/20 L=70	22,38,38		
529	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01	2d8/20 L=70	22,89,85		
	s=5,m=3	70.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.02	2d8/20 L=70	22,66,10		
532	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01	2d8/20 L=37	22,89,85		
	s=5,m=3	70.0	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.02	2d8/15 L=33	22,66,8		
535	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	9.59e-03	2d8/15 L=70	22,89,38		
	s=5,m=3	70.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.03	2d8/15 L=70	15,66,8		
538	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.11	0.02	2d8/15 L=65	16,63,88		
	s=5,m=3	65.0	0.21	12.6	12.6	0.0	0.05	0.03	0.14	0.05	2d8/15 L=65	16,63,50		
541	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.12	0.03	2d8/15 L=65	16,63,88		
	s=5,m=3	65.0	0.21	12.6	12.6	0.0	0.07	9.76e-03	0.16	0.07	2d8/15 L=65	33,63,50		
							M_T= 25	Z=0.0	N=1	N=127				
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T	cls	V V/T	acc	Staffe	Rif. cmb
128	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.11	0.06	2d8/15 L=61	98,16,8		
	s=5,m=3	60.5	0.21	12.6	12.6	0.0	0.07	0.05	0.10	0.05	2d8/15 L=61	98,16,2		
160	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.09	0.05	2d8/15 L=43	98,16,64		
	s=5,m=3	60.5	0.21	12.6	12.6	0.0	0.07	0.07	0.08	0.04	2d8/20 L=18	40,16,54		
187	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.08	0.08	0.05	2d8/20 L=140	50,16,59		
	s=5,m=3	140.0	0.21	12.6	12.6	0.0	0.07	0.11	0.05	0.02	2d8/20 L=140	2,15,98		
212	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.05	0.02	2d8/20 L=73	2,16,59		
	s=5,m=3	73.2	0.21	12.6	12.6	0.0	0.07	0.12	0.04	0.02	2d8/20 L=73	2,15,98		
237	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.12	0.04	9.30e-03	2d8/20 L=73	2,64,63		
	s=5,m=3	73.2	0.21	12.6	12.6	0.0	0.07	0.11	0.05	0.03	2d8/20 L=73	2,50,49		
261	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.04	0.01	2d8/20 L=73	2,26,2		

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



		s=5,m=3	73.2	0.21	12.6	12.6	0.0	0.07	0.09	0.06	0.04	2d8/20 L=73	2,36,50	
284	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.10	0.05	0.04		2d8/20 L=73	2,26,2	
	s=5,m=3	73.2	0.21	12.6	12.6	0.0	0.07	0.07	0.07	0.07		2d8/20 L=73	2,36,50	
306	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.07	0.06		2d8/20 L=43	2,26,2	
	s=5,m=3	73.2	0.21	12.6	12.6	0.0	0.07	0.02	0.09	0.07		2d8/15 L=30	2,36,50	
328	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.09	0.07		2d8/15 L=73	40,36,8	
	s=5,m=3	73.2	0.21	12.6	12.6	0.0	0.05	0.05	0.11	0.10		2d8/15 L=73	64,36,50	
							M_T= 26	Z=0.0	N=1	N=55				
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T	cls	V V/T	acc	Staffe	Rif. cmb
129	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.07	0.07			2d8/15 L=10	16,46,2
	s=5,m=3	9.5	0.21	12.6	12.6	0.0	0.07	9.44e-03	0.07	0.06			2d8/15 L=10	70,46,2
161	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.01	0.08	0.07			2d8/15 L=77	16,46,2
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.05	0.06	0.04			2d8/15 L=77	26,46,2
188	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.06	0.06			2d8/15 L=16	26,46,2
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.09	0.04	0.04			2d8/20 L=61	2,46,2
213	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.09	0.05	0.06			2d8/20 L=77	2,40,2
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.12	0.03	0.03			2d8/20 L=77	2,46,22
238	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.12	0.04	0.05			2d8/20 L=77	2,40,2
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.14	0.02	0.01			2d8/20 L=77	2,86,21
262	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.13	0.03	0.03			2d8/20 L=77	2,40,22
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.14	0.02	8.64e-03			2d8/20 L=77	2,86,91
285	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.14	0.02	0.02			2d8/20 L=77	2,86,21
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.14	0.02	0.02			2d8/20 L=77	2,2,91
307	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.14	0.02	0.01			2d8/20 L=77	2,94,23
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.13	0.03	0.04			2d8/20 L=77	8,54,2
329	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.13	0.02	0.02			2d8/20 L=77	8,54,91
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.12	0.04	0.05			2d8/20 L=77	8,54,2
348	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.12	0.03	0.03			2d8/20 L=62	8,54,91
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.09	0.05	0.05			2d8/15 L=16	49,54,2
363	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.09	0.04	0.03			2d8/15 L=77	49,54,2
	s=5,m=3	77.5	0.21	12.6	12.6	0.0	0.05	0.08	0.06	0.06			2d8/15 L=77	51,54,2
375	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.07	0.08			2d8/15 L=10	51,54,2
	s=5,m=3	10.0	0.21	12.6	12.6	0.0	0.05	0.07	0.08	0.08			2d8/15 L=10	51,54,2
385	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.05	0.04			2d8/15 L=76	51,59,49
	s=5,m=3	76.5	0.21	12.6	12.6	0.0	0.05	0.05	0.04	0.02			2d8/15 L=76	51,91,49
393	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.04	0.02			2d8/15 L=27	51,83,35
	s=5,m=3	86.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.01			2d8/20 L=59	51,93,70
400	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.03	7.02e-03			2d8/20 L=86	51,83,72
	s=5,m=3	86.0	0.21	12.6	12.6	0.0	0.05	0.05	0.04	0.03			2d8/20 L=86	51,93,21
406	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.01			2d8/20 L=56	51,83,2
	s=5,m=3	55.7	0.21	12.6	12.6	0.0	0.05	0.05	0.04	0.03			2d8/20 L=56	51,83,49
412	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.04	0.02			2d8/20 L=56	51,83,67
	s=5,m=3	55.7	0.21	12.6	12.6	0.0	0.05	0.06	0.04	0.03			2d8/15 L=48	51,45,49
418	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.04	0.02			2d8/15 L=56	51,83,32
	s=5,m=3	55.7	0.21	12.6	12.6	0.0	0.05	0.07	0.05	0.04			2d8/15 L=56	51,45,49
424	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.06	0.04			2d8/15 L=25	51,49,63
	s=5,m=3	25.5	0.21	12.6	12.6	0.0	0.05	0.06	0.05	0.03			2d8/15 L=25	51,49,63
430	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.06	0.03			2d8/15 L=78	51,49,35
	s=5,m=3	95.0	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.01			2d8/20 L=17	51,95,83
435	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.02			2d8/20 L=63	51,93,63
	s=5,m=3	63.2	0.21	12.6	12.6	0.0	0.05	0.03	0.04	0.02			2d8/20 L=63	51,93,92
440	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.04	0.01			2d8/20 L=23	51,93,65
	s=5,m=3	63.2	0.21	12.6	12.6	0.0	0.05	0.03	0.04	0.02			2d8/15 L=40	51,59,92
445	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.04	0.01			2d8/15 L=63	51,95,92
	s=5,m=3	63.2	0.21	12.6	12.6	0.0	0.05	0.04	0.05	0.03			2d8/15 L=63	51,59,45
450	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.03			2d8/15 L=43	51,89,2
	s=5,m=3	43.5	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.02			2d8/15 L=43	49,89,93
455	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.04			2d8/15 L=60	49,93,93
	s=5,m=3	85.5	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.02			2d8/20 L=26	50,85,93
460	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.04			2d8/20 L=85	50,85,93
	s=5,m=3	85.5	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01			2d8/20 L=85	2,85,72
465	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.02			2d8/20 L=74	2,89,93
	s=5,m=3	74.1	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.02			2d8/20 L=74	2,89,2
470	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01			2d8/20 L=74	2,83,83
	s=5,m=3	74.1	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.02			2d8/20 L=74	31,89,2
475	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.01	1.00e-02			2d8/20 L=74	31,45,67
	s=5,m=3	74.1	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.03			2d8/20 L=74	31,46,2
480	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	6.44e-03			2d8/20 L=45	31,48,70
	s=5,m=3	74.1	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.03			2d8/15 L=29	35,46,2
483	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	9.37e-03			2d8/15 L=74	31,46,94
	s=5,m=3	74.1	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.03			2d8/15 L=74	35,46,2
486	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.04	0.05			2d8/15 L=103	35,92,49
	s=5,m=3	192.5	0.21	12.6	12.6	0.0	0.07	0.02	0.01	0.01			2d8/20 L=178	83,74,73
		385.0	0.21	12.6	12.6	0.0	0.05	0.07	0.04	0.05			2d8/15 L=103	21,21,21
489	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.02			2d8/15 L=57	21,94,2
	s=5,m=3	56.7	0.21	12.6	12.6	0.0	0.05	0.06	0.03	7.66e-03			2d8/15 L=57	21,94,86



492	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.02	2d8/15 L=47	21,94,2
	s=5,m=3	56.7	0.21	12.6	12.6	0.0	0.05	0.06	0.02	3.65e-03	2d8/20 L=10	21,94,4
495	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.02	2d8/20 L=57	21,94,2
	s=5,m=3	56.7	0.21	12.6	12.6	0.0	0.05	0.06	0.02	7.26e-03	2d8/20 L=57	21,92,31
498	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.02	2d8/20 L=77	21,93,93
	s=5,m=3	76.7	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.02	2d8/20 L=77	21,92,72
501	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01	2d8/20 L=77	21,92,72
	s=5,m=3	76.7	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.03	2d8/20 L=77	21,92,32
504	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.02	2d8/20 L=77	21,92,72
	s=5,m=3	76.7	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.05	2d8/20 L=77	73,92,2
507	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.02	2d8/20 L=7	73,92,1
	s=5,m=3	55.0	0.21	12.6	12.6	0.0	0.05	0.03	0.04	0.03	2d8/15 L=48	23,46,2
510	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.03	0.02	2d8/15 L=55	23,92,2
	s=5,m=3	55.0	0.21	12.6	12.6	0.0	0.07	0.02	0.04	0.04	2d8/15 L=55	23,46,2
513	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.05	0.05	2d8/15 L=84	23,45,49
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.07	0.03	0.03	0.03	2d8/15 L=84	31,86,49
516	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.04	0.04	2d8/15 L=19	67,86,49
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.07	0.06	0.02	0.02	2d8/20 L=65	31,86,49
519	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.03	0.04	2d8/20 L=84	31,86,49
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.07	0.07	0.01	5.89e-03	2d8/20 L=84	31,86,84
522	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.02	0.02	2d8/20 L=84	31,90,49
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.07	0.07	0.01	0.01	2d8/20 L=84	31,94,21
525	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.02	5.36e-03	2d8/20 L=84	72,86,84
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.07	0.06	0.03	0.03	2d8/20 L=84	92,86,49
528	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.02	0.02	2d8/20 L=65	92,45,21
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.07	0.04	0.04	0.03	2d8/15 L=19	92,45,49
531	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.03	0.03	2d8/15 L=84	92,45,49
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.05	2d8/15 L=84	23,45,49
534	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.06	0.05	2d8/15 L=76	23,46,2
	s=5,m=3	75.7	0.21	12.6	12.6	0.0	0.05	0.03	0.04	0.02	2d8/15 L=76	24,45,2
537	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.05	0.04	2d8/15 L=28	24,46,2
	s=5,m=3	75.7	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.01	2d8/20 L=48	22,45,2
540	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.04	0.04	2d8/20 L=76	22,46,2
	s=5,m=3	75.7	0.21	12.6	12.6	0.0	0.05	0.06	0.02	5.16e-03	2d8/20 L=76	12,51,37
543	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.04	0.05	2d8/20 L=210	22,22,2
	s=5,m=3	210.5	0.21	12.6	12.6	0.0	0.05	0.04	0.05	0.06	2d8/20 L=210	12,64,2
545	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01	2d8/20 L=61	12,63,26
	s=5,m=3	60.8	0.21	12.6	12.6	0.0	0.05	0.04	0.04	0.05	2d8/20 L=61	12,64,2
547	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.02	2d8/20 L=18	12,63,54
	s=5,m=3	60.8	0.21	12.6	12.6	0.0	0.05	0.02	0.05	0.04	2d8/15 L=43	16,64,2
549	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.04	0.02	2d8/15 L=61	12,63,26
	s=5,m=3	60.8	0.21	12.6	12.6	0.0	0.07	8.68e-03	0.05	0.05	2d8/15 L=61	72,60,2
M_T= 27 Z=0.0 N=55 N=177												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
130	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.01	0.05	0.04	2d8/15 L=71	88,32,36
	s=5,m=3	70.5	0.21	12.6	12.6	0.0	0.07	0.04	0.05	0.03	2d8/15 L=71	88,32,2
162	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.04	0.03	2d8/15 L=33	88,32,35
	s=5,m=3	70.5	0.21	12.6	12.6	0.0	0.07	0.06	0.04	0.03	2d8/20 L=38	88,32,2
189	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.03	0.03	2d8/20 L=71	88,32,35
	s=5,m=3	70.5	0.21	12.6	12.6	0.0	0.07	0.08	0.02	0.02	2d8/20 L=71	88,32,2
214	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.08	0.02	0.02	2d8/20 L=71	88,21,35
	s=5,m=3	70.5	0.21	12.6	12.6	0.0	0.07	0.09	0.01	0.01	2d8/20 L=71	88,83,2
239	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.01	7.74e-03	2d8/20 L=71	88,83,83
	s=5,m=3	70.5	0.21	12.6	12.6	0.0	0.07	0.09	0.02	0.01	2d8/20 L=71	88,86,88
263	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.02	0.01	2d8/20 L=128	88,86,88
	s=5,m=3	128.0	0.21	12.6	12.6	0.0	0.07	0.06	0.03	0.03	2d8/20 L=128	40,88,49
286	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.02	0.02	2d8/20 L=73	50,31,49
	s=5,m=3	73.1	0.21	12.6	12.6	0.0	0.07	0.05	0.04	0.04	2d8/20 L=73	40,35,49
308	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.04	0.04	2d8/20 L=43	40,31,50
	s=5,m=3	73.1	0.21	12.6	12.6	0.0	0.07	0.02	0.05	0.04	2d8/15 L=30	2,31,49
330	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.05	0.04	2d8/15 L=73	40,32,8
	s=5,m=3	73.1	0.21	12.6	12.6	0.0	0.05	0.03	0.06	0.06	2d8/15 L=73	63,31,49
M_T= 28 Z=0.0 N=392 N=421												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
132	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.01	0.04	0.04	2d8/15 L=73	97,49,2
	s=5,m=3	73.0	0.21	12.6	12.6	0.0	0.05	0.03	0.03	0.02	2d8/15 L=73	26,95,2
164	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.06	0.08	2d8/15 L=30	12,50,2
	s=5,m=3	273.5	0.21	12.6	12.6	0.0	0.05	0.11	0.02	0.02	2d8/20 L=413	50,37,23
		547.0	0.21	12.6	12.6	0.0	0.05	0.08	0.05	0.07	2d8/15 L=103	51,2,2
191	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.09	0.07	0.06	2d8/15 L=74	51,59,63
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.05	0.06	0.06	0.04	2d8/15 L=74	51,60,35
216	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.06	0.05	2d8/15 L=30	51,63,63
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.04	2d8/20 L=44	93,60,49
241	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.05	2d8/20 L=74	93,63,63
	s=5,m=3	73.7	0.21	12.6	12.6	0.0	0.07	0.05	0.04	0.03	2d8/20 L=74	93,64,21
265	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.04	0.04	2d8/20 L=74	93,63,21



	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.06	0.02	0.02	2d8/20 L=74	12,54,82
288	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.03	0.02	2d8/20 L=74	12,50,21
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.07	0.02	0.01	2d8/20 L=74	12,40,79
310	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.02	0.01	2d8/20 L=74	12,40,82
	s=5,m=3	73.7	0.21	12.6	12.6	0.0	0.07	0.07	0.03	0.02	2d8/20 L=74	12,45,79
332	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.03	0.01	2d8/20 L=44	12,46,79
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.06	0.04	0.03	2d8/15 L=30	12,45,63
350	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.04	0.03	2d8/15 L=74	12,46,63
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.04	0.05	0.05	2d8/15 L=74	12,49,63
365	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.08	0.08	2d8/15 L=103	12,2,2
	s=5,m=3	285.5	0.21	12.6	12.6	0.0	0.05	0.07	0.03	0.02	2d8/20 L=364	2,12,77
		571.0	0.21	12.6	12.6	0.0	0.05	0.04	0.05	0.05	2d8/15 L=103	23,2,2
377	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.03	6.44e-03	2d8/15 L=61	22,98,98
	s=5,m=3	60.7	0.21	12.6	12.6	0.0	0.05	0.06	0.04	0.02	2d8/15 L=61	22,98,2
387	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.01	2d8/15 L=61	21,88,88
	s=5,m=3	60.7	0.21	12.6	12.6	0.0	0.05	0.04	0.01	6.17e-03	2d8/15 L=61	49,88,76
395	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.01	2d8/15 L=43	49,96,2
	s=5,m=3	60.7	0.21	12.6	12.6	0.0	0.05	0.04	8.56e-03	5.78e-03	2d8/20 L=18	50,96,24
402	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.04	2d8/20 L=284	35,2,2
	s=5,m=3	284.0	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.04	2d8/20 L=284	21,2,2
408	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.01	4.77e-03	2d8/20 L=18	22,90,82
	s=5,m=3	60.7	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.01	2d8/15 L=43	50,90,2
414	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.01	6.95e-03	2d8/15 L=61	50,98,82
	s=5,m=3	60.7	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.02	2d8/15 L=61	63,98,98
420	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.04	0.02	2d8/15 L=61	36,88,88
	s=5,m=3	60.7	0.21	12.6	12.6	0.0	0.05	0.05	0.03	7.31e-03	2d8/15 L=61	36,88,65
426	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.05	0.05	2d8/15 L=103	37,2,2
	s=5,m=3	285.5	0.21	12.6	12.6	0.0	0.05	0.07	0.02	0.02	2d8/20 L=364	2,76,76
		571.0	0.21	12.6	12.6	0.0	0.07	0.08	0.07	0.08	2d8/15 L=103	26,2,2
432	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.05	2d8/15 L=74	79,45,63
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.06	0.04	0.03	2d8/15 L=74	79,46,63
437	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.04	0.03	2d8/15 L=30	79,45,63
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.07	0.02	0.02	2d8/20 L=44	79,46,77
442	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.03	0.03	2d8/20 L=74	79,45,63
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.08	0.02	8.44e-03	2d8/20 L=74	95,88,76
447	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.08	0.02	0.02	2d8/20 L=74	95,77,77
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.08	0.02	0.02	2d8/20 L=74	83,88,76
452	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.08	0.02	0.01	2d8/20 L=74	83,54,76
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.07	0.03	0.03	2d8/20 L=74	83,63,35
457	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.03	0.02	2d8/20 L=74	83,60,49
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.06	0.04	0.05	2d8/20 L=74	83,59,63
462	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.04	0.04	2d8/20 L=44	83,60,49
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.05	2d8/15 L=30	83,59,63
467	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.04	2d8/15 L=74	83,60,21
	s=5,m=3	73.8	0.21	12.6	12.6	0.0	0.05	0.06	0.07	0.06	2d8/15 L=74	51,59,63
472	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.06	0.07	2d8/15 L=103	51,2,2
	s=5,m=3	273.5	0.21	12.6	12.6	0.0	0.05	0.09	0.03	9.38e-03	2d8/20 L=413	2,23,51
		547.0	0.21	12.6	12.6	0.0	0.07	0.02	0.07	0.07	2d8/15 L=30	76,2,2
477	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.03	0.01	2d8/15 L=73	12,89,2
	s=5,m=3	73.0	0.21	12.6	12.6	0.0	0.05	0.01	0.04	0.03	2d8/15 L=73	21,21,2
							M_T=29	Z=0.0	N=283	N=421		
Trave	Note	Pos.	%Af	Af inf.	Af sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
133	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.08	0.07	2d8/15 L=79	88,32,64
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.04	0.07	0.06	2d8/15 L=79	54,32,54
165	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.07	0.06	2d8/15 L=25	2,31,63
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.08	0.06	0.05	2d8/20 L=54	54,32,64
192	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.05	0.06	2d8/20 L=79	2,31,63
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.10	0.04	0.04	2d8/20 L=79	54,32,64
217	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.10	0.04	0.04	2d8/20 L=79	2,31,63
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.12	0.02	0.02	2d8/20 L=79	54,32,64
242	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.03	0.03	2d8/20 L=79	2,89,63
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.12	0.02	0.01	2d8/20 L=79	54,89,83
266	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.12	0.02	0.02	2d8/20 L=79	2,89,83
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.12	0.02	0.01	2d8/20 L=79	83,88,86
289	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.12	0.02	9.80e-03	2d8/20 L=79	83,88,83
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.12	0.03	0.02	2d8/20 L=79	83,88,50
311	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.12	0.03	0.02	2d8/20 L=79	83,32,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.11	0.04	0.03	2d8/20 L=79	83,31,50
333	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.04	0.03	2d8/20 L=79	83,32,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.10	0.06	0.05	2d8/20 L=79	83,31,36
351	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.10	0.06	0.05	2d8/20 L=54	83,32,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.07	0.07	0.07	0.05	2d8/15 L=25	83,32,36
366	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.07	0.05	2d8/15 L=79	83,32,2
	s=5,m=3	78.6	0.21	12.6	12.6	0.0	0.05	0.04	0.08	0.06	2d8/15 L=79	83,32,36
378	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.06	0.02	2d8/15 L=67	90,21,35
	s=5,m=3	66.7	0.21	12.6	12.6	0.0	0.05	0.03	0.05	9.83e-03	2d8/15 L=67	83,22,2

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



388	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.06	0.01	2d8/15 L=67	83,21,35
	s=5,m=3	66.7	0.21	12.6	12.6	0.0	0.07	0.02	0.05	7.84e-03	2d8/15 L=67	83,21,87
396	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.05	6.40e-03	2d8/15 L=67	83,22,2
	s=5,m=3	66.7	0.21	12.6	12.6	0.0	0.05	0.01	0.06	0.02	2d8/15 L=67	83,21,59
M_T= 30 Z=0.0 N=128 N=394												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
135	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.01	2d8/15 L=88	93,93,92
	s=5,m=3	88.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.02	2d8/15 L=88	93,93,93
167	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	7.85e-03	2d8/15 L=15	93,12,68
	s=5,m=3	89.5	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.02	2d8/20 L=74	95,73,2
194	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01	2d8/20 L=86	95,54,71
	s=5,m=3	86.5	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.02	2d8/20 L=86	95,12,2
219	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.02	0.02	2d8/20 L=88	95,2,72
	s=5,m=3	88.0	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.02	2d8/20 L=88	95,93,54
244	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.10	0.02	0.04	2d8/20 L=65	95,93,92
	s=5,m=3	140.0	0.21	12.6	12.6	0.0	0.05	0.07	0.04	0.03	2d8/15 L=75	95,93,93
268	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.03	0.01	2d8/15 L=28	95,93,93
	s=5,m=3	28.0	0.21	12.6	12.6	0.0	0.05	0.07	0.03	0.02	2d8/15 L=28	95,93,93
291	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.05	0.03	2d8/15 L=190	95,95,95
	s=5,m=3	190.0	0.21	12.6	12.6	0.0	0.05	0.09	0.07	0.05	2d8/15 L=190	21,35,98
313	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.02	0.01	2d8/15 L=72	21,91,97
	s=5,m=3	72.1	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.03	2d8/15 L=72	23,91,2
335	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.02	0.02	2d8/15 L=31	23,91,97
	s=5,m=3	262.5	0.21	12.6	12.6	0.0	0.07	0.10	0.05	0.08	2d8/20 L=231	93,2,2
353	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.02	0.02	2d8/20 L=53	93,91,97
	s=5,m=3	78.0	0.21	12.6	12.6	0.0	0.07	0.11	0.03	0.03	2d8/15 L=25	93,2,2
368	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.01	0.01	2d8/15 L=78	93,95,15
	s=5,m=3	78.0	0.21	12.6	12.6	0.0	0.07	0.12	0.02	0.02	2d8/15 L=78	93,35,15
380	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.06	0.04	2d8/15 L=78	2,49,2
	s=5,m=3	78.0	0.21	12.6	12.6	0.0	0.07	0.08	0.05	0.02	2d8/15 L=78	2,21,59
390	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.06	0.04	2d8/15 L=25	2,49,2
	s=5,m=3	95.0	0.21	12.6	12.6	0.0	0.07	0.06	0.05	0.03	2d8/20 L=70	93,49,40
398	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.06	0.05	2d8/20 L=67	93,21,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.07	0.05	0.05	0.03	2d8/20 L=67	51,21,26
404	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.06	0.06	2d8/20 L=31	51,21,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.05	0.06	0.05	0.03	2d8/15 L=36	51,21,54
410	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.07	0.06	2d8/15 L=67	37,22,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.05	0.09	0.06	0.04	2d8/15 L=67	35,21,2
416	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.09	0.04	0.04	2d8/15 L=40	35,23,63
	s=5,m=3	39.9	0.21	12.6	12.6	0.0	0.05	0.07	0.05	0.05	2d8/15 L=40	35,23,35
422	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.04	0.04	2d8/15 L=135	35,23,65
	s=5,m=3	135.0	0.21	12.6	12.6	0.0	0.07	0.03	0.06	0.06	2d8/15 L=135	95,23,63
428	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.05	0.05	2d8/15 L=25	95,23,35
	s=5,m=3	25.2	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.05	2d8/15 L=25	95,23,35
M_T= 31 Z=0.0 N=48 N=419												
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
138	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.02	0.03	2d8/15 L=65	86,23,51
	s=5,m=3	64.6	0.21	12.6	12.6	0.0	0.07	0.03	0.01	0.01	2d8/15 L=65	88,23,51
170	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.03	0.03	2d8/15 L=39	88,23,51
	s=5,m=3	94.0	0.21	12.6	12.6	0.0	0.07	0.03	0.01	0.02	2d8/20 L=55	88,2,2
197	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.02	0.02	2d8/20 L=33	88,51,51
	s=5,m=3	33.0	0.21	12.6	12.6	0.0	0.07	0.03	0.01	0.01	2d8/20 L=33	88,51,51
222	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.02	0.03	2d8/20 L=95	88,51,51
	s=5,m=3	95.0	0.21	12.6	12.6	0.0	0.07	0.04	0.02	0.02	2d8/20 L=95	65,85,2
247	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.01	0.02	2d8/20 L=72	65,37,51
	s=5,m=3	72.5	0.21	12.6	12.6	0.0	0.07	0.04	0.01	0.02	2d8/20 L=72	65,2,2
271	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.02	0.02	2d8/20 L=73	65,83,83
	s=5,m=3	72.5	0.21	12.6	12.6	0.0	0.07	0.04	9.68e-03	0.01	2d8/20 L=73	65,86,86
294	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.02	0.03	2d8/20 L=72	86,36,2
	s=5,m=3	72.5	0.21	12.6	12.6	0.0	0.05	0.05	8.99e-03	8.64e-03	2d8/20 L=72	65,38,2
316	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.03	0.05	2d8/20 L=93	83,8,2
	s=5,m=3	171.5	0.21	12.6	12.6	0.0	0.05	0.06	0.01	0.01	2d8/15 L=79	65,83,89
338	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01	2d8/15 L=24	65,71,40
	s=5,m=3	24.4	0.21	12.6	12.6	0.0	0.05	0.06	0.01	0.01	2d8/15 L=24	65,71,84
356	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01	2d8/15 L=84	83,74,40
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.01	2d8/15 L=84	83,24,83
371	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.01	2d8/15 L=19	83,74,2
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.02	2d8/20 L=65	89,24,36
382	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.02	0.02	2d8/20 L=84	89,74,2
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.05	0.07	0.02	0.02	2d8/20 L=84	89,24,36
391	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.02	0.02	2d8/20 L=84	89,90,2
	s=5,m=3	84.3	0.21	12.6	12.6	0.0	0.05	0.09	0.01	0.01	2d8/20 L=84	89,24,56
399	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.10	0.03	0.04	2d8/20 L=80	89,90,86
	s=5,m=3	82.5	0.21	12.6	12.6	0.0	0.05	0.08	0.02	0.02	2d8/15 L=3	89,87,83
405	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.09	0.03	0.03	2d8/15 L=82	89,90,86
	s=5,m=3	82.5	0.21	12.6	12.6	0.0	0.05	0.07	0.03	0.03	2d8/15 L=82	89,87,83

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



411	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.03	0.02	2d8/15 L=18 89,90,86
	s=5,m=3	18.0	0.21	12.6	12.6	0.0	0.05	0.07	0.02	0.02	2d8/15 L=18 89,90,86
417	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.06	0.03	2d8/15 L=190 85,89,89
	s=5,m=3	190.0	0.21	12.6	12.6	0.0	0.05	0.07	0.06	0.04	2d8/20 L=190 49,21,88
423	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.02	0.01	2d8/15 L=72 35,35,87
	s=5,m=3	72.1	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.03	2d8/15 L=72 49,35,2
429	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.03	0.02	2d8/15 L=31 37,85,87
	s=5,m=3	262.5	0.21	12.6	12.6	0.0	0.07	0.09	0.05	0.08	2d8/20 L=231 89,64,2
434	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.08	0.03	0.02	2d8/20 L=53 89,63,59
	s=5,m=3	78.0	0.21	12.6	12.6	0.0	0.07	0.10	0.04	0.03	2d8/15 L=25 83,64,2
439	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.10	0.02	0.01	2d8/15 L=78 83,63,31
	s=5,m=3	78.0	0.21	12.6	12.6	0.0	0.07	0.11	0.03	0.02	2d8/15 L=78 83,63,31
444	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.04	0.04	2d8/15 L=73 2,49,2
	s=5,m=3	73.0	0.21	12.6	12.6	0.0	0.07	0.08	0.03	0.02	2d8/15 L=73 2,49,15
449	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.09	0.04	0.04	2d8/15 L=30 2,86,2
	s=5,m=3	105.0	0.21	12.6	12.6	0.0	0.07	0.05	0.03	0.03	2d8/20 L=75 87,88,84
454	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.04	0.05	2d8/20 L=62 87,49,2
	s=5,m=3	62.1	0.21	12.6	12.6	0.0	0.07	0.05	0.03	0.03	2d8/20 L=62 51,49,12
459	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.04	0.06	2d8/20 L=31 51,35,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.05	0.06	0.04	0.03	2d8/15 L=36 51,35,54
464	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.05	0.05	2d8/15 L=67 51,36,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.05	0.08	0.04	0.04	2d8/15 L=67 21,35,2
469	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.09	0.04	0.04	2d8/15 L=40 21,37,63
	s=5,m=3	39.9	0.21	12.6	12.6	0.0	0.05	0.07	0.04	0.05	2d8/15 L=40 49,37,21
474	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.04	0.04	2d8/15 L=135 21,37,65
	s=5,m=3	135.0	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.06	2d8/15 L=135 89,37,63
479	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.02	0.05	0.05	2d8/15 L=25 89,37,21
	s=5,m=3	25.2	0.21	12.6	12.6	0.0	0.07	0.03	0.05	0.05	2d8/15 L=25 89,37,21
M_T= 32 Z=0.0 N=175 N=281											
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
139	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.03	9.42e-03	2d8/15 L=67 63,26,85
	s=5,m=3	66.8	0.21	12.6	12.6	0.0	0.05	0.02	0.03	0.01	2d8/15 L=67 59,26,10
171	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.03	0.01	2d8/15 L=37 89,26,85
	s=5,m=3	66.8	0.21	12.6	12.6	0.0	0.05	0.03	0.03	0.02	2d8/20 L=30 89,26,4
198	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.02	0.02	2d8/20 L=67 89,26,89
	s=5,m=3	66.8	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.01	2d8/20 L=67 89,88,86
223	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.02	2d8/20 L=67 89,2,89
	s=5,m=3	66.8	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.01	2d8/20 L=67 89,88,86
248	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.02	2d8/20 L=67 89,88,2
	s=5,m=3	66.8	0.21	12.6	12.6	0.0	0.05	0.06	0.01	6.12e-03	2d8/20 L=67 89,88,37
272	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.03	2d8/20 L=83 89,88,88
	s=5,m=3	86.5	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.02	2d8/15 L=4 89,88,89
295	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.03	0.02	2d8/15 L=86 89,88,88
	s=5,m=3	86.5	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.02	2d8/15 L=86 83,89,89
317	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.03	2d8/15 L=13 83,90,84
	s=5,m=3	13.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.03	2d8/15 L=13 83,90,84
339	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.06	0.03	2d8/15 L=25 83,89,83
	s=5,m=3	25.1	0.21	12.6	12.6	0.0	0.05	0.03	0.06	0.03	2d8/15 L=25 63,89,83
357	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.06	0.03	2d8/15 L=140 83,83,83
	s=5,m=3	140.0	0.21	12.6	12.6	0.0	0.05	0.03	0.05	0.03	2d8/15 L=140 49,89,88
372	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.03	0.05	0.03	2d8/15 L=25 49,83,86
	s=5,m=3	24.9	0.21	12.6	12.6	0.0	0.05	0.04	0.05	0.03	2d8/15 L=25 49,83,86
M_T= 33 Z=0.0 P=8 P=17											
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe Rif. cmb
142	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.04	0.03	2d8/15 L=49 84,49,49
	s=5,m=3	48.5	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.02	2d8/15 L=49 84,49,51
173	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.03	0.03	2d8/15 L=49 84,49,49
	s=5,m=3	48.5	0.21	12.6	12.6	0.0	0.05	0.03	0.02	0.02	2d8/15 L=49 65,92,51
200	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.04	0.04	2d8/15 L=6 63,49,49
	s=5,m=3	105.0	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.02	2d8/20 L=99 65,2,85
225	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.03	0.03	2d8/20 L=77 65,49,49
	s=5,m=3	77.4	0.21	12.6	12.6	0.0	0.05	0.05	0.02	0.02	2d8/20 L=77 65,92,2
250	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.03	2d8/20 L=77 65,50,83
	s=5,m=3	77.4	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.02	2d8/20 L=77 83,98,86
274	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.06	0.02	0.03	2d8/20 L=77 83,26,83
	s=5,m=3	77.4	0.21	12.6	12.6	0.0	0.05	0.07	0.03	0.03	2d8/20 L=77 83,94,86
297	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.02	0.03	2d8/20 L=77 83,2,83
	s=5,m=3	77.4	0.21	12.6	12.6	0.0	0.05	0.10	0.03	0.03	2d8/20 L=77 83,94,86
319	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.11	0.02	0.03	2d8/20 L=77 83,2,2
	s=5,m=3	77.4	0.21	12.6	12.6	0.0	0.05	0.11	0.03	0.02	2d8/20 L=77 83,94,90
341	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.15	0.02	0.02	2d8/20 L=8 83,86,4
	s=5,m=3	85.0	0.21	12.6	12.6	0.0	0.05	0.15	0.02	0.02	2d8/15 L=77 83,74,89
359	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.15	0.02	7.12e-03	2d8/15 L=26 83,94,59
	s=5,m=3	25.9	0.21	12.6	12.6	0.0	0.05	0.14	0.03	0.01	2d8/15 L=26 83,94,59
141	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.16	0.08	0.09	2d8/15 L=103 86,2,2
	s=5,m=3	355.0	0.21	12.6	12.6	0.0	0.05	0.11	0.04	0.03	2d8/20 L=503 89,85,83

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



		710.0	0.21	12.6	12.6	0.0	0.07	0.18	0.10	0.12	2d8/15 L=103	2,2,2
140	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.06	0.02	0.01	2d8/15 L=77	54,26,4
	s=5,m=3	77.1	0.21	12.6	12.6	0.0	0.07	0.07	0.02	0.01	2d8/15 L=77	54,82,1
172	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.02	0.02	2d8/15 L=26	2,84,88
	s=5,m=3	252.5	0.21	12.6	12.6	0.0	0.07	0.13	0.05	0.06	2d8/20 L=226	54,2,2
199	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.02	0.01	2d8/20 L=58	87,59,15
	s=5,m=3	83.0	0.21	12.6	12.6	0.0	0.07	0.12	0.03	0.03	2d8/15 L=25	87,2,2
224	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.12	0.02	0.01	2d8/15 L=78	2,2,4
	s=5,m=3	78.0	0.21	12.6	12.6	0.0	0.07	0.13	0.02	0.02	2d8/15 L=78	2,45,45
249	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.13	0.06	0.04	2d8/15 L=78	2,2,2
	s=5,m=3	78.0	0.21	12.6	12.6	0.0	0.07	0.10	0.05	0.02	2d8/15 L=78	2,26,59
273	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.11	0.07	0.04	2d8/15 L=25	2,2,2
	s=5,m=3	95.0	0.21	12.6	12.6	0.0	0.07	0.07	0.05	0.03	2d8/20 L=70	2,26,45
296	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.07	0.07	0.05	2d8/20 L=67	2,2,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.07	0.04	0.05	0.03	2d8/20 L=67	2,2,60
318	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.04	0.07	0.06	2d8/20 L=31	2,2,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.07	0.05	0.06	0.03	2d8/15 L=36	51,2,54
340	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.05	0.08	0.06	2d8/15 L=67	51,2,2
	s=5,m=3	67.1	0.21	12.6	12.6	0.0	0.05	0.07	0.07	0.04	2d8/15 L=67	49,2,2
358	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.05	0.03	2d8/15 L=40	49,35,63
	s=5,m=3	39.9	0.21	12.6	12.6	0.0	0.05	0.06	0.05	0.04	2d8/15 L=40	49,35,63
373	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.07	0.05	0.03	2d8/15 L=135	65,35,65
	s=5,m=3	135.0	0.21	12.6	12.6	0.0	0.05	0.02	0.06	0.05	2d8/15 L=135	89,35,63
383	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.02	0.05	0.04	2d8/15 L=25	89,35,65
	s=5,m=3	25.2	0.21	12.6	12.6	0.0	0.07	0.02	0.05	0.04	2d8/15 L=25	89,35,65
							M_T= 34	Z=0.0	N=33	N=154		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
143	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.01	0.03	0.03	2d8/15 L=71	96,93,85
	s=5,m=3	71.3	0.21	12.6	12.6	0.0	0.05	0.02	0.02	0.01	2d8/15 L=71	85,93,92
174	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.03	0.03	2d8/15 L=32	85,93,85
	s=5,m=3	71.3	0.21	12.6	12.6	0.0	0.05	0.04	0.02	0.02	2d8/20 L=39	85,92,84
201	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.05	0.03	0.04	2d8/20 L=71	85,91,87
	s=5,m=3	71.3	0.21	12.6	12.6	0.0	0.05	0.07	0.02	0.02	2d8/20 L=71	85,94,90
226	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.08	0.03	0.03	2d8/20 L=71	85,91,83
	s=5,m=3	71.3	0.21	12.6	12.6	0.0	0.05	0.09	0.02	0.02	2d8/20 L=71	85,94,90
251	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.10	0.02	0.03	2d8/20 L=76	85,95,2
	s=5,m=3	76.3	0.21	12.6	12.6	0.0	0.05	0.11	0.01	4.45e-03	2d8/20 L=76	85,98,86
145	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.13	0.04	0.07	2d8/20 L=235	85,2,2
	s=5,m=3	338.4	0.21	12.6	12.6	0.0	0.07	0.05	0.05	0.06	2d8/15 L=103	83,54,2
							M_T= 38	Z=0.0	N=320	N=321		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
565	ok,ok	0.0	0.21	12.6	12.6	0.0	0.05	0.04	0.06	0.07	2d8/15 L=103	59,59,59
	s=5,m=3	295.0	0.21	12.6	12.6	0.0	0.07	0.08	0.01	2.69e-03	2d8/20 L=383	59,2,21
		590.0	0.21	12.6	12.6	0.0	0.07	0.03	0.06	0.06	2d8/15 L=103	31,59,59
							M_T= 39	Z=0.0	N=322	N=323		
Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc	Staffe	Rif. cmb
566	ok,ok	0.0	0.21	12.6	12.6	0.0	0.07	0.03	0.06	0.06	2d8/15 L=103	15,59,59
	s=5,m=3	295.0	0.21	12.6	12.6	0.0	0.07	0.08	9.14e-03	2.21e-03	2d8/20 L=383	59,2,49
		590.0	0.21	12.6	12.6	0.0	0.05	0.04	0.06	0.07	2d8/15 L=103	15,59,59
Trave			%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc		
			0.23	18.84	18.85	12.59	0.07	0.30	0.25	0.92		

14. STATI LIMITE D' ESERCIZIO

LEGENDA TABELLA STATI LIMITE D' ESERCIZIO

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati, in relazione al tipo di elemento strutturale, i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni rare
- Combinazioni frequenti
- Combinazioni quasi permanenti.

I valori di interesse sono i seguenti:

rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]
wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]
dR	massima deformazione in combinazioni rare
dF	massima deformazione in combinazioni frequenti
dP	massima deformazione in combinazioni quasi permanenti

Per ognuno dei nove valori soprariportati viene indicata (Rif.cmb) la combinazione in cui si è verificato.

In relazione al tipo di elemento strutturale i valori sono selezionati nel modo seguente:

pilastr	rRfck	rRfyk	rPfck	per sezioni significative
travi	rRfck	rRfyk	rPfck	per sezioni significative
	wR	wF	wP	per sezioni significative
	dR	dF	dP	massimi in campata
	rRfck	rRfyk	rPfck	massimi nei nodi dell'elemento
setti e gusci	wR	wF	wP	massimi nei nodi dell'elemento

Si precisa che i valori di massima deformazione per travi sono riferiti al piano verticale (piano locale 1-2 con momenti flettenti 3-3).

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



Trave	Pos. cm	rRfck	rRfyk	rPfck	Rif. cmb	wR mm	wF mm	wP mm	Rif. cmb	dR cm	dF cm	dP cm	Rif. cmb
105	0.0	6.02e-03	0.01	6.54e-03	153,151,171	0.0	0.0	0.0	0,0,0	-0.18	-0.12	-	
0.11162,166,171	58.4	5.64e-03	0.02	6.22e-03	162,162,171	0.0	0.0	0.0	0,0,0				
106	0.0	2.39e-03	7.46e-03	2.15e-		0.08	0.07	0.07	162,166,171				
03161,161,1710.0	77.8	3.03e-03	0.01	2.67e-03	162,162,171	0.0	0.0	0.0	0,0,0				
107	0.0	0.05	0.15	0.04	158,132,171	0.0	0.0	0.0	0,0,0	0.11	0.09	0.08	160,170,1
71	78.6	0.05	0.15	0.04	158,132,171	0.0	0.0	0.0	0,0,0				
108	0.0	5.32e-03	0.01	5.54e-		0.07	0.07	0.07	135,166,171				
03137,132,1710.0	26.0	2.45e-03	7.12e-03	2.71e-03	148,148,171	0.0	0.0	0.0	0,0,0				
109	0.0	0.03	0.07	0.03	151,151,171	0.0	0.0	0.0	0,0,0	0.07	0.06	0.06	162,166,1
71	355.0	0.02	0.08	0.02	163,163,171	0.0	0.0	0.0	0,0,0				
110	710.0	0.06	0.17	0.05	132,158,171	0.0	0.0	0.0	0,0,0				
03 0.0 153,154,0	0.0	1.77e-03	2.91e-	0.0	0,0,0	0.14	0.09	0.08	162,166,171				
111	72.3	1.61e-03	6.96e-03	5.26e-04	160,160,171	0.0	0.0	0.0	0,0,0				
03163,132,1710.0	0.0	3.22e-03	7.23e-03	3.26e-		0.03	0.03	0.03	141,166,171				
112	47.0	4.17e-03	0.01	4.38e-03	142,132,171	0.0	0.0	0.0	0,0,0	-0.06	-0.05	-	
0.04155,166,171	0.0	0.03	0.07	0.03	151,132,171	0.0	0.0	0.0	0,0,0				
113	355.0	0.01	0.06	0.01	156,135,171	0.0	0.0	0.0	0,0,0				
0.030.02	710.0	0.09	0.24	0.09	158,158,171	0.0	0.0	0.0	0,0,0				
114	0.0	0.0	0.02	0.0	0,141,0	0.0	0.0	0.0	0,0,0				
0.02158,166,171	82.2	5.22e-04	0.02	0.0	144,149,0	0.0	0.0	0.0	0,0,0	-0.05	-0.02	-	
115	0.0	2.09e-03	7.82e-03	1.60e-		0.05	0.04	0.04	162,166,171				
03161,158,1710.0	70.9	3.92e-03	8.43e-03	2.66e-03	151,151,171	0.0	0.0	0.0	0,0,0				
116	0.0	7.44e-03	0.02	6.22e-03	138,141,171	0.0	0.0	0.0	0,0,0	-0.23	-0.17	-	
0.16148,166,171	82.0	0.01	0.05	0.01	144,144,171	0.0	0.0	0.0	0,0,0				
117	0.0	1.03e-03	3.22e-03	2.30e-		0.12	0.11	0.11	141,166,171				
04148,141,1710.0	23.0	5.07e-03	0.02	5.32e-03	148,141,171	0.0	0.0	0.0	0,0,0				
124	0.0	0.02	0.06	0.02	141,141,171	0.0	0.0	0.0	0,0,0	-0.08	-0.05	-	
0.04155,166,171	78.6	6.58e-03	6.31e-03	4.03e-03	158,158,171	0.0	0.0	0.0	0,0,0				
125	0.0	1.28e-03	1.29e-03	1.38e-		0.01	0.01	0.01	148,166,171				
03153,153,1710.0	60.0	6.17e-03	5.92e-03	6.08e-03	163,158,171	0.0	0.0	0.0	0,0,0				
126	0.0	6.35e-03	6.45e-03	5.62e-		0.10	0.10	0.10	162,166,171				
03163,163,1710.0	70.4	0.01	0.03	0.01	163,163,171	0.0	0.0	0.0	0,0,0				
127	0.0	2.99e-03	3.87e-03	1.76e-		0.02	0.01	0.01	148,166,171				
03139,137,1710.0	60.0	0.02	0.04	0.02	141,141,171	0.0	0.0	0.0	0,0,0				
128	0.0	1.80e-03	6.18e-03	0.0	153,154,0	0.0	0.0	0.0	0,0,0	-0.14	-0.11	-	
0.20162,166,171	60.5	0.02	0.04	0.02	151,151,171	0.0	0.0	0.0	0,0,0				
129	0.0	5.24e-03	0.01	3.95e-		0.32	0.31	0.31	148,166,171				
03139,139,1710.0	9.5	2.78e-03	4.52e-03	7.53e-04	138,139,171	0.0	0.0	0.0	0,0,0				
130	0.0	9.71e-04	6.32e-03	4.18e-		0.13	0.12	0.12	162,166,171				
04161,161,1710.0	70.5	9.61e-03	0.03	0.01	154,151,171	0.0	0.0	0.0	0,0,0				
131	0.0	0.05	0.13	0.06	142,142,171	0.0	0.0	0.0	0,0,0	-0.21	-0.16	-	
0.15148,166,171	310.0	0.02	0.09	0.02	135,135,171	0.0	0.0	0.0	0,0,0				
132	620.0	8.65e-03	0.04	5.64e-03	155,155,171	0.0	0.0	0.0	0,0,0				
0.10148,166,171	0.0	1.45e-03	8.79e-03	1.46e-03	148,148,171	0.0	0.0	0.0	0,0,0	-0.14	-0.11	-	
133	73.0	5.44e-03	0.03	6.59e-03	144,132,171	0.0	0.0	0.0	0,0,0				
03148,155,1710.0	0.0	8.67e-03	0.02	8.16e-		0.05	0.05	0.05	158,165,171				

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
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	78.6	0.01	0.04	9.79e-03	158,132,171	0.0	0.0	0.0	0,0,0			
134	0.0	0.02	0.03	0.02	142,158,171	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-
0.01148,166,171												
	64.8	2.22e-03	2.05e-03	2.59e-03	146,146,171	0.0	0.0	0.0	0,0,0			
135	0.0	8.14e-03	0.02	7.04e-								
03163,158,171	10.0	0.0	0.0	0,0,0	0.06	0.05	0.05	162,166,171				
	88.0	6.95e-03	0.02	5.71e-03	162,163,171	0.0	0.0	0.0	0,0,0			
136	0.0	0.03	0.08	0.01	158,132,171	0.0	0.0	0.0	0,0,0	0.06	0.06	0.05 160,170,1
71												
	72.1	0.02	0.08	0.01	158,132,171	0.0	0.0	0.0	0,0,0			
137	0.0	0.05	0.16	0.05	158,132,171	0.0	0.0	0.0	0,0,0	-		
0.110.04	0.04	160,170,171										
	78.6	0.05	0.16	0.04	158,132,171	0.0	0.0	0.0	0,0,0			
138	0.0	3.51e-03	6.90e-03	1.31e-03	153,153,171	0.0	0.0	0.0	0,0,0	-0.30	-0.22	-
0.18162,166,171												
	64.6	1.57e-03	6.22e-03	0.0	154,162,0	0.0	0.0	0.0	0,0,0			
139	0.0	5.71e-03	0.01	5.01e-03	162,158,171	0.0	0.0	0.0	0,0,0	-0.11	-0.11	-
0.10162,166,171												
	66.8	5.21e-03	9.89e-03	5.40e-03	162,158,171	0.0	0.0	0.0	0,0,0			
140	0.0	0.02	0.06	7.10e-03	158,132,171	0.0	0.0	0.0	0,0,0	-0.04	-0.04	-
0.04160,170,171												
	77.1	0.02	0.06	9.03e-03	158,132,171	0.0	0.0	0.0	0,0,0			
141	0.0	0.02	0.06	0.03	151,132,171	0.0	0.0	0.0	0,0,0	-0.14	-0.12	-
0.12162,166,171												
	355.0	0.02	0.09	0.02	163,163,171	0.0	0.0	0.0	0,0,0			
	710.0	0.06	0.15	0.04	132,132,171	0.0	0.0	0.0	0,0,0			
142	0.0	2.60e-03	5.57e-03	4.73e-								
04153,153,171	10.0	0.0	0.0	0,0,0	0.08	0.06	0.05	162,166,171				
	48.5	2.47e-03	0.01	1.87e-03	162,162,171	0.0	0.0	0.0	0,0,0			
143	0.0	1.55e-03	2.26e-03	4.31e-05	153,154,171	0.0	0.0	0.0	0,0,0	-0.10	-0.07	-
0.06162,166,171												
	71.3	2.93e-03	0.01	2.21e-03	160,160,171	0.0	0.0	0.0	0,0,0			
144	0.0	4.06e-03	0.02	4.06e-								
04160,160,171	10.0	0.0	0.0	0,0,0	0.14	0.09	0.08	162,166,171				
	338.4	2.62e-03	0.02	0.0	163,163,0	0.0	0.0	0.0	0,0,0			
145	0.0	7.19e-03	0.04	4.72e-03	160,160,171	0.0	0.0	0.0	0,0,0	-0.10	-0.07	-
0.06162,166,171												
	338.4	3.10e-03	0.01	3.64e-03	153,132,171	0.0	0.0	0.0	0,0,0			
146	0.0	5.40e-03	0.02	5.97e-03	162,160,171	0.0	0.0	0.0	0,0,0	-0.18	-0.12	-
0.11162,166,171												
	58.4	0.01	0.05	0.01	162,162,171	0.0	0.0	0.0	0,0,0			
147	0.0	3.00e-03	0.01	2.66e-								
03162,162,171	10.0	0.0	0.0	0,0,0	0.12	0.08	0.07	162,166,171				
	77.8	3.65e-03	0.01	2.89e-03	162,162,171	0.0	0.0	0.0	0,0,0			
148	0.0	0.05	0.15	0.04	158,132,171	0.0	0.0	0.0	0,0,0	0.11	0.09	0.08 160,170,1
71												
	78.6	0.04	0.15	0.03	158,132,171	0.0	0.0	0.0	0,0,0			
149	0.0	0.03	0.07	0.04	132,132,171	0.0	0.0	0.0	0,0,0	0.08	0.07	0.07 142,166,1
71												
	260.0	0.04	0.15	0.04	132,132,171	0.0	0.0	0.0	0,0,0			
	520.0	0.02	0.05	0.02	132,132,171	0.0	0.0	0.0	0,0,0			
150	0.0	1.72e-03	7.76e-03	5.48e-								
04160,160,171	10.0	0.0	0.0	0,0,0	0.14	0.09	0.08	162,166,171				
	72.3	2.60e-03	0.01	9.39e-04	160,160,171	0.0	0.0	0.0	0,0,0			
151	0.0	3.64e-03	9.18e-03	3.78e-								
03142,137,171	10.0	0.0	0.0	0,0,0	0.04	0.03	0.03	141,166,171				
	105.0	4.92e-03	0.02	4.97e-03	137,137,171	0.0	0.0	0.0	0,0,0			
152	0.0	9.39e-04	0.02	0.0	144,149,0	0.0	0.0	0.0	0,0,0	-		
0.030.02	0.02	148,166,171										
	82.2	3.18e-03	0.03	1.78e-03	144,149,171	0.0	0.0	0.0	0,0,0			
153	0.0	3.68e-03	8.74e-03	2.44e-								
03154,151,171	10.0	0.0	0.0	0,0,0	0.06	0.05	0.04	162,166,171				
	70.9	7.91e-03	0.02	6.94e-03	151,132,171	0.0	0.0	0.0	0,0,0			
154	0.0	0.02	0.04	0.02	139,142,171	0.0	0.0	0.0	0,0,0	-0.23	-0.17	-
0.16148,166,171												
	257.5	0.04	0.17	0.05	132,144,171	0.0	0.0	0.0	0,0,0			
	515.0	0.03	0.06	0.03	132,144,171	0.0	0.0	0.0	0,0,0			
155	0.0	0.03	0.07	0.03	132,137,171	0.0	0.0	0.0	0,0,0	0.17	0.12	0.11 141,166,1
71												
	262.5	0.04	0.17	0.05	132,137,171	0.0	0.0	0.0	0,0,0			
	525.0	0.02	0.05	0.02	147,149,171	0.0	0.0	0.0	0,0,0			
156	0.0	3.36e-03	3.22e-03	1.48e-03	158,158,171	0.0	0.0	0.0	0,0,0	-0.08	-0.05	-
0.04155,166,171												
	78.6	0.03	0.05	0.03	158,132,171	0.0	0.0	0.0	0,0,0			
157	0.0	6.33e-03	5.95e-03	6.36e-								
03163,163,171	10.0	0.0	0.0	0,0,0	0.02	0.01	0.01	148,166,171				

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



	60.0	0.02	0.03	0.02163,158,171	0.0	0.0	0.0	0,0,0			
158	0.0	0.01	0.03	0.01163,163,171	0.0	0.0	0.0	0,0,0	0.12	0.10	0.10 162,166,1
71											
	70.4	0.02	0.05	0.02162,163,171	0.0	0.0	0.0	0,0,0			
159	0.0	0.02	0.04	0.02141,141,171	0.0	0.0	0.0	0,0,0	0.02	0.02	0.01 148,166,1
71											
	60.0	0.03	0.08	0.04141,155,171	0.0	0.0	0.0	0,0,0			
160	0.0	0.01	0.04	0.02154,151,171	0.0	0.0	0.0	0,0,0	-0.14	-0.11	-
0.20162,166,171											
	60.5	0.02	0.07	0.03151,151,171	0.0	0.0	0.0	0,0,0			
161	0.0	3.84e-03	5.64e-03	2.26e-							
03139,139,1710.0	0.0	0.0	0.0	0,0,0	0.28	0.32	0.31148,166,171				
	77.5	9.59e-03	0.04	0.01144,144,171	0.0	0.0	0.0	0,0,0			
162	0.0	8.93e-									
030.03	0.01153,151,171		0.0	0.0	0.0	0,0,0	0.16	0.13	0.12162,166,171		
	70.5	0.02	0.05	0.02154,151,171	0.0	0.0	0.0	0,0,0			
163	0.0	0.02	0.08	0.02155,155,171	0.0	0.0	0.0	0,0,0	-0.02	-0.01	-
0.01162,166,171											
	65.3	0.02	0.07	0.02155,155,171	0.0	0.0	0.0	0,0,0			
164	0.0	8.62e-03	0.02	8.81e-03137,137,171	0.0	0.0	0.0	0,0,0	-0.14	-0.11	-
0.10148,166,171											
	273.5	0.02	0.09	0.03156,156,171	0.0	0.0	0.0	0,0,0			
	547.0	0.01	0.05	6.38e-03155,155,171	0.0	0.0	0.0	0,0,0			
165	0.0	9.38e-03	0.04	6.68e-							
03158,132,1710.0	0.0	0.0	0.0	0,0,0	0.07	0.05	0.05158,165,171				
	78.6	0.02	0.08	0.02158,132,171	0.0	0.0	0.0	0,0,0			
166	0.0	3.06e-03	3.02e-03	2.23e-03142,142,171	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-
0.01148,166,171											
	64.8	8.49e-03	0.02	0.01146,147,171	0.0	0.0	0.0	0,0,0			
167	0.0	7.39e-03	0.02	6.06e-							
03163,163,1710.0	0.0	0.0	0.0	0,0,0	0.06	0.05	0.05162,166,171				
	89.5	6.30e-03	0.02	4.66e-03162,163,171	0.0	0.0	0.0	0,0,0			
168	0.0	0.03	0.09	0.02158,132,171	0.0	0.0	0.0	0,0,0	0.06	0.06	0.05 160,170,1
71											
	257.5	0.04	0.12	0.03158,132,171	0.0	0.0	0.0	0,0,0			
169	0.0	0.05	0.16	0.04158,132,171	0.0	0.0	0.0	0,0,0	-		
0.110.04	0.04160,170,171										
	78.6	0.05	0.16	0.04158,132,171	0.0	0.0	0.0	0,0,0			
170	0.0	3.13e-03	4.24e-03	6.44e-04154,161,171	0.0	0.0	0.0	0,0,0	-0.30	-0.22	-
0.18162,166,171											
	94.0	3.16e-03	0.01	3.27e-04162,162,171	0.0	0.0	0.0	0,0,0			
171	0.0	5.16e-03	0.01	5.27e-03160,158,171	0.0	0.0	0.0	0,0,0	-0.11	-0.11	-
0.10162,166,171											
	66.8	5.32e-03	0.01	5.38e-03160,158,171	0.0	0.0	0.0	0,0,0			
172	0.0	0.02	0.07	0.01158,132,171	0.0	0.0	0.0	0,0,0	-0.04	-0.04	-
0.04161,170,171											
	252.5	0.04	0.11	0.03158,132,171	0.0	0.0	0.0	0,0,0			
173	0.0	2.49e-03	0.01	1.87e-							
03162,162,1710.0	0.0	0.0	0.0	0,0,0	0.08	0.06	0.05162,166,171				
	48.5	4.79e-03	0.02	3.92e-03162,162,171	0.0	0.0	0.0	0,0,0			
174	0.0	2.98e-03	0.01	2.18e-03160,160,171	0.0	0.0	0.0	0,0,0	-0.10	-0.07	-
0.06162,166,171											
	71.3	4.90e-03	0.02	3.89e-03160,160,171	0.0	0.0	0.0	0,0,0			
175	0.0	0.01	0.05	0.01162,162,171	0.0	0.0	0.0	0,0,0	-0.18	-0.12	-
0.11162,166,171											
	58.4	0.02	0.07	0.02162,162,171	0.0	0.0	0.0	0,0,0			
176	0.0	3.66e-03	0.01	2.93e-							
03162,162,1710.0	0.0	0.0	0.0	0,0,0	0.12	0.08	0.07162,166,171				
	77.8	3.97e-03	0.01	2.93e-03162,162,171	0.0	0.0	0.0	0,0,0			
177	0.0	0.04	0.15	0.03158,132,171	0.0	0.0	0.0	0,0,0	0.11	0.09	0.08 158,165,1
71											
	78.6	0.04	0.15	0.03158,132,171	0.0	0.0	0.0	0,0,0			
178	0.0	9.26e-									
030.04	0.01162,162,171		0.0	0.0	0.0	0,0,0	0.08	0.07	0.07146,168,171		
	25.0	5.96e-03	0.02	6.16e-03162,162,171	0.0	0.0	0.0	0,0,0			
179	0.0	2.74e-03	0.01	9.65e-							
04160,160,1710.0	0.0	0.0	0.0	0,0,0	0.14	0.09	0.08162,166,171				
	72.3	3.51e-03	0.02	1.39e-03160,160,171	0.0	0.0	0.0	0,0,0			
180	0.0	5.17e-03	0.02	5.44e-							
03137,132,1710.0	0.0	0.0	0.0	0,0,0	0.04	0.03	0.03141,166,171				
	67.6	5.21e-03	0.02	5.42e-03137,137,171	0.0	0.0	0.0	0,0,0			
181	0.0	3.16e-03	0.02	1.92e-03144,149,171	0.0	0.0	0.0	0,0,0	-		
0.030.02	0.02148,166,171										
	82.2	4.54e-03	0.03	3.22e-03132,135,171	0.0	0.0	0.0	0,0,0			
182	0.0	7.83e-03	0.02	6.89e-							
03151,132,1710.0	0.0	0.0	0.0	0,0,0	0.06	0.05	0.04162,166,171				

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



	70.9	0.01	0.03	0.01151,132,171	0.0	0.0	0.0	0,0,0			
183	0.0	6.14e-03	0.02	6.39e-03141,148,171	0.0	0.0	0.0	0,0,0	-0.23	-0.17	-
0.16148,166,171	23.0	2.25e-03	6.42e-03	1.47e-03141,148,171	0.0	0.0	0.0	0,0,0			
184	0.0	9.50e-									
030.05	0.01137,137,171	0.0	0.0	0.0	0,0,0	0.17	0.12	0.11141,166,171			
	72.0	6.87e-03	0.02	5.43e-03146,148,171	0.0	0.0	0.0	0,0,0			
185	0.0	0.02	0.06	0.02158,132,171	0.0	0.0	0.0	0,0,0	-0.08	-0.05	-
0.04155,166,171	78.6	0.04	0.10	0.04158,132,171	0.0	0.0	0.0	0,0,0			
186	0.0	0.02	0.05	0.02163,163,171	0.0	0.0	0.0	0,0,0	0.12	0.10	0.10 162,166,1
71	70.4	0.02	0.06	0.02162,163,171	0.0	0.0	0.0	0,0,0			
187	0.0	0.03	0.06	0.03156,151,171	0.0	0.0	0.0	0,0,0	-0.14	-0.11	-
0.20162,166,171	140.0	0.04	0.09	0.04132,132,171	0.0	0.0	0.0	0,0,0			
188	0.0	9.32e-									
030.04	0.01144,144,171	0.0	0.0	0.0	0,0,0	0.28	0.32	0.31148,166,171			
	77.5	0.02	0.07	0.02132,132,171	0.0	0.0	0.0	0,0,0			
189	0.0	0.02	0.05	0.02155,151,171	0.0	0.0	0.0	0,0,0	0.16	0.13	0.12 162,166,1
71	70.5	0.02	0.06	0.03156,132,171	0.0	0.0	0.0	0,0,0			
190	0.0	0.02	0.06	0.02155,155,171	0.0	0.0	0.0	0,0,0	-0.02	-0.01	-
0.01162,166,171	65.3	0.01	0.04	0.01155,155,171	0.0	0.0	0.0	0,0,0			
191	0.0	0.02	0.07	0.02155,155,171	0.0	0.0	0.0	0,0,0	-		
0.030.02	0.02148,166,171	0.03	5.64e-03155,155,171	0.0	0.0	0.0	0.0	0,0,0			
	73.8	9.18e-03	0.08	0.02158,132,171	0.0	0.0	0.0	0,0,0	0.07	0.05	0.05 158,165,1
192	0.0	0.02	0.08	0.02158,132,171	0.0	0.0	0.0	0,0,0			
71	78.6	0.03	0.11	0.03158,132,171	0.0	0.0	0.0	0,0,0			
193	0.0	8.08e-03	0.02	0.01146,144,171	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-
0.01148,166,171	64.8	0.01	0.04	0.02149,144,171	0.0	0.0	0.0	0,0,0			
194	0.0	6.79e-03	0.02	5.07e-							
03162,158,1710.0	0.0	0.0	0.0	0.0,0 0.06	0.05	0.05162,166,171					
	86.5	6.28e-03	0.02	4.42e-03162,163,171	0.0	0.0	0.0	0,0,0			
195	0.0	0.03	0.12	0.03158,132,171	0.0	0.0	0.0	0,0,0	0.06	0.06	0.05 158,165,1
71	83.0	0.04	0.13	0.03158,132,171	0.0	0.0	0.0	0,0,0			
196	0.0	0.05	0.16	0.04158,132,171	0.0	0.0	0.0	0,0,0	-		
0.110.04	0.04158,170,171	0.15	0.03132,132,171	0.0	0.0	0.0	0.0	0,0,0			
	78.6	0.04	0.01	6.53e-04162,162,171	0.0	0.0	0.0	0,0,0	-0.30	-0.22	-
197	0.0	3.46e-03	0.01	6.53e-04162,162,171	0.0	0.0	0.0	0,0,0			
0.18162,166,171	33.0	3.97e-03	0.02	7.48e-04162,162,171	0.0	0.0	0.0	0,0,0			
198	0.0	5.32e-03	0.01	5.26e-03160,158,171	0.0	0.0	0.0	0,0,0	-0.11	-0.11	-
0.10162,166,171	66.8	5.61e-03	0.01	5.47e-03160,158,171	0.0	0.0	0.0	0,0,0			
199	0.0	0.03	0.11	0.03158,132,171	0.0	0.0	0.0	0,0,0	-0.04	-0.04	-
0.04158,165,171	83.0	0.04	0.12	0.03158,132,171	0.0	0.0	0.0	0,0,0			
200	0.0	4.46e-03	0.02	3.55e-							
03162,162,1710.0	0.0	0.0	0.0	0.0,0 0.08	0.06	0.05162,166,171					
	105.0	8.00e-03	0.03	6.21e-03162,162,171	0.0	0.0	0.0	0,0,0			
201	0.0	5.00e-03	0.02	3.90e-03160,160,171	0.0	0.0	0.0	0,0,0	-0.10	-0.07	-
0.06162,166,171	71.3	6.54e-03	0.03	5.27e-03160,160,171	0.0	0.0	0.0	0,0,0			
202	0.0	0.02	0.07	0.02162,162,171	0.0	0.0	0.0	0,0,0	-0.18	-0.12	-
0.11162,166,171	58.4	0.02	0.08	0.02162,162,171	0.0	0.0	0.0	0,0,0			
203	0.0	4.02e-03	0.01	3.00e-							
03162,162,1710.0	0.0	0.0	0.0	0.0,0 0.12	0.08	0.07162,166,171					
	77.8	4.11e-03	0.01	2.91e-03162,162,171	0.0	0.0	0.0	0,0,0			
204	0.0	0.04	0.15	0.03132,132,171	0.0	0.0	0.0	0,0,0	0.11	0.09	0.08 158,165,1
71	78.6	0.04	0.14	0.03132,132,171	0.0	0.0	0.0	0,0,0			
205	0.0	5.89e-03	0.02	6.11e-							
03162,162,1710.0	0.0	0.0	0.0	0.0,0 0.08	0.07	0.07146,168,171					
	49.0	8.13e-03	0.02	6.25e-03132,132,171	0.0	0.0	0.0	0,0,0			
206	0.0	3.66e-03	0.02	1.42e-							
03160,160,1710.0	0.0	0.0	0.0	0.0,0 0.14	0.09	0.08162,166,171					
	72.3	4.54e-03	0.02	2.29e-03160,160,171	0.0	0.0	0.0	0,0,0			
207	0.0	5.25e-03	0.02	5.50e-							
03137,137,1710.0	0.0	0.0	0.0	0.0,0 0.04	0.03	0.03141,166,171					
	67.6	4.91e-03	0.02	5.22e-03137,137,171	0.0	0.0	0.0	0,0,0			

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



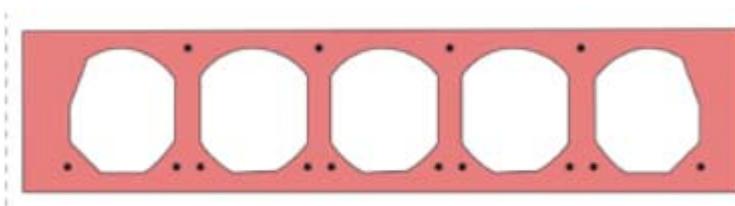
208	0.0	4.44e-03	0.02	3.19e-03	132,135,171	0.0	0.0	0.0	0,0,0	-		
0.030.02	0.02148,166,171											
	82.2	5.10e-03	0.03	3.76e-03	132,135,171	0.0	0.0	0.0	0,0,0			
209	0.0	0.01	0.03	0.01151,132,171		0.0	0.0	0.0	0,0,0	0.06	0.05	0.04 162,166,1
71												
	70.9	0.01	0.03	0.01132,132,171		0.0	0.0	0.0	0,0,0			
210	0.0	0.03	0.10	0.04158,132,171		0.0	0.0	0.0	0,0,0	-0.08	-0.05	-
0.04155,166,171												
	78.6	0.04	0.12	0.05158,132,171		0.0	0.0	0.0	0,0,0			
211	0.0	0.02	0.06	0.02162,163,171		0.0	0.0	0.0	0,0,0	0.12	0.10	0.10 162,166,1
71												
	70.4	0.02	0.07	0.03163,163,171		0.0	0.0	0.0	0,0,0			
212	0.0	0.04	0.10	0.04151,132,171		0.0	0.0	0.0	0,0,0	-0.14	-0.11	-
0.20162,166,171												
	73.2	0.04	0.10	0.05132,132,171		0.0	0.0	0.0	0,0,0			
213	0.0	0.02	0.07	0.02132,132,171		0.0	0.0	0.0	0,0,0	0.28	0.32	0.31 148,166,1
71												
	77.5	0.02	0.10	0.03132,132,171		0.0	0.0	0.0	0,0,0			
214	0.0	0.02	0.06	0.03155,151,171		0.0	0.0	0.0	0,0,0	0.16	0.13	0.12 162,166,1
71												
	70.5	0.02	0.07	0.03156,132,171		0.0	0.0	0.0	0,0,0			
215	0.0	0.01	0.04	0.01155,155,171		0.0	0.0	0.0	0,0,0	-0.02	-0.01	-
0.01162,166,171												
	43.9	9.22e-03	0.02	6.76e-03	162,162,171	0.0	0.0	0.0	0,0,0			
216	0.0	9.05e-03	0.03	5.55e-03	155,155,171	0.0	0.0	0.0	0,0,0	-		
0.030.02	0.02148,166,171											
	73.8	7.55e-03	0.02	5.04e-03	132,158,171	0.0	0.0	0.0	0,0,0			
217	0.0	0.03	0.11	0.03158,132,171		0.0	0.0	0.0	0,0,0	0.07	0.05	0.05 158,165,1
71												
	78.6	0.04	0.12	0.04158,132,171		0.0	0.0	0.0	0,0,0			
218	0.0	0.01	0.04	0.02149,144,171		0.0	0.0	0.0	0,0,0	-0.03	-0.02	-
0.01148,166,171												
	64.8	0.02	0.05	0.02149,144,171		0.0	0.0	0.0	0,0,0			
219	0.0	6.74e-03	0.02	4.79e-		0.0	0.0	0.0	0,0,0			
03162,158,171	10.0	0.0	0.0	0,0,0	0.06	0.05	0.05162,166,171					
	88.0	6.80e-03	0.02	4.99e-03	162,163,171	0.0	0.0	0.0	0,0,0			
220	0.0	0.04	0.13	0.03158,132,171		0.0	0.0	0.0	0,0,0	0.06	0.06	0.05 158,165,1
71												
	78.0	0.04	0.13	0.04158,132,171		0.0	0.0	0.0	0,0,0			
221	0.0	0.04	0.15	0.03132,132,171		0.0	0.0	0.0	0,0,0	-		
0.110.04	0.04158,165,171											
	78.6	0.04	0.14	0.03132,132,171		0.0	0.0	0.0	0,0,0			
222	0.0	3.66e-03	0.01	3.74e-04	162,162,171	0.0	0.0	0.0	0,0,0	-0.30	-0.22	-
0.18162,166,171												
	95.0	4.94e-03	0.02	5.91e-04	162,162,171	0.0	0.0	0.0	0,0,0			
223	0.0	5.65e-03	0.01	5.40e-03	160,158,171	0.0	0.0	0.0	0,0,0	-0.11	-0.11	-
0.10162,166,171												
	66.8	6.21e-03	0.01	6.02e-03	160,158,171	0.0	0.0	0.0	0,0,0			
224	0.0	0.04	0.12	0.03158,132,171		0.0	0.0	0.0	0,0,0	-0.04	-0.04	-
0.04158,165,171												
	78.0	0.04	0.12	0.04158,132,171		0.0	0.0	0.0	0,0,0			
225	0.0	7.26e-03	0.03	5.58e-		0.0	0.0	0.0	0,0,0			
03162,162,171	10.0	0.0	0.0	0,0,0	0.08	0.06	0.05162,166,171					
	77.4	8.44e-03	0.03	6.01e-03	162,162,171	0.0	0.0	0.0	0,0,0			
226	0.0	6.68e-03	0.03	5.34e-03	160,160,171	0.0	0.0	0.0	0,0,0	-0.10	-0.07	-
0.06162,166,171												
	71.3	8.01e-03	0.04	6.69e-03	160,160,171	0.0	0.0	0.0	0,0,0			
227	0.0	0.02	0.09	0.02162,162,171		0.0	0.0	0.0	0,0,0	-0.18	-0.12	-
0.11162,166,171												
	95.0	0.02	0.10	0.03162,162,171		0.0	0.0	0.0	0,0,0			
228	0.0	4.19e-03	0.02	3.00e-		0.0	0.0	0.0	0,0,0			
03162,162,171	10.0	0.0	0.0	0,0,0	0.12	0.08	0.07162,166,171					
	77.8	4.10e-03	0.01	2.83e-03	162,162,171	0.0	0.0	0.0	0,0,0			
229	0.0	0.04	0.14	0.03132,132,171		0.0	0.0	0.0	0,0,0	0.11	0.09	0.08 158,165,1
71												
	78.6	0.03	0.13	0.02132,132,171		0.0	0.0	0.0	0,0,0			
230	0.0	3.13e-03	2.89e-03	9.38e-04	132,132,171	0.0	0.0	0.0	0,0,0	-6.84e-03	-4.78e-03	-4.35e-
03146,168,171												
	14.0	4.18e-03	5.00e-03	2.32e-03	132,132,171	0.0	0.0	0.0	0,0,0			
231	0.0	4.71e-03	0.02	2.34e-		0.0	0.0	0.0	0,0,0			
03160,160,171	10.0	0.0	0.0	0,0,0	0.14	0.09	0.08162,166,171					
	72.3	5.86e-03	0.03	4.14e-03	160,160,171	0.0	0.0	0.0	0,0,0			
232	0.0	5.13e-03	0.02	5.45e-		0.0	0.0	0.0	0,0,0			
03142,137,171	10.0	0.0	0.0	0,0,0	0.04	0.03	0.03142,166,171					
	67.6	4.36e-03	0.01	4.70e-03	142,137,171	0.0	0.0	0.0	0,0,0			
233	0.0	5.03e-03	0.02	3.70e-03	132,132,171	0.0	0.0	0.0	0,0,0	-		

Realizzazione nuova scuola dell'infanzia "Staccia Buratta" nel Comune di Vinci (FI)
 RELAZIONE DI CALCOLO DELLA FONDAZIONE



0.030.02	0.02148,166,171												
	82.2	4.96e-03	0.02	3.68e-03	132,132,171	0.0	0.0	0.0	0,0,0				
234	0.0	0.01	0.03	0.01151,	132,171	0.0	0.0	0.0	0,0,0	0.06	0.05	0.04 162,166,1	
71													
	70.9	0.01	0.03	0.01132,	132,171	0.0	0.0	0.0	0,0,0				
235	0.0	0.04	0.13	0.05158,	132,171	0.0	0.0	0.0	0,0,0	-0.08	-0.05	-	
0.04155,166,171													
	78.6	0.05	0.14	0.05158,	132,171	0.0	0.0	0.0	0,0,0				
236	0.0	0.02	0.08	0.03163,	163,171	0.0	0.0	0.0	0,0,0	0.12	0.10	0.10 162,166,1	
71													
	70.4	0.03	0.08	0.03163,	163,171	0.0	0.0	0.0	0,0,0				
237	0.0	0.04	0.10	0.05132,	132,171	0.0	0.0	0.0	0,0,0	-0.14	-0.11	-	
0.20162,166,171													
	73.2	0.04	0.10	0.04132,	132,171	0.0	0.0	0.0	0,0,0				
238	0.0	0.02	0.09	0.03132,	132,171	0.0	0.0	0.0	0,0,0	0.28	0.32	0.31 148,166,1	
71													
	77.5	0.03	0.11	0.03132,	132,171	0.0	0.0	0.0	0,0,0				
239	0.0	0.03	0.07	0.03155,	132,171	0.0	0.0	0.0	0,0,0	0.16	0.13	0.12 162,166,1	
71													
	70.5	0.02	0.07	0.03156,	132,171	0.0	0.0	0.0	0,0,0				
240	0.0	9.55e-03	0.02	7.26e-03	162,162,171	0.0	0.0	0.0	0,0,0	7.27e-03	4.57e-03	3.92e-	
03162,166,171													
	21.4	8.43e-03	0.02	5.92e-03	162,162,171	0.0	0.0	0.0	0,0,0				
241	0.0	7.83e-03	0.02	5.28e-03	132,158,171	0.0	0.0	0.0	0,0,0	-			
0.030.02	0.02148,166,171												
	73.7	0.01	0.03	0.02132,	158,171	0.0	0.0	0.0	0,0,0				
242	0.0	0.03	0.12	0.04158,	132,171	0.0	0.0	0.0	0,0,0	0.07	0.05	0.05 158,165,1	
71													
	78.6	0.04	0.13	0.04158,	132,171	0.0	0.0	0.0	0,0,0				
243	0.0	0.02	0.05	0.02149,	144,171	0.0	0.0	0.0	0,0,0	-0.03	-0.02	-	
0.01148,166,171													
	64.8	0.02	0.06	0.02149,	144,171	0.0	0.0	0.0	0,0,0				
244	0.0	7.93e-03	0.03	5.75e-									
03162,158,171	10.0	0.0	0.0	0,0,0	0.06	0.05	0.05	162,166,171					
	140.0	6.62e-03	0.02	4.70e-03	148,163,171	0.0	0.0	0.0	0,0,0				
245	0.0	0.04	0.13	0.04132,	132,171	0.0	0.0	0.0	0,0,0	-0.14	-0.11	-	
0.10158,165,171													
	73.0	0.03	0.11	0.03132,	132,171	0.0	0.0	0.0	0,0,0				
246	0.0	0.04	0.14	0.03132,	132,171	0.0	0.0	0.0	0,0,0	-			
0.110.04	0.04158,165,171												
	78.6	0.03	0.13	0.03132,	132,171	0.0	0.0	0.0	0,0,0				
247	0.0	4.18e-03	0.01	6.09e-04	132,132,171	0.0	0.0	0.0	0,0,0	-0.30	-0.22	-	
0.18162,166,171													
	72.5	4.98e-03	0.01	8.45e-04	132,132,171	0.0	0.0	0.0	0,0,0				
248	0.0	6.23e-03	0.02	5.96e-03	160,158,171	0.0	0.0	0.0	0,0,0	-0.11	-0.11	-	
0.10162,166,171													
	66.8	7.11e-03	0.02	7.25e-03	160,158,171	0.0	0.0	0.0	0,0,0				
249	0.0	0.04	0.12	0.04132,	132,171	0.0	0.0	0.0	0,0,0	0.07	0.06	0.05 158,165,1	
71													
	78.0	0.03	0.10	0.03132,	132,171	0.0	0.0	0.0	0,0,0				
250	0.0	8.30e-03	0.03	5.86e-									
03162,162,171	10.0	0.0	0.0	0,0,0	0.08	0.06	0.05	162,166,171					
	77.4	9.06e-03	0.03	6.00e-03	162,162,171	0.0	0.0	0.0	0,0,0				
251	0.0	8.18e-03	0.04	6.80e-03	160,160,171	0.0	0.0	0.0	0,0,0	-0.10	-0.07	-	
0.06162,166,171													
	76.3	9.47e-03	0.04	8.63e-03	160,160,171	0.0	0.0	0.0	0,0,0				
252	0.0	0.02	0.09	0.03162,	162,171	0.0	0.0	0.0	0,0,0	-0.18	-0.12	-	
0.11162,166,171													
	74.3	0.02	0.09	0.02162,	162,171	0.0	0.0	0.0	0,0,0				
253	0.0	4.22e-03	0.02	2.93e-									
03162,162,171	10.0	0.0	0.0	0,0,0	0.12	0.08	0.07	162,166,171					
	77.8	4.02e-03	0.01	2.73e-03	162,162,171	0.0	0.0	0.0	0,0,0				
254	0.0	0.03	0.13	0.02132,	132,171	0.0	0.0	0.0	0,0,0	0.11	0.09	0.08 158,165,1	
71													
	78.6	0.03	0.11	0.02132,	132,171	0.0	0.0	0.0	0,0,0				
255	0.0	7.24e-03	0.01	1.68e-03	132,132,171	0.0	0.0	0.0	0,0,0	-6.84e-03	-4.78e-03	-4.35e-	
03139,167,171													
...													
	566	590.0	7.21e-03	0.03	8.54e-03	160,138,171	0.0	0.0	0.0	0,0,0	0.04	0.02	-
0.01141,166,171													
Trave		rRfck	rRfyk	rPfck		wR	wF	wP		dR	dF	dP	
		0.10	0.25	0.09		0.0	0.0	0.0		-0.30	-0.22	-0.20	
										0.28	0.32	0.31	

VERIFICA SOLAIO ALVEOLARE



NOTA: I carichi sono da considerarsi utili, cioè oltre il peso proprio del solaio. Il solaio è stato considerato senza soletta collaborante. In presenza dell'eventuale soletta da 4 - 6 cm il maggior peso è compensato dalla maggior portata, pertanto l'abaco dei carichi non cambia. Le luci di calcolo indicate prescindono dal rispetto della limitazione.

ABACO PORTATE UTILI SOLAIO R90 APPOGGIO																			
LUCI MAX (m)		6	7	8	9	10	11	12	13	14	15	16	17	18	19	20			
		21.00	15.00	11.50	8.50	6.50	5.00	3.50	2.00								H26.5		
CARICHI		24.00	19.00	15.00	12.50	10.00	7.50	5.70	4.50	3.20	2.20						H32		
(KN/M²)				22.00	18.20	15.00	12.20	9.80	7.80	6.00	4.80	3.80	2.80	2.00			H36		
					23.00	18.00	14.50	12.00	10.00	8.00	6.50	5.00	3.90	3.00	2.20	1.50	H40		
						24.00	19.80	16.00	12.70	10.10	8.00	6.20	4.60	3.20			H50		

ANALISI DEI CARICHI

Pavimento sp. 2 cm	50	Kg/m ²	G2
Riscaldamento a pavimento (EPS 2 cm + massetto 4 cm)	90	Kg/m ²	G2
Pannello isolante XPS sp. 10 cm	8	Kg/m ²	G2
Soletta c.c.a. sp. 5 cm	125	Kg/m ²	G1
Solaio alveolare sp. 26.5 cm	360	Kg/m ²	G1
TOTALE PESO PROPRIO + PERMANENTE	485	Kg/m²	G1
PESO PERMANENTE NON DEFINITO	148	Kg/m²	G2
CARICO VARIABILE cat. C	300	Kg/m²	Q

CARICHI PORTATI: G1 = 125 KG/mq G2 = 148 KG/mq Q = 300 KG/mq

Combinazione SLU:

$$q = 1.3 \times 125 + 1.5 \times 148 + 1.5 \times 300 = 834.5 \text{ kg/mq} = 8.35 \text{ kN/mq}$$

Luce massima: 7.65 m

Dalla tabella di dimensionamento fornita dal produttore, entrando con luce massima 8 m e altezza solaio 26.5 cm, si ha una portata utile di 8.50 kN/mq, superiore a quella di progetto allo SLU.